

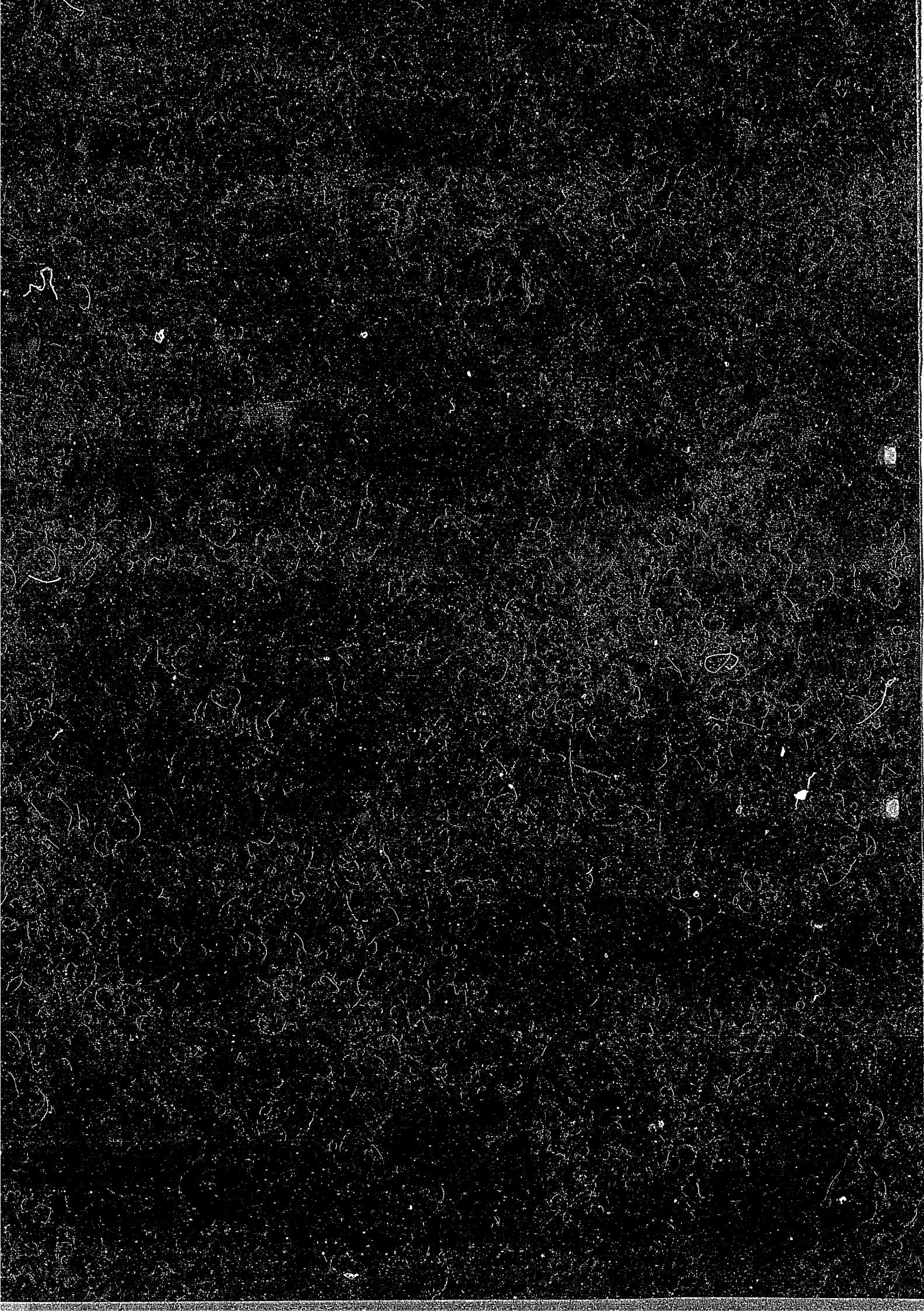
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**ANGULAR DEPENDENCE OF SPUTTERING YIELDS  
OF MONATOMIC SOLIDS**

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## Abstract

The angular dependence of sputtering yields of light-ion sputtering and heavy-ion sputtering has been investigated in detail, and the following empirical formula is proposed:

$$\frac{Y(\theta)}{Y(0)} = t^f \exp [ -\Sigma (t - 1)] ,$$

where  $\theta$  is the angle of incidence measured from the surface normal, and  $t = 1/\cos \theta$ . The parameters  $f$  and  $\Sigma$  are adjustable parameters which are determined by the least-square method so as to fit the present empirical formula to available experimental data.

The best-fit parameters and their average values are listed in tables, where the value of  $\theta_{opt}$  is listed in place of  $\Sigma$ . Here,  $\theta_{opt}$  is the angle of incidence at the maximum yield and the relation between  $\theta_{opt}$  and  $\Sigma$  is simple, i.e.,

$$\Sigma = f \cos \theta_{opt} .$$

The present empirical formula has been compared with available experimental data of various ion-target combinations, and it is found that the agreement is satisfactory in a wide range of the angle of incidence.

## 1. Introduction

Current needs for sputtering yield at normal incidence and at oblique incidence have accelerated the experimental measurements of sputtering yields, particularly by light ions. The extensive uses of sputtering data for the design of the fusion reactors required the comparison of experimental data with empirical formula and the reliable empirical formulae at normal and oblique incidences.

The empirical formulae for the sputtering yields at normal incidence have been proposed by Bohdansky et al.<sup>1</sup>, Matsunami et al.<sup>2</sup>, and Yamamura et al.<sup>3</sup> The compilations of the experimental data for available combinations of ions and target atoms have been published<sup>4,5</sup>.

The angular dependence of sputtering yields has been investigated by many authors<sup>6-25</sup> and it was found that its dependence on the angle of incidence was roughly given by  $\cos^{-1}\theta$  for not-too-oblique incidence,<sup>8</sup> where  $\theta$  is measured from the surface normal. On the other hand, the theoretical investigation on the angular dependence of sputtering yields was done by Sigmund<sup>26</sup>, who showed that the normalized yield  $Y(\theta)/Y(0)$  had the  $\cos^{-f}\theta$ -dependence at not-too-oblique incidence, where  $1 < f < 2$ .

At energies around 1 keV, the angular dependence of sputtering yields has been investigated systematically by Oechsner<sup>19</sup>. For not-too-large angles of incidence, he found that the normalized yield obeyed a simple relation  $\Delta Y(\theta)/\Delta Y(\theta_{opt}) = 1.2 \hat{\theta}^2$ , where  $\hat{\theta} = \theta/\theta_{opt}$ ,  $\Delta Y(\theta) = Y(\theta) - Y(0)$ , and  $\theta_{opt}$  is the angle of incidence at the maximum yield.

The rapid variation of sputtering yields with the angle of incidence has been reported by Bay et al.<sup>20</sup> for light-ion sputtering in low keV region. They found that the lighter the projectile, the maximum of the normalized yield was higher and also it increased with increasing

the energy and increasing the surface binding energy. For the grazing angle of incidence, the surface channeling plays an important role and makes the drop-off of the sputtering yield at the glancing angles.

It is desired to have some analytical formula describing the angular dependence of the sputtering yields in a wide range of the angle of incidence. In this paper, a simple formula for the angular dependence of the normalized sputtering yield  $Y(\theta)/Y(0)$  is proposed, taking into account the effect of the surface channeling at large angles, and the comparison of the present empirical formula with the existing experimental data will be made in detail.

## 2. An empirical formula for angular dependence of sputtering yields

Light-ion sputtering is mainly due to collision cascades created by ions backscattered from the interior of the solid, while the heavy-ion sputtering is due to collision cascades generated by incoming ions directly<sup>27</sup>. This difference is very important for low-energy sputtering, especially for the angular dependence of low-energy sputtering.

In the case of light-ion sputtering, the angular dependence of the threshold energy does not have a clear minimum. On the contrary, in the case of heavy-ion sputtering, the angular dependence of the threshold energy has a minimum near  $60^\circ$ . The threshold energy of heavy-ion sputtering is a decreasing function of the angle of incidence because of the anisotropic velocity distribution of recoil atoms near the surface, and for grazing angles of incidence it increases rapidly with increasing angle of incidence because of surface channeling. (see APPENDIX A). In other words, even if the ion energy is less than the threshold energy at normal incidence, the finite number of target atoms will be sputtered in oblique incidence in the case of heavy-ion sputtering. It must be noted that the normalized sputtering yield  $Y(\theta)/Y(0)$  can not be well defined in such a low energy region.

## 2.1 Angular dependence of light-ion sputtering

Light-ion sputtering is directly connected with the particle reflection coefficient because it is due to collision cascades generated by backscattered ions. Recently, Yamamura et al. have derived the following formula<sup>28</sup>

$$Y(E) = 0.042 \frac{F_D(E^*) R_N(E)}{U_s} [1 - (\frac{E_{th}}{E})^{\frac{1}{2}}]^{2.8} \quad (1)$$

for light-ion sputtering at normal incidence, where  $F_D(E^*)$  is the deposited energy near the solid surface by a backscattered ion,  $E^*$  is the average energy of the reflected ion, and  $R_N(E)$  is the particle reflection coefficient of the ion with the incident energy  $E$ . The surface binding energy  $U_s$  is taken to be equal to the sublimation energy.  $E_{th}$  is the threshold energy of the sputtering at normal incidence.

For not-too-oblique incidence, the normalized yield is given by

$$\frac{Y(\theta)}{Y(0)} = \frac{F_D(E^*(\theta))}{F_D(E^*)} \frac{R_N(E, \theta)}{R_N(E)} \quad (2)$$

where the threshold effect of the light ion sputtering is neglected because of its weak angular dependence and  $Y(0)$  is the sputtering yield at normal incidence which is described by  $Y(E)$  in eq.(1). Similarly  $R_N(E)$  means  $R_N(E, \theta=0)$ .

The angular dependence of the reflection coefficient is roughly estimated in terms of the range distribution. For very small angles of incidence, the ratio  $R_N(E, \theta)/R_N(E)$  is given by

$$\frac{R_N(E, \theta)}{R_N(E)} = \frac{\int_0^\infty dx F(E, \theta, x)}{\int_0^\infty dx F(E, 0, x)} = (\cos \theta)^{-f_R}, \quad (3)$$

where

$$f_R = 1 + \frac{\langle Y^2 \rangle_R}{\langle \Delta X^2 \rangle_R}, \quad (4)$$

and  $F(E, \theta, x)$  is the range distribution and the subscript R of the moments means those of the range distribution. The exponent  $f_R$  is nearly equal to 2 for large mass ratio<sup>29</sup>.

Since  $E^*(\theta)$  does not depend so largely on the angle of incidence,

the angular dependence of  $Y(\theta)/Y(0)$  is mainly determined by those of the particle reflection coefficient, and we can write

$$\frac{Y(\theta)}{Y(0)} = (\cos \theta)^{-f_R} . \quad (5)$$

As the angle of incidence increases, the effect of surface channeling becomes important. In order to sputter target atoms at the outermost layer, the projectile must penetrate the first layer of the solid surface, and this penetration probability is roughly estimated by

$$\exp(-N\sigma R_0/\cos \theta),$$

where  $\sigma$  is the hard-sphere collision cross section between a projectile and a target atom,  $R_0 = N^{-\frac{1}{3}}$  is the average lattice constant of the random target, and  $N$  is the number density of the target atom.

From above discussions we know that the angular dependence of the normalized yield will have the form

$$\frac{Y(\theta)}{Y(0)} = t^f \exp[-\Sigma(t - 1)] , \quad (6)$$

where  $t = 1/\cos \theta$  and the parameters  $f$  and  $\Sigma$  are adjustable parameters. The angle of incidence at the maximum yield is simply given by

$$\theta_{opt} = \cos^{-1}\left(\frac{\Sigma}{f}\right) . \quad (7)$$

Using the least-square method, the best-fit parameters to the present empirical formula are obtained from experimental data<sup>19,20,21,24</sup> and computer results (ACAT)<sup>30</sup>. The best-fit values of  $f$  and  $\theta_{opt}$  are listed in Table 2. It is very interesting that the best fit  $f$ 's are nearly equal to 2 which is a theoretical value of Eq. (4).

The best-fit values of  $f$  depend slightly on the sublimation energy and so the ratio of the best-fit  $f$  to  $\sqrt{U_s}$  is plotted as a function of mass ratio  $M_2/M_1$  in Fig. 1, where  $M_1$  and  $M_2$  are the atomic masses of a projectile and a target atom, respectively. The solid line in Fig. 1 corresponds to the average value of  $f$  which satisfies the following relation:

$$\frac{f}{\sqrt{U_s}} = 0.94 - 1.33 \times 10^{-3} (M_2/M_1). \quad (8)$$

In Fig. 2 the best-fit values of  $\theta_{opt}$  are plotted as a function of

$$\eta = \frac{a}{R_0} \left( \frac{1}{2 \epsilon q} \right)^{\frac{1}{2}}, \quad (9)$$

where  $q = (U_s/\gamma E)^{\frac{1}{2}}$  corresponds to the cosine of the scattering angle of a recoil atom which gains the energy  $U_s$  in a single collision.

The LSS reduced energy  $\epsilon$  is defined by  $\epsilon = E/E_L$ , where

$$E_L = \frac{M_1 + M_2}{M_2} \frac{z_1 z_2 e^2}{a}, \quad (10)$$

$$a = 0.4685 \left( \frac{1}{z_1^{2/3} + z_2^{2/3}} \right)^{\frac{1}{2}}. \quad (11)$$

$z_1$  and  $z_2$  are the atomic numbers of a projectile and a target atom, respectively and  $\gamma = 4M_1 M_2 / (M_1 + M_2)^2$ ,  $M_1$  and  $M_2$  being their masses.

The solid line in Fig. 2 is a theoretical curve of  $\theta_{opt}^{31}$

$$\theta_{opt} = 90^\circ - 57.3 \eta \quad (12)$$

which is derived from the direct knock-out model. The Agreement between the best-fit values and the theoretical results is very good, and so we can calculate  $\theta_{opt}$  from the theoretical formula.

## 2.2 Angular dependence of heavy-ion sputtering

In the case of heavy-ion sputtering, one cannot neglect the threshold effect which is a decreasing function of the angle of incidence for the not-too-oblique incidence. This means that the normalized yield has the following angular dependence:

$$\frac{Y(\theta)}{Y(0)} = (\cos \theta)^{-f_S} \left[ \frac{1 - (E_{th}/E)^{\frac{1}{2}} \cos \theta}{1 - (E_{th}/E)^{\frac{1}{2}}} \right] \quad (13)$$

where the exponent  $f_S$  is given in the form by Sigmund<sup>26</sup> as follows:

$$f_S = 1 + \frac{\langle Y^2 \rangle_D}{\langle \Delta X^2 \rangle_D} [ \frac{\langle X \rangle_D^2}{\langle \Delta X^2 \rangle_D} - 1 ] \quad (14)$$

for not-too-large angles of incidence, where the subscript D of the moment means those of the damage distribution.

The necessary condition for the genuine collision cascade near the solid surface is that the projectile must penetrate a few layer of the surface. This means that an empirical formula for heavy-ion sputtering can be expressed by the product of the similar expression to that for light-ion sputtering and the threshold term of Eq. (13). At present, the threshold energy is not well established. For simplicity, let us employ an empirical formula with the same functional form as that of light-ion sputtering, eq.(6), i.e.,

$$\frac{Y(\theta)}{Y(0)} = t^f \exp[-\Sigma(t-1)], \quad (15)$$

where the exponent f will include the threshold effect of Eq. (13), and so it will depend on the ion energy in the low-energy region. This tendency is much different from light-ion sputtering.

The best-fit parameters to the present formula, Eq. (15), are obtained for about 25 ion-target combinations (Table 1), using the least-square method and are listed in Table 3. In the energy region where the threshold effect can be neglected, the best-fit values of f are consistent with Sigmund  $f_S$ , as shown in Fig. 3.

In Fig. 4 the ratios of the best-fit f's to Sigmund  $f_S$  are plotted as a function of  $\zeta = 1 - (E_{th}/E)^{\frac{1}{2}}$ , where  $E_{th}$  is calculated from the following relation:<sup>3</sup>

$$E_{th} = 1.5 \frac{U_S}{\gamma} [ 1 + 1.38 (M_1/M_2)^h ]^2 \quad (16)$$

with  $h = 0.834$  for  $M_2 > M_1$  and  $h = 0.18$  for  $M_2 < M_1$ . This empirical relation for the threshold energy corresponds to the second Matsunami formula for sputtering yields at normal incidence<sup>3</sup>. The solid line in Fig. 4 is

$$\frac{f}{f_s} = 1 + 2.5 \frac{1 - \zeta}{\zeta} . \quad (17)$$

Equation (17) shows that  $f$  is infinite at  $E = E_{th}$ , which corresponds to the fact that the normalized sputtering yield  $Y(\theta)/Y(0)$  is not well defined in the energy region of  $E < E_{th}$ .

In Fig. 5 the best-fit values of  $90^\circ - \theta_{opt}$  are plotted against

$$\psi = \left( \frac{a}{R_0} \right)^{3/2} \left| \frac{z_1 z_2}{(z_1^{2/3} + z_2^{2/3})^{1/2}} \frac{1}{E} \right|^{\frac{1}{2}} . \quad (18)$$

The parameter  $\psi$  is directly connected with the critical angle

$$\psi_c = (U_R(0)/E)^{\frac{1}{2}} \quad (19)$$

of surface channeling, where  $U_R(0)$  is the average potential at the amorphous solid surface which is defined in APPENDIX A. The solid line in Fig. 5 means the average value of the best-fit  $\theta_{opt}$ 's which has the form

$$\theta_{opt} = 90^\circ - 286.0 \psi^{0.45} . \quad (20)$$

### 3. Compilation of Experimental Data on Angular Dependence of Sputtering Yields

The angular dependence of sputtering yields of various combinations has been compiled and stored in a computer. The compiled data are summarized in Table 1. When determining the best-fit values of the adjustable parameters  $f$  and  $\Sigma$ , we excluded the experimental data which do not have explicit maximum values or which do not have the data at normal incidence.

Table 4 shows the physical constants necessary for calculating the angular dependence of the sputtering yield by means of the present empirical formula. For extensive use of the present empirical formula, the parameters  $f$  and  $\eta$  are calculated from Eq. (8) and Eq. (9) for typical projectiles H, D, T and He, which are listed in Tables 5, 6

7 and 8, where the calculated parameters  $\eta$  correspond to 1 keV ion.

For calculations of the angular dependence of heavy-ion sputtering,  
<sup>26</sup> Sigmund f of  $m = 1/3$  and  $\psi$  for 1 eV ion are also calculated and listed in Tables 9 through 18, where as the typical projectiles C, Al, Ar, Fe, Ni, Cu, Kr, Xe and Hg ions are selected.

The plots of the angular dependence of sputtering yields for various combinations of the incident ions and the target atoms are shown in Figs. 6 through 58, where Figs. 6 through 24 correspond to light-ion sputtering and Figs. 25 through 58 to heavy-ion sputtering. The solid lines in these figures are best fit curves to the present empirical formula, and the solid lines with cross marks show the results calculated by putting the average values of the best-fit parameters into each empirical formula.

In order to know the absolute yield  $Y(\theta)$ , one must calculate the sputtering yield at normal incidence. The authors recommend to use the third Matsunami formula for the sputtering yield at normal incidence, which has the form<sup>32</sup>

$$Y(E) = P \frac{s_n(\varepsilon)}{1 + 0.35U_s s_e(\varepsilon)} [1 - (E_{th}/E)^{\frac{1}{2}}]^{2.8}, \quad (21)$$

where

$$P = 0.042 \frac{E_L}{R_L} \frac{N}{U_s} \alpha(M_2/M_1) Q(z_2), \quad (22)$$

$$R_L = \frac{1}{\pi a_N^2 \gamma}, \quad (22)$$

$$s_e(\varepsilon) = k \varepsilon^{\frac{1}{2}}, \quad (23)$$

and  $s_n(\varepsilon)$  is the LSS elastic stopping cross section in the reduced unit and the following analytical expression is useful for the present purpose:<sup>2</sup>

$$s_n(\varepsilon) = \frac{3.441\sqrt{\varepsilon} \log(\varepsilon + 2.718)}{1 + 6.355\sqrt{\varepsilon} + \varepsilon(-1.708 + 6.882\sqrt{\varepsilon})}. \quad (24)$$

The inelastic coefficient  $k$  of  $s_e(\varepsilon)$  is given as<sup>33</sup>

$$k = 0.0793 z_1^{1/6} \frac{(z_1 z_2)^{1/2} (M_1 + M_2)^{3/2}}{(z_1^{2/3} + z_2^{2/3})^{3/4} M_1 (M_1 M_2)^{1/2}}, \quad (25)$$

and the threshold energy  $E_{th}$  for the third Matsunami formula has the following empirical relation:

$$E_{th} = U_s [1.9 + 3.8(M_1/M_2) + 0.314(M_2/M_1)^{1.24}]. \quad (26)$$

The parameter  $\alpha(M_2/M_1)$  is represented as

$$\alpha(M_2/M_1) = 0.08 + 0.164 (M_2/M_1)^{0.45} + 0.0145 (M_2/M_1)^{1.29} \quad (27)$$

and  $Q(z_2)$  is listed in Table 4 for each element. For extensive uses of the third Matsunami formula, the parameters  $E_L$ ,  $P$ ,  $E_{th}$ ,  $\alpha$  and  $k$  are listed in Tables 19 through 32 for various ion-target combinations, where as the projectile H, D, T, He, C, Ne, Al, Ar, Fe, Ni, Cu, Kr, Xe and Hg are selected.

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APPENDIX A: ANGULAR DEPENDENCE OF THRESHOLD ENERGY OF LIGHT-ION SPUTTERING AND HEAVY-ION SPUTTERING

The sputtering mechanism for oblique incidence is separated into three parts: 1) The mechanism due to the direct knock-out collisions with incident ions at the outermost layer of the solid surface (mechanism Ia of Fig. A1). 2) The mechanism due to collision cascades created by incoming ions near the solid surface (mechanism Ib of Fig. A1) 3) The mechanism due to collision cascades generated by ions backscattered from the interior of the solids (mechanism II of Fig. A1).

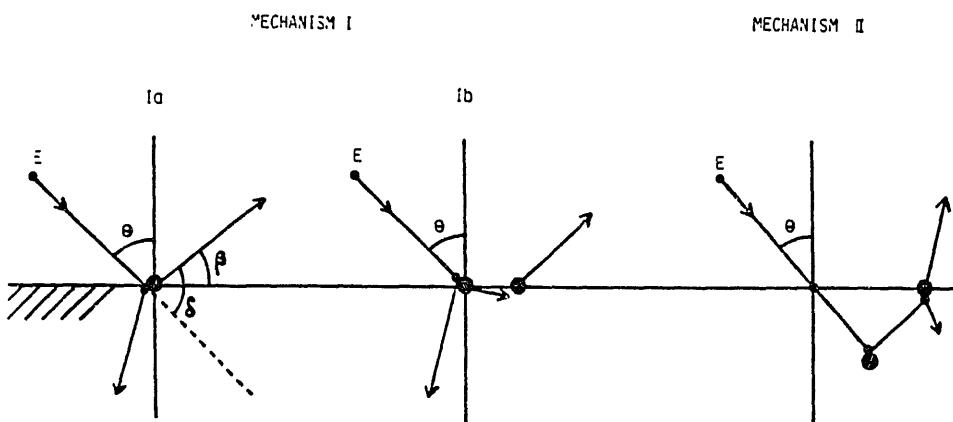


Fig. A1 Schematic representation of sputtering mechanism at oblique incidence

For light-ion sputtering the mechanisms Ia and II play an important role.

The threshold energy of mechanism II is given as<sup>34</sup>

$$E_{th} = \frac{U_s}{\gamma} \frac{1}{(1 - \gamma)} \quad (A1)$$

for normal incidence. For not-too-large angles of incidence, the factor  $(1 - \gamma)$  of Eq. (A1) must be modified. If only a single collision process is taken into consideration, the threshold energy will be a slightly decreasing function of the angle of incidence. For oblique incidence, however, the multiple scattering becomes important and this effect weaken the angular dependence of the factor  $(1 - \gamma)$ . Roughly speaking, the threshold energy of mechanism II is

$$E_{th} = \frac{U_s}{\gamma} \frac{1}{1 - \gamma \cos^2(\theta/2)} \quad (A2)$$

for not-too-oblique incidence, where the difference of the scattering angles between in the L system and in the CM system is neglected because of large mass ratio.

For oblique incidence, an incoming ion must penetrate the first layer for mechanism II. The average potential at the surface of the amorphous solids is roughly estimated by

$$U_R(y) = \frac{1}{R_0^3} \int_{-R_0/2}^{+R_0/2} dz \int_0^\infty 2\pi r dr V(\sqrt{(y-z)^2 + r^2}) \quad (A3)$$

where  $y$  is the distance from the surface and  $V(r)$  is the interatomic potential. If one employ the Moliere potential as the interatomic potential we have

$$U_R(y) = 4\pi \frac{A}{A+1} E_L \left( \frac{a}{R_0} \right)^3 \sum_{i=1}^3 \frac{\alpha_i}{\beta_i^2} \sinh\left(\frac{\beta_i R_0}{2a}\right) \exp\left(-\frac{\beta_i}{a}y\right),$$

where  $A = M_2/M_1$ ,  $(A4)$

$$\alpha_i = (0.35, 0.55, 0.10)$$

$$\beta_i = (0.3, 1.2, 6.0).$$

The critical angle for penetration through the first layer is given as

$$\psi_c = \cos^{-1} \left[ \frac{U_R(0)}{E} \right]^{\frac{1}{2}}, \quad (A5)$$

where  $\psi_c$  is measured from the surface normal. The critical angle  $\psi_c$  for the incident energy of the order of the threshold energy is about  $50^\circ$  for H - Ni. For  $\theta < \psi_c$ ,  $E_{th}$  of the mechanism II is given by eq.(2).

For grazing angles of incidence ( $\theta > 70^\circ$ ), the direct knock-out process become important and the criterion of the sputtering due to this process is given by <sup>31</sup>

$$\cos \theta + 2q < 1 \quad (A7)$$

$$p_2 > p_1 > R_0 \cos \theta \quad (A8)$$

where  $q = (U_s/\gamma E)^{\frac{1}{2}}$  and the impact parameters  $p_1$  and  $p_2$  are the lower and the upper limits of the impact parameters available for the sputtering due to the direct knock-out process.

From the inequality of Eq. (A7) we obtain

$$E_{th}(\theta) = \frac{U_s}{\gamma} \frac{1}{\sin^4(\theta/2)} \quad (A9)$$

The criterion of Eq. (A8) is not important as compared with surface channeling for oblique incidence. Namely, in order to knock off an atom at the outermost layer, an ion must arrive at the surface. This leads to the following expression for the threshold energy:

$$E_{th}(\theta) = \frac{U_R(R_0/2)}{\cos^2 \theta} \quad (A10)$$

where  $U_R(R_0/2)$  is the average potential at the distance  $R_0/2$ , at which there exists an atom with a finite probability in the case of the random target. From Eq. (A4),

$$U_R(R_0/2) \approx U_R(0)/2.$$

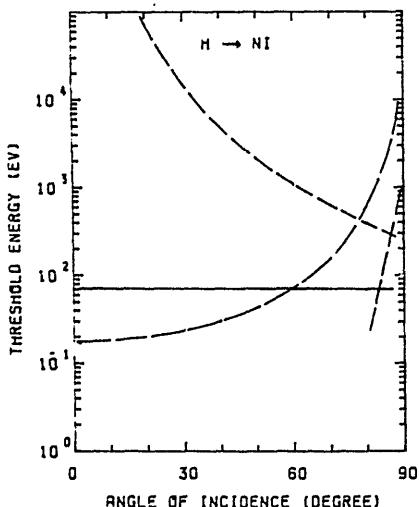


Fig. A2

The angular dependence of the threshold energies for  $H + Ni$ .

— mechanism II  
- - - direct knock-out process  
- - - - surface channeling

In Fig. A2 the threshold energies corresponding to each mechanism are plotted against the angle of incidence. Figure A2 tells us that the threshold energies corresponding to the direct knock-out process can be neglected. Finally we get

$$E_{th}^L(\theta) = \begin{cases} \frac{U_s}{\gamma} \frac{1}{1 - \gamma \cos^2(\theta/2)} & \text{for not-too-oblique incidence} \\ 26.85 \frac{A}{1 + A} E_L \left( \frac{a}{R_0} \right)^2 \frac{\cos^2 \theta}{\cos^2 \theta} & \text{for grazing angles of incidence} \end{cases} \quad (\text{A11})$$

When the incident energy is very low, sputtered atoms will be ejected before they lose the memory of the direction of the incident ion beam. This means that the velocity distribution of recoil atoms generated by incoming heavy-ions is anisotropic. Taking into account the anisotropic effect of the recoil flux, Yamamura showed that the angular dependence of the heavy-ion sputtering was proportional to  $\cos^2 \theta^{35}$ .

For grazing angles of incidence, the surface channeling will play an important role. In the case of heavy-ion sputtering, the threshold energy due to surface channeling is given by

$$E_{th}(\theta) = \frac{U_R(y_{min})}{\cos^2 \theta}, \quad (\text{A12})$$

where  $y_{min}$  is the minimum distance above which the projectile will be reflected without producing any recoil atom available for sputtering. For the amorphous solid surface the minimum distance  $y_{min}$  may be of the order of

$$y_{min} = \frac{R_0}{2} + p_{min}, \quad (\text{A13})$$

where  $p_{min}$  is the collision diameter for the Moliere potential and depends on the incident energy. Since the incident energy of present interest is very low,  $p_{min}$  is roughly given by

$$p_{min} = sa$$

where  $s$  is the solution of the following transcendental equation:

$$\epsilon = \exp(-0.3s)/s.$$

Let us consider a typical example, i.e.,  $\text{Ar}^+ - \text{Cu}$ . In this case,  $s$  is nearly equal to 15. In Fig. A3 the angular dependence of threshold energy for  $\text{Ar}^+ - \text{Cu}$  is plotted as a function of the angle of incidence. Finally, we have

$$E_{\text{th}}^H(\theta) = \begin{cases} E_{\text{th}}(0) \cos^2 \theta & \text{for not-too-oblique incidence} \\ \frac{0.3 \frac{A}{A+1} E_L \left(\frac{a}{R_0}\right)^3}{\cos^2 \theta} & \text{for grazing angles of incidence} \end{cases} \quad (\text{A14})$$

where  $E_{\text{th}}(0)$  is the threshold energy at normal incidence, and  $y_{\min}$  is set to equal to  $R_0/2 + 15a$ .

Fig. A3

The angular dependence  
of the threshold energies  
for  $\text{Ar} + \text{Cu}$ .

— mechanism I  
- - - surface channeling

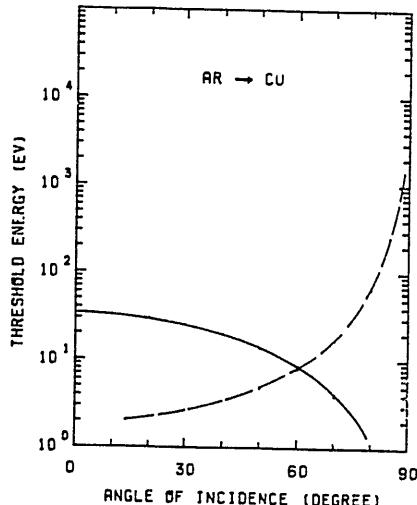


Table 1 Ion-target combinations in the present data compilation

References	Ion	Target													
		C	Al	Ti	Fe	Ni	Cu	Zr	Nb	Mo	Pd	Ag	Ta	W	Pt
Wehner (1959)	Hg			o	o				o		o	o	o	o	o
Rol et al. (1960)	Ar						o								
Marchanov et al. (1961)	Ar						o								
Almen et al. (1961)	Kr						o								
Dushikov et al. (1962)	He						o								
	N						o								
	Ne						o								
	Ar						o								
Ramer et al. (1964)	Ar						o					o			
Marchanov et al. (1965)	Ar						o		o			o			
Cheney et al. (1965)	Ar						o								
	Xe						o		o			o			
Dupp et al. (1966)	Ar						o								
Evdokimov et al. (1968)	Ne								o						
	Ar							o		o					
	Kr							o							
Ismail et al. (1968)	Hg						o								
Holmen et al. (1970)	Hg	o			o										
Summers et al. (1971)	D						o								
	He						o								
	Nb						o								
Oechsner (1973)	He						o								
	Ne						o								
	Ar	o	o		o	o	o				o	o	o	o	o
	Kr					o									
	Xe					o									
Bay et al. (1979)	H					o			o						
	D					o			o						
	He								o						
Bay et al. (1980)	H						o								
Kruger et al. (1980)	Ar					o			o		o				
Thompson et al. (1980)	P										o				
	Sb										o				
	Bi										o				
Bohdansky et al. (1982)	H				o	o	o		o		o				
	D								o						
	He				o				o		o				
Bohdansky (1983)	H						o								

Table 2 Best-fit parameters of the present empirical formula for light-ion sputtering

Energy	Ion	Target	Best-fit values		Ref.
			f	$\theta_{\text{opt}}$	
450 eV	H	Ni	1.62	74.4°	25
1 keV	H	Ni	2.34	78.3°	20
4 keV	H	Ni	2.27	82.3°	20
450 eV	H	Ni	2.19	78.7°	20
1 keV	H	Ni	2.32	82.9°	30
4 keV	H	Ni	2.62	84.2°	30
1 keV	D	Ni	1.88	80.4°	25
100 eV	He	Ni	3.20	56.3°	30
500 eV	He	Ni	3.30	66.1°	30
1 keV	He	Ni	2.50	72.1°	30
4 keV	He	Ni	2.09	79.0°	30
4 keV	He	Ni	1.52	80.5°	20
50 keV	H	Cu	1.88	82.1°	24
1.05 keV	He	Cu	1.55	66.5°	19
2 keV	H	Mo	2.40	81.8°	20
8 keV	H	Mo	2.80	82.0°	20
2 keV	D	Mo	1.98	82.0°	20
4 keV	He	Mo	2.23	77.3°	20
1 keV	H	Au	1.14	78.0°	20
4 keV	H	Au	1.53	79.5°	20
1 keV	D	Au	1.22	79.2°	20

Table 3 Best-fit parameters of the present empirical formula for heavy-ion sputtering

Energy	Ion	Target	Best-fit values		Ref.
			f	$\theta_{\text{opt}}$	
30 eV	Ar	Cu	35.4	44.2°	30
50 eV	Ar	Cu	9.33	46.1°	30
100 eV	Ar	Cu	5.25	43.6°	30
500 eV	Ar	Cu	3.35	49.6°	30
1 keV	Ar	Cu	3.07	55.7°	30
5 keV	Ar	Cu	2.66	65.7°	30
20 keV	Ar	Cu	2.19	75.0°	30
50 eV	Hg	Ni	37.1	47.5°	30
100 eV	Hg	Ni	15.0	52.5°	30
500 eV	Hg	Ni	5.01	61.2°	30
1 keV	Hg	Ni	4.02	63.3°	30
5 keV	Hg	Ni	3.56	64.7°	30
50 eV	Ni	Ni	22.8	44.2	30
100 eV	Ni	Ni	11.8	45.5°	30
500 eV	Ni	Ni	3.75	50.5°	30
1 keV	Ni	Ni	3.05	56.2°	30
5 keV	Ni	Ni	3.13	64.2°	30
10 keV	Ni	Ni	3.37	66.4°	30
200 eV	Hg	Ni	12.8	48.2	6
800 eV	Hg	Ni	8.57	51.0°	6
400 eV	Hg	Fe	15.5	57.6°	6
800 eV	Hg	Fe	9.53	60.7°	6
200 eV	Hg	Mo	26.0	53.0°	6
800 eV	Hg	Mo	26.9	50.9°	6
400 eV	Hg	Ta	15.0	62.0°	6
200 eV	Hg	W	5.87	58.3°	6
400 eV	Hg	W	10.6	52.8°	6
800 eV	Hg	W	7.64	56.1°	6

Table 3 (continued)

Energy	Ion	Target	Best-fit values		Ref.
			f	$\theta_{\text{opt}}$	
1.05 keV	Ar	Al	2.10	70.2°	19
1.05 keV	Ar	Ti	2.04	68.8°	19
1.05 keV	Ar	Ni	1.72	69.5°	19
1.05 keV	Ne	Cu	1.03	70.6°	19
1.05 keV	Ar	Cu	1.29	69.8°	19
1.05 keV	Kr	Cu	2.19	66.9°	19
550 eV	Xe	Cu	9.40	53.8°	19
1.05 keV	Xe	Cu	4.56	61.5°	19
1.55 keV	Xe	Cu	3.89	64.0°	19
2.05 keV	Xe	Cu	2.44	69.0°	19
1.05 keV	Ar	Zr	1.73	67.7°	19
1.05 keV	Ar	Pd	1.85	63.1°	19
1.05 keV	Ar	Ag	1.50	63.7°	19
1.05 keV	Ar	Ta	1.75	67.5°	19
1.05 keV	Ar	Au	1.50	59.8°	19
37 keV	Ar	Cu	1.16	71.9°	13
30 keV	Xe	Cu	1.94	75.0°	13
9.5 keV	Xe	Cu	2.53	69.5°	13
30 keV	Xe	Mo	2.58	76.7°	13
30 keV	Xe	W	1.33	78.5°	13
9.5 keV	Xe	W	1.07	76.0°	13

Table 4 Some physical constants for calculations of sputtering yields.

Table 5 through 8

The parameters for the angular dependence of light-ion sputtering.

The correspondence between Tables and projectiles are as follows:

H : Table 5

D : Table 6

T : Table 7

He : Table 8

Let us show briefly how to use these tables and suppose the angular dependence of  $4 \text{ keV } H^+ \rightarrow Ni$  is desired.

The appropriate table is Table 5. From Table 5 we have

$$f = (4.44)^{\frac{1}{2}} \times (0.94 - 0.00133 \times 58.24) = 1.82 ,$$

where figures in italics corresponds to values in Table 5.

The quantity  $\eta$  is inversely proportional to  $E^{1/4}$  and so we get

$$\eta = (\frac{1}{4})^{1/4} \times 0.1535 = 0.1085 .$$

From Eq. (12)  $\theta_{opt}$  can be calculated as follows:

$$\theta_{opt} = 90^\circ - 57.3 \times 0.1085 = 83.8^\circ .$$

Since  $\Sigma = f \cos \theta_{opt}$ , we have

$$\Sigma = 1.82 \cos 83.8^\circ = 0.197 .$$

Finally, we have the following angular dependence for  $4 \text{ keV } H^+ \rightarrow Ni$ :

$$\frac{Y(\theta)}{Y(0)} = x^{1.82} \exp[-0.197(x-1)] ,$$

where  $x = 1/\cos \theta$

Tables 9 through 18

The parameters for the angular dependence of heavy-ion sputtering.

The correspondence between Tables and projectiles are as follows:

C : Table 9	Ne : Table 10
Al : Table 11	Ar : Table 12
Fe : Table 13	Ni : Table 14
C <sub>u</sub> : Table 15	Kr : Table 16
Xe : Table 17	Hg : Table 18

Let us show briefly how to use these table for calculations of the angular dependence of heavy-ion sputtering. Then, suppose the angular dependence of 1 keV Ar<sup>+</sup> → Cu is desired. The appropriate table is Table 15. First of all, we must calculate the quantity  $\zeta$

$$\zeta = 1 - (E_{th}/E)^{\frac{1}{2}} = 1 - (20.72/1000)^{\frac{1}{2}} = 0.8561.$$

Since  $f_s = 1.71$ , the parameter  $f$  is calculated from Eq. (17),  

$$f = 1.71 \times (1 + 2.5 \times 0.1439/0.8561) = 2.43$$

The quantity  $\psi$  is inversely proportional to  $\sqrt{E}$ , which is known from Eq. (18). Then, we have

$$\psi = 0.1305/\sqrt{1000} = 0.004127 .$$

From Eq. (20) we get

$$\theta_{opt} = 90^\circ - 286 \times 0.004127^{0.45} = 65.8^\circ$$

The relation  $\Sigma = f \cos \theta_{opt}$  yields

$$\Sigma = 2.43 \cos 65.8^\circ = 0.9961.$$

In the above calculations, figures in italics are the values in Table 15. Finally, we get the following angular dependence for 1 keV Ar<sup>+</sup> → Cu;

$$\frac{Y(\theta)}{Y(0)} = x^{2.43} \exp[-0.9961(x - 1)].$$

where  $x = 1/\cos \theta$ .

Table 19 through 32

The parameters for the third Matsunami formula,  
where the correspondences between Tables and projectiles  
are as follows:

H : Table 19	D : Table 20	T : Table 21
He : Table 22	C : Table 23	Ne : Table 24
Al : Table 25	Ar : Table 26	Fe : Table 27
Ni : Table 28	Cu : Table 29	Kr : Table 30
Xe : Table 31	Hg : Table 32.	

Let us show how to use these tables for calculations of sputtering yields at normal incidence by the third Matsunami formula. Suppose the sputtering yield of 1 keV  $H^+ - Ni$  is desired. The appropriate table is Table 19. The reduced energy  $\epsilon$  for 1 keV  $Ar^+ \rightarrow Ni$  is calculated like this

$$\epsilon = 1000 / (2.799 \times 1000) = 0.3572.$$

Direct insertion of this value into Eqs. (23) and (24) yields

$$s_e(\epsilon) = 4.35 \times \sqrt{0.3572} = 2.60$$

$$s_n(\epsilon) = 0.408 .$$

Since  $P = 0.4814$  and  $E_{th} = 100.6$ , we have

$$Y = 0.4814 \times 0.408 / (1 + 0.35 \times 4.44 \times 2.60 ) \\ \times [1 - (100.6)^{\frac{1}{2}}]^{2.8} = 1.33 \times 10^{-2} (\text{atoms/ion}),$$

where  $U_s = 4.44$  eV is in Table 4, and in the above calculations figures in italics corresponds to those in the present tables.

TABLE 4 PHYSICAL CONSTANTS FOR THE THIRD HATSUMAMI FORMULA AND THE PRESENT EMPIRICAL FORMULA

1.008		4.003	
H 1	He 2.		
1.089 0	1.179 0		
2.66 1	3.34 1		
Li 3	Be 4	9.012	Mass Number
6.941			Symbol
1.43 1.43	1.85 3.32		Atomic Number
1.53 1.43	1.85 2.01		Sublimation Energy (ev)
1.53 2.66	2.15 2.01		Density (g/cm <sup>3</sup> )
2.15 2.66	2.01 1		Q value of the 3rd
2.15 2.01	2.01 1		Average Lattice Constant R <sub>0</sub> (Å)
2.15 2.01	2.01 1		of Random Target
25	24.3		Hatsumami Empirical Formula
Na 11	Mg 12	44.95	47.9
1.11 1.11	1.74 1.51	50.94	52
1.97 1.41	3.41 2.86	54.93	52
1.54 1.54	1.84 2.99	58.95	56
1.54 1.52	1.84 2.93	62	Cr 24
1.54 1.52	1.84 2.93	66	Mn 25
1.54 1.52	1.84 2.93	70	Fe 26
1.54 1.52	1.84 2.93	74	Co 27
1.54 1.52	1.84 2.93	78	Ni 28
1.54 1.52	1.84 2.93	82	Cu 29
1.54 1.52	1.84 2.93	86	Zn 30
1.54 1.52	1.84 2.93	90	Ga 31
1.54 1.52	1.84 2.93	94	Ge 32
1.54 1.52	1.84 2.93	98	As 33
1.54 1.52	1.84 2.93	102	Se 34
1.54 1.52	1.84 2.93	106	Br 35
1.54 1.52	1.84 2.93	110	Ar 36
1.54 1.52	1.84 2.93	114	
1.54 1.52	1.84 2.93	118	
1.54 1.52	1.84 2.93	122	
1.54 1.52	1.84 2.93	126	
1.54 1.52	1.84 2.93	130	
1.54 1.52	1.84 2.93	134	
1.54 1.52	1.84 2.93	138	
1.54 1.52	1.84 2.93	142	
1.54 1.52	1.84 2.93	146	
1.54 1.52	1.84 2.93	150	
1.54 1.52	1.84 2.93	154	
1.54 1.52	1.84 2.93	158	
1.54 1.52	1.84 2.93	162	
1.54 1.52	1.84 2.93	166	
1.54 1.52	1.84 2.93	170	
1.54 1.52	1.84 2.93	174	
1.54 1.52	1.84 2.93	178	
1.54 1.52	1.84 2.93	182	
1.54 1.52	1.84 2.93	186	
1.54 1.52	1.84 2.93	190	
1.54 1.52	1.84 2.93	194	
1.54 1.52	1.84 2.93	198	
1.54 1.52	1.84 2.93	202	
1.54 1.52	1.84 2.93	206	
1.54 1.52	1.84 2.93	210	
1.54 1.52	1.84 2.93	214	
1.54 1.52	1.84 2.93	218	
1.54 1.52	1.84 2.93	222	
1.54 1.52	1.84 2.93	226	
1.54 1.52	1.84 2.93	230	
1.54 1.52	1.84 2.93	234	
1.54 1.52	1.84 2.93	238	

TABLE 5  
PARAMETERS FOR ANGULAR DEPENDENCE OF LIGHT-ION SPUTTERING YIELD  
PROJECTILE: H, He, Be, C, N, F, Ne, Ar, Kr, Xe  
Z - NUMBER: 1, 2, 4, 6, 12, 14, 16, 18, 36, 40, 42, 54, 72, 84, 92  
MASS-NUMBER: 1, 2, 3, 4, 6, 12, 14, 16, 18, 20, 32, 36, 40, 42, 54, 72, 84, 92, 108, 128, 140, 160, 180, 208, 224, 240, 260, 280, 300, 320, 340, 360, 380, 400, 420, 440, 460, 480, 500, 520, 540, 560, 580, 600, 620, 640, 660, 680, 700, 720, 740, 760, 780, 800, 820, 840, 860, 880, 900, 920, 940, 960, 980, 1000

•0B69		H 1		He 2		•1238	
1	0	1	0	3.971	0	3.971	0
0	0	0	0	0	0	0	0
•1B53	•2B55	•2555	•2555	•4146	•4978	•5845	•6725
L1 3	Be 4	Symbol	Atomic Number	B 5	C 6	N 7	F 9
6.886 1.63	B.94 3.32	Mass Ratio (M2/M1)	Sublimation Energy (eV)	10.72 5.77	11.91 7.37	13.9 4.92	18.85 .84
.1178 1.19	.1438 1.69	n for 1 kev Ion	f for Light-Ion Sputtering	.1321 2.22	.124 2.51	.1022 2.04	.1807 .84
•B606	•9597	1.7071	1.8231	1.9367	2.0542	2.1754	2.2958
Na 11	Mg 12	Sc 21	Ti 22	V 23	Cr 24	Mn 25	Fe 26
22.82 1.11	24.11 1.51	39.76 1.94	44.59 5.9	47.52 4.85	50.54 5.31	51.59 4.1	55.49 2.92
.1282 .96	.1431 1.12	.1161 1.74	.1235 1.93	.1308 2.01	.1483 1.76	.1601 1.48	.1489 1.79
K 19	Ca 20	•4.1441	•4.2855	•4.4294	•4.5758	•4.7195	•4.8666
84.79 85	86.92 1.72	88.2 4.37	90.5 6.25	92.17 7.57	95.18 6.82	98.13 6.85	102.1 5.75
.1141 .76	.1135 1.08	.1075 1.72	.111 2.05	.1247 2.25	.1247 2.12	.1262 2.12	.1307 2.09
4.0034	4.0034	4.1441	4.2855	4.4294	4.5758	4.7195	4.8666
Rb 37	Sr 39	Y 39	Zr 40	Nb 41	Hf 42	Tc 43	Ru 44
84.79 85	86.92 1.72	88.2 4.37	90.5 6.25	92.17 7.57	95.18 6.82	98.13 6.85	102.1 5.75
.1141 .76	.1135 1.08	.1075 1.72	.111 2.05	.1247 2.25	.1247 2.12	.1262 2.12	.1307 2.09
6.6985	6.8869	7.0174	9.5229	9.6965	9.8707	10.446	10.496
Cs 55	Ba 56	La 57	Hf 72	Ta 73	W 74	Re 75	Ds 76
131.8 .8	136.2 1.9	137.8 4.47	177 6.44	179.5 8.1	182.3 8.9	184.7 8.03	188.7 8.17
.1102 .68	.1075 1.05	.1048 1.6	.1152 1.79	.1172 2.05	.1201 2.08	.1259 1.97	.1278 1.97
12.203	12.387	12.575	7.1769	7.3416	7.5041	7.6685	7.8321
Fr 87	Ra 88	Ac 89	Ce 58	Pr 59	Nd 60	Pm 61	Sm 62
221.2 0	224.2 1.66	225.2 4.25	159 4.32	139.8 3.7	143.1 3.4	145.8 0	149.1 2.14
0	1.092 .93	.1093 1.32	.109 1.57	.1138 1.45	.1166 1.38	0	156 4.14
12.758	12.758	12.758	12.758	12.758	12.758	12.758	12.758
Th 90	Pa 91	U 92	220.2 6.2	229.2 0	236.1 5.55	242.5 1.77	245.2 0
0	.1065 1.58	0	0	0	0	0	0

TABLE 6 PARAMETERS FOR ANGULAR DEPENDENCE OF LIGHT-ION SPUTTERING YIELD  
PROJECTILE . . . . .

TABLE 7  
PARAMETERS FOR ANGULAR DEPENDENCE OF LIGHT-ION SPUTTERING YIELD  
PROJECTILE .....  
Z - NUMBER ..... 1  
·MASS-NUMBER ..... 3.016

TABLE 8  
PARAMETERS FOR ANGULAR DEPENDENCE OF LIGHT-ION SPUTTERING YIELD

TABLE 9  
PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD  
PROJECTILE ..... C  
Z - NUMBER ..... 6  
MAY3-NUMBER ..... 12.01

O		H 1		He 2		Ne 10	
L1	3	Be 4	O 5	C 6	N 7	F 8	Ar 18
16.76	30.59	30.59	30.59	50.26	62.62	36.38	5.003
L1 3	Be 4	Symbol (H2/M1)	Atomic Number	B 5	C 6	N 7	F 9
.578 1.65	.75 3.32	.75 3.32	Threshold Energy (eV)	.9 5.77	1 7.37	1.167 4.92	1.582 .84
.564 1.85	.0947 1.85	.0947 1.85	Sublimation Energy (eV)	.1013 1.83	.0978 1.81	1.332 2.6	1.582 1.71
6.002	7.984	for 1 eV	Sigmund +	17.29	25.34	16.9	13.95
Na 11	Mg 12	Symbol (H2/M1)	Mass Ratio (H2/M1)	A1 13	Si 14	P 15	C1 17
1.915 1.11	2.023 1.51	30.59	30.59	2.246 3.39	2.358 4.63	2.579 3.43	2.952 1.4
.0502 1.64	.0658 1.63	.0947 1.85	for 1 eV	.0783 1.59	.0719 1.58	.0609 1.54	.0639 1.53
4.457	8.811	18.71	23.39	25.77	19.75	14.34	14.61
K 19	Ca 20	Tl 22	V 23	Cr 24	Mn 25	Fe 26	Co 27
3.255 1.93	3.337 1.84	3.743 3.9	3.988 4.85	4.241 5.31	4.133 4.1	4.574 2.92	4.888 4.44
.0378 1.44	.0498 1.45	.0658 1.36	.0884 1.34	.0955 1.31	.0944 1.29	.0963 1.28	.0963 1.25
4.749	9.706	24.61	35.87	43.79	40.02	40.76	40.5
Rb 37	Sr 38	V 39	Zr 40	Nb 41	Mo 42	Tc 43	Ru 44
7.117 1.05	7.296 1.72	7.403 4.37	7.595 6.25	7.736 7.37	7.988 6.82	8.236 6.95	8.41
.0344 1.04	.0442 1.03	.0573 1.02	.0685 1.01	.0772 1	.0837 .98	.0875 .96	.0889 .95
5.35	13.45	31.82	53.61	68.06	75.58	68.79	71
Cs 55	Ba 56	La 57	Hf 72	Ta 73	W 74	Re 75	Os 76
11.07 8	11.43 1.9	11.57 4.47	14.85 6.44	15.06 8.61	15.3 8.9	15.5 8.03	16.4 8.17
.0503 .75	.0405 .73	.0534 .72	.0679 .48	.0758 .46	.0812 .44	.0836 .43	.0861 .4
0	16.28	41.81		30.91	26.36	24.74	0
Fr 87	Ra 88	Ac 89	Ce 58	Pr 59	Nd 60	Sm 61	Eu 62
18.57 0	18.92 1.66	18.9 4.25	11.67 4.32	11.73 3.7	12.01 3.4	12.07 0	12.51 2.14
0 .21	.0357 1.19	.0352 1.18	.0356 .71	.0355 .7	.0357 .68	.0357 .68	.0354 .45

TABLE 10  
PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD

O	H 1 .05 0 .0414 1.7	22.52	39.3	Symbol (H2/M1)	39.3	Threshold Energy (eV)	39.3	Atomic Number	4	Sublimation Energy (eV)	.447 3.32 .0994 1.64	for 1 eV
Li 3	Be 4											
-3.44 1.63 .0358 1.82	.447 3.32 .0994 1.64											
B 37	10.88											
Na 11	Mg 12											
1.14 1.11 1.204 1.51 .0357 1.79	.0735 1.78											
K 19	Ca 20	Sc 21	19.94	24.35	26.27	20.2	14.24	20.82	21.21	21.46	16.47	15.45
1.937 .933 1.956 1.86 .03572 1.85	.07356 1.85	V 23	11 22	2.574 4.85 2.524 5.34 .1021 1.55	2.577 4.1 2.722 2.92 .1119 1.51	Cr 24	25	2.92	4.39	3.149 3.49 3.126 1.45	3.24 1.17	3.455 2.81 3.095 1.44
Rb 37	Sr 38	Y 39	21.32	30.42	37.21	35.72	34.09	35.69	28.87	19.69	14.98	5.75B
4.235 .85 4.352 1.72 .0406 1.32	4.406 4.37 4.052 1.3 .0579 1.3	Zr 40	Nb 41	4.52 6.25 4.604 7.57 .0916 1.28	4.52 6.82 4.754 6.82 .0994 1.27	Tc 43	Ru 44	5.005 6.74 5.099 5.75 .1038 1.25	5.273 3.89 5.342 2.95 .1038 1.25	Pd 46	Ag 47	Cd 4B
Ca 55	Ba 56	La 57	24.65	39.64	50.2	55.6	50.5	51.94	44.36	37.61	24.66	4.379
6.586 .8 6.586 1.9 .0354 1.08	6.804 1.9 6.804 1.08	Hf 72	Ta 73	W 74	Re 75	Ds 76	Ir 77	Pt 78	Au 79	Hg 80	Tl 81	Pb 82
Ff 87	Ra 88	Ac 89	11.6	29.77	23.9	20.51	19.03	0	12.18	10.63	24.02	23.41
11.05 0 0 .75	11.2 1.74 0.0448 1.74	11.25 4.25 11.25 4.25	29.77	Ce 5B	Pr 59	Nd 60	Pm 61	Sm 62	Eu 63	Dy 64	Tb 65	Ho 67
O				6.943 4.32 6.943 4.32	6.902 3.7 6.902 3.7	7.146 3.4 7.185 0	7.146 3.4 7.185 0	7.448 2.4 7.527 1.86	7.79 4.14 8.053 3.04	8.171 3.14 8.285 3.29	8.41 0.8 8.573 2.42	Lu 71
				.06668 1.05 .06668 1.05	.06668 1.05 .06668 1.05	1.04 1.04	1.04 1.04	1.02 1.02	.0593 1.01 .0593 1.01	.05666 9.99 .0712 9.96	.0712 9.99 .0712 9.96	
												27.01
				43.98	0							39.96
				Th 90	Pa 91							U 92
				11.76 6.2 .06776 .72	11.45 0 .06852 .7							11.79 5.35 .06776 .72

**TABLE 11** PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD  
 PROJECTILE ..... Al  
 Z - NUMBER ..... 13  
 MASS-NUMBER ..... 26.98

**TABLE 12** PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD  
PROJECTILE ..... Ar  
Z - NUMBER ..... 18  
MASS-NUMBER ..... 39, 94

TABLE 13 PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD  
 PROJECTILE ..... Fe  
 Z - NUMBER ..... 26  
 MASS-NUMBER ..... 55.85

O		He 2	
H 1	.018 0	.072 " "	.0355 1.7
O	56.27	68.51	U
L 1 3	Be 4	B 5	129.8
.124 1.63	.161 3.32	C 6	150.9
.0557 1.76	.1016 1.77	N 7	88.3
		D 8	41.93
		F 9	11.91
		G 10	.272
		Ne 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	
		D 8	
		F 9	
		G 10	
		B 5	
		C 6	
		N 7	

PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD	
PROJECTILE	NI
Z NUMBER	28
MASS NUMBER	58.71

TABLE 15 PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD  
 PROJECTILE: Cu  
 Z - NUMBER: 29  
 MASS-NUMBER: 63-55

O		He 2		Ne 10	
H 1	.016 0	O	.065 0	O	.298
Li 3	100.4	B 5	C 6	N 7	F 9
.109 1.65	Be 4	.17 5.77	.189 7.37	.22 4.92	.259 .84
.10934 1.72	.142 5.32	.1121 1.78	.1115 1.8	.0842 1.81	.0835 1.82
15.06	19.73	41.4	55.16	31.45	14.65
Na 11	Mg 12	A1 13	S1 14	P 15	C1 17
.362 1.11	.382 1.51	.425 3.39	.442 4.63	.504 2.85	.556 1.4
.0322 1.82	.0842 1.83	.1015 1.84	.0845 1.84	.0809 1.85	.0833 1.85
K 19	18.17	9.289	36.73	44.62	47.85
Ca 20	Sc 21	Tl 22	V 23	Cr 24	Mn 25
.631 1.84	.754 4.85	.802 5.31	.818 4.1	.864 2.92	.927 4.39
.0596 1.85	.1111 1.85	.1263 1.84	.1374 1.84	.1347 1.83	.1461 1.82
Rb 37	Sr 38	Y 39	Zr 40	Nb 41	Mo 42
1.345 1.85	1.379 1.72	1.399 4.37	1.402 3.9	1.433 6.25	1.556 6.85
.0685 1.75	.0891 1.74	.1068 6.25	.1068 6.25	.11315 1.73	.11377 1.72
Cs 55	Ba 56	La 57	Hf 72	Ta 73	W 74
2.091 1.8	2.161 1.9	2.169 4.47	2.007 6.44	2.867 8.1	2.592 8.9
.0693 1.62	.0653 1.6	.0897 1.6	.1151 1.5	.1286 1.49	.1318 1.49
O	7.949	20.35	22.16	18.95	17.29
Fr 87	Ra 88	Ac 89	Ce 58	Pr 59	Nd 60
3.509 0	3.556 1.66	3.572 4.25	2.205 4.32	2.217 3.7	2.249 3.4
0 1.4	.0637 1.38	.0904 1.38	.0915 1.6	.0916 1.6	.0922 1.59

Threshold Energy (eV)  
 Atomic Number  
 Sublimation Energy (eV)

Symbol  
 Mass Ratio (M2/M1)  
 1.142 3.32  
 1.1015 1.76  
 for 1 eV

Sigmoid +

146.3	169.4	98.55	46.52	13.1	*298
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
A1 13	S1 14	P 15	S 16	C1 17	Ar 18
.425 3.39	.442 4.63	.487 3.43	.504 2.85	.556 1.4	.638 1.08
.1015 1.84	.0845 1.84	.0809 1.85	.0839 1.85	.0833 1.85	.0833 1.85
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
A1 13	S1 14	P 15	S 16	C1 17	Ar 18
.425 3.39	.442 4.63	.487 3.43	.504 2.85	.556 1.4	.638 1.08
.1015 1.84	.0845 1.84	.0809 1.85	.0839 1.85	.0833 1.85	.0833 1.85
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.82	.0833 1.82
41.4	55.16	38.58	31.45	14.65	.791
B 5	C 6	N 7	O 8	F 9	Ne 10
.17 5.77	.189 7.37	.22 4.92	.252 2.6	.259 .84	.318 .02
.1121 1.78	.1115 1.8	.0733 1.8	.0842 1.81	.0835 1.	

**TABLE 16** PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD  
 PROJECTILE ..... Kr  
 Z - NUMBER ..... 36  
 MASS-NUMBER, ..... 83.8

O	H 1	135.1	Symbol	135.1	Threshold Energy (eV)
H	1	Be 4	Atomic Number	Be 4	Sublimation Energy (eV)
.012 0	.0373 1.7	Mass Ratio (M2/M1)	.108 3.32	.1006 1.72	for 1 eV
.083 1.63	.098 1.63		.108 3.32	.1006 1.72	Sigmund &
.0548 1.77	.0659 1.81		.1006 1.72	.0653 1.82	
1B.52	24.12	41.64	50.15	53.33	40.79
Na 11	Mg 12	Ca 20	Sc 21	V 23	Cr 24
.274 1.11	.29 1.51	.466 1.84	.572 4.95	.608 5.31	.621 4.1
.0659 1.81	.0713 1.85	.0555 1.85	.0999 1.85	.1299 1.85	.1141 1.85
K 19	41.64	50.15	53.33	40.79	28.36
466 .95	.478 1.84	.572 3.9	.608 4.95	.621 4.1	.646 4.28
.0555 1.85	.0713 1.85	.0999 1.85	.1299 1.85	.1141 1.85	.1048 1.85
10.73	20.92	41.64	50.15	53.33	40.79
Rb 37	35.12	41.64	50.15	53.42	41.64
1.02 .85	1.046 4.37	2r 40	Nb 41	Tc 43	Re 45
.0352 1.81	.0713 1.88	.1046 4.37	.1089 6.25	.1109 7.57	.1145 6.82
7.087	14.01	41.64	50.15	53.42	41.64
Rb 37	35.12	49.07	58.47	51.23	50.16
1.02 .85	1.046 4.37	2r 40	Nb 41	Mo 42	Tc 43
.0352 1.81	.0713 1.88	.1046 4.37	.1089 6.25	.1109 7.57	.1145 6.82
4.758	11.09	25.93	33.42	41.64	45.73
Ca 35	Ba 56	La 57	Hf 72	Ta 73	W 74
1.586 .8	1.638 1.9	1.658 4.47	2.159 6.44	2.193 8.9	2.222 6.03
.052 1.71	.0697 1.7	.0921 1.7	.1215 1.61	.1258 1.6	.1305 1.59
0	8.109	20.75	24.94	21.3	19.34
Ff 87	Ra 88	Ac 89	Ce 58	Pr 59	Nd 60
2.661 0	2.697 1.02	2.709 4.25	2.772 4.32	1.681 3.7	1.721 3.4
1.53	.0678 1.02	.078 1.52	.0962 1.69	.0923 1.69	.097 1.68
30.16	0	26.9	Th 90	Pa 91	U 92
2.768 6.2	.2757 0	.284 5.35	.1024 1.51	.1175 1.51	.1253 1.49

TABLE 17  
PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD  
PROJECTILE .....  $X_e$   
 $Z$  - NUMBER ..... 54  
MASS-NUMBER ..... 131.3

0		He 2	
H 1	.008 O	.03 O	.0344 1.7
L <sub>1</sub> 3	Be 4	C 6	N 8
.055 1.63	.069 3.32	.082 7.77	F 9
.0532 1.7	.0984 1.7	.1099 1.7	Ne 10
143.2	216.8	308	198.9
L <sub>1</sub> 3	Be 4	B 5	91.58
.055 1.63	.069 3.32	C 6	24.9
.0532 1.7	.0984 1.7	N 7	*559
27.39	35.38	.091 7.37	O 8
Na 11	Hg 12	.1102 1.7	F 9
.175 1.11	.185 1.51	.107 4.92	Ne 10
.045 1.78	.0864 1.8	.122 2.6	.145 .84
K 19	Ca 20	.073 1.72	.0944 1.76
.298 .95	.305 1.84	72.25	.0849 1.77
.0551 1.82	.0737 1.82	95.24	.0849 1.81
B 281	16.58	65.44	23.66
Rb 37	Sr 38	55.03	1.232
.651 .85	.667 1.72	52.35	Ar 18
.0585 1.85	.677 4.37	55.99	Kr 36
6.719	15.47	Cr 24	Xe 54
C <sub>1</sub> 55	Ba 56	Hn 25	1.359
1.012 .8	1.046 1.9	Fe 26	1.360
.0562 1.81	.0997 1.8	Ni 28	1.361
0	9.439	Co 27	1.362
Fr 87	Ra 88	51.81	1.363
1.688 0	1.721 1.46	52.52	1.364
0	.0746 1.68	52.52	1.365
14.56	28.25	52.35	1.366
K 19	Ca 20	55.99	1.367
.298 .95	.305 1.84	52.2	1.368
.0551 1.82	.0737 1.82	52.2	1.369
B 281	16.58	65.44	1.370
Rb 37	Sr 38	55.03	1.371
.651 .85	.667 1.72	63.03	1.372
.0585 1.85	.677 4.37	63.45	1.373
6.719	15.47	62.32	1.374
C <sub>1</sub> 55	Ba 56	52.71	1.375
1.012 .8	1.046 1.9	57.28	1.376
.0562 1.81	.0997 1.8	51.23	1.377
0	9.439	51.23	1.378
Fr 87	Ra 88	57.28	1.379
1.688 0	1.721 1.46	52.48	1.380
0	.0746 1.68	52.48	1.381
143.2	216.8	52.48	1.382
L <sub>1</sub> 3	Be 4	52.48	1.383
.055 1.63	.069 3.32	52.48	1.384
.0532 1.7	.0984 1.7	52.48	1.385
27.39	35.38	52.48	1.386
Na 11	Hg 12	52.48	1.387
.175 1.11	.185 1.51	52.48	1.388
.045 1.78	.0864 1.8	52.48	1.389
K 19	Ca 20	52.48	1.390
.298 .95	.305 1.84	52.48	1.391
.0551 1.82	.0737 1.82	52.48	1.392
B 281	16.58	52.48	1.393
Rb 37	Sr 38	52.48	1.394
.651 .85	.667 1.72	52.48	1.395
.0585 1.85	.677 4.37	52.48	1.396
6.719	15.47	52.48	1.397
C <sub>1</sub> 55	Ba 56	52.48	1.398
1.012 .8	1.046 1.9	52.48	1.399
.0562 1.81	.0997 1.8	52.48	1.400
0	9.439	24.11	1.401
Fr 87	Ra 88	34.53	1.402
1.688 0	1.721 1.46	29.42	1.403
0	.0746 1.68	29.42	1.404
143.2	216.8	26.48	1.405
L <sub>1</sub> 3	Be 4	34.53	1.406
.055 1.63	.069 3.32	29.42	1.407
.0532 1.7	.0984 1.7	34.53	1.408
27.39	35.38	34.53	1.409
Na 11	Hg 12	34.53	1.410
.175 1.11	.185 1.51	34.53	1.411
.045 1.78	.0864 1.8	34.53	1.412
K 19	Ca 20	34.53	1.413
.298 .95	.305 1.84	34.53	1.414
.0551 1.82	.0737 1.82	34.53	1.415
B 281	16.58	34.53	1.416
Rb 37	Sr 38	34.53	1.417
.651 .85	.667 1.72	34.53	1.418
.0585 1.85	.677 4.37	34.53	1.419
6.719	15.47	34.53	1.420
C <sub>1</sub> 55	Ba 56	34.53	1.421
1.012 .8	1.046 1.9	34.53	1.422
.0562 1.81	.0997 1.8	34.53	1.423
0	9.439	24.11	1.424
Fr 87	Ra 88	34.53	1.425
1.688 0	1.721 1.46	34.53	1.426
0	.0746 1.68	34.53	1.427
143.2	216.8	34.53	1.428
L <sub>1</sub> 3	Be 4	34.53	1.429
.055 1.63	.069 3.32	34.53	1.430
.0532 1.7	.0984 1.7	34.53	1.431
27.39	35.38	34.53	1.432
Na 11	Hg 12	34.53	1.433
.175 1.11	.185 1.51	34.53	1.434
.045 1.78	.0864 1.8	34.53	1.435
K 19	Ca 20	34.53	1.436
.298 .95	.305 1.84	34.53	1.437
.0551 1.82	.0737 1.82	34.53	1.438
B 281	16.58	34.53	1.439
Rb 37	Sr 38	34.53	1.440
.651 .85	.667 1.72	34.53	1.441
.0585 1.85	.677 4.37	34.53	1.442
6.719	15.47	34.53	1.443
C <sub>1</sub> 55	Ba 56	34.53	1.444
1.012 .8	1.046 1.9	34.53	1.445
.0562 1.81	.0997 1.8	34.53	1.446
0	9.439	24.11	1.447
Fr 87	Ra 88	34.53	1.448
1.688 0	1.721 1.46	34.53	1.449
0	.0746 1.68	34.53	1.450
143.2	216.8	34.53	1.451
L <sub>1</sub> 3	Be 4	34.53	1.452
.055 1.63	.069 3.32	34.53	1.453
.0532 1.7	.0984 1.7	34.53	1.454
27.39	35.38	34.53	1.455
Na 11	Hg 12	34.53	1.456
.175 1.11	.185 1.51	34.53	1.457
.045 1.78	.0864 1.8	34.53	1.458
K 19	Ca 20	34.53	1.459
.298 .95	.305 1.84	34.53	1.460
.0551 1.82	.0737 1.82	34.53	1.461
B 281	16.58	34.53	1.462
Rb 37	Sr 38	34.53	1.463
.651 .85	.667 1.72	34.53	1.464
.0585 1.85	.677 4.37	34.53	1.465
6.719	15.47	34.53	1.466
C <sub>1</sub> 55	Ba 56	34.53	1.467
1.012 .8	1.046 1.9	34.53	1.468
.0562 1.81	.0997 1.8	34.53	1.469
0	9.439	24.11	1.470
Fr 87	Ra 88	34.53	1.471
1.688 0	1.721 1.46	34.53	1.472
0	.0746 1.68	34.53	1.473
143.2	216.8	34.53	1.474
L <sub>1</sub> 3	Be 4	34.53	1.475
.055 1.63	.069 3.32	34.53	1.476
.0532 1.7	.0984 1.7	34.53	1.477
27.39	35.38	34.53	1.478
Na 11	Hg 12	34.53	1.479
.175 1.11	.185 1.51	34.53	1.480
.045 1.78	.0864 1.8	34.53	1.481
K 19	Ca 20	34.53	1.482
.298 .95	.305 1.84	34.53	1.483
.0551 1.82	.0737 1.82	34.53	1.484
B 281	16.58	34.53	1.485
Rb 37	Sr 38	34.53	1.486
.651 .85	.667 1.72	34.53	1.487
.0585 1.85	.677 4.37	34.53	1.488
6.719	15.47	34.53	1.489
C <sub>1</sub> 55	Ba 56	34.53	1.490
1.012 .8	1.046 1.9	34.53	1.491
.0562 1.81	.0997 1.8	34.53	1.492
0	9.439	24.11	1.493
Fr 87	Ra 88	34.53	1.494
1.688 0	1.721 1.46	34.53	1.495
0	.0746 1.68	34.53	1.496
143.2	216.8	34.53	1.497
L <sub>1</sub> 3	Be 4	34.53	1.498
.055 1.63	.069 3.32	34.53	1.499
.0532 1.7	.0984 1.7	34.53	1.500
27.39	35.38	34.53	1.501
Na 11	Hg 12	34.53	1.502
.175 1.11	.185 1.51	34.53	1.503
.045 1.78	.0864 1.8	34.53	1.504
K 19	Ca 20	34.53	1.505
.298 .95	.305 1.84	34.53	1.506
.0551 1.82	.0737 1.82	34.53	1.507
B 281	16.58	34.53	1.508
Rb 37	Sr 38	34.53	1.509
.651 .85	.667 1.72	34.53	1.510
.0585 1.85	.677 4.37	34.53	1.511
6.719	15.47	34.53	1.512
C <sub>1</sub> 55	Ba 56	34.53	1.513
1.012 .8	1.046 1.9	34.53	1.514
.0562 1.81	.0997 1.8	34.53	1.515
0	9.439	24.11	1.516
Fr 87	Ra 88	34.53	1.517
1.688 0	1.721 1.46	34.53	1.518
0	.0746 1.68	34.53	1.519
143.2	216.8	34.53	1.520
L <sub>1</sub> 3	Be 4	34.53	1.521
.055 1.63	.069 3.32	34.53	1.522
.0532 1.7	.0984 1.7	34.53	1.523
27.39	35.38	34.53	1.524
Na 11	Hg 12	34.53	1.525
.175 1.11	.185 1.51	34.53	1.526
.045 1.78	.0864 1.8	34.53	1.527
K 19	Ca 20	34.53	1.528
.298 .95	.305 1.84	34.53	1.529
.0551 1.82	.0737 1.82	34.53	1.530
B 281	16.58	34.53	1.531
Rb 37	Sr 38	34.53	1.532
.651 .85	.667 1.72	34.53	1.533
.0585 1.85	.677 4.37	34.53	1.534
6.719	15.47	34.53	1.535
C <sub>1</sub> 55	Ba 56	34.53	1.536
1.012 .8	1.046 1.9	34.53	1.537
.0562 1.81	.0997 1.8	34.53	1.538
0	9.439	24.11	1.539
Fr 87	Ra 88	34.53	1.540
1.688 0	1.721 1.46	34.53	1.541
0	.0746 1.68	34.53	1.542
143.2	216.8	34.53	1.543
L <sub>1</sub> 3	Be 4	34.53	1.544
.055 1.63	.069 3.32	34.53	1.545
.0532 1.7	.0984 1.7	34.53	1.546
27.39	35.38	34.53	1.547
Na 11	Hg 12	34.53	1.548
.175 1.11	.185 1.51	34.53	1.549
.045 1.78	.0864 1.8	34.53	1.550
K 19	Ca 20	34.53	1.551
.298 .95	.305 1.84	34.53	1.552
.0551 1.82	.0737 1.82	34.53	1.553
B 281	16.58	34.53	1.554
Rb 37	Sr 38	34.53	1.555
.651 .85	.667 1.72	34.53	1.556
.0585 1.85	.677 4.37	34.53	1.557
6.719	15.47	34.53	1.558
C <sub>1</sub> 55	Ba 56	34.53	1.559
1.012 .8	1.046 1.9	34.53	1.560
.0562 1.81	.0997 1.8	34.53	1.561
0	9.439	24.11	1.562
Fr 87	Ra 88	34.53	1.563
1.688 0	1.721 1.46	34.53	1.564
0	.0746 1.68	34.53	1.565
143.2	216.8	34.53	1.566
L <sub>1</sub> 3	Be 4	34.53	1.567
.055 1.63	.069 3.32	34.53	1.568
.0532 1.7	.0984 1.7	34.53	1.569
27.39	35.38	34.53	1.57

TABLE 18 PARAMETERS FOR ANGULAR DEPENDENCE OF HEAVY-ION SPUTTERING YIELD  
 Z - NUMBER ..... Hg  
 BO  
 MASS-NUMBER..... 200.5

O		He 2 .		He 1 .		He 0 .	
H 1	.005 0	Li 3	B 4	N 2	O 3	F 4	Ne 10
.035 1.63	.045 3.32	.045 3.32	.045 3.32	.067 1.7	.067 1.7	.067 1.7	.067 1.7
.0513 1.7	.0513 1.7	.0513 1.7	.0513 1.7	.0513 1.7	.0513 1.7	.0513 1.7	.0513 1.7
235.3	352.1	352.1	352.1	495.6	581.2	314.9	38.51
Li 3	B 4	B 4	B 4	B 5	C 6	N 7	He 9
.035 1.63	.045 3.32	.045 3.32	.045 3.32	.054 5.77	.06 7.37	.07 4.92	.095 1.84
.0513 1.7	.0513 1.7	.0513 1.7	.0513 1.7	.071 1.7	.079 1.7	.071 1.7	.094 1.7
41.61	53.48	53.48	53.48	108	141.7	95.37	34.23
Na 11	Mg 12	Mg 12	Mg 12	Al 13	S 14	P 15	Ar 18
.115 1.11	.121 1.51	.121 1.51	.121 1.51	.135 3.59	.14 4.63	.154 3.45	.177 1.4
.0642 1.76	.0642 1.76	.0642 1.76	.0642 1.76	.1048 1.76	.0981 1.76	.0846 1.77	.0682 1.78
20.78	40.19	76.99	90.67	94.3	71.59	69.39	19.73
K 19	Ca 20	Sc 21	Tl 22	V 23	Cr 24	Mn 25	Fe 26
.195 1.73	.224 1.84	.224 1.84	.239 1.84	.254 1.84	.259 1.84	.274 2.92	.293 4.44
.0359 1.8	.0749 1.8	.0749 1.8	.1001 1.81	.1379 1.81	.1508 1.81	.1508 1.81	.1651 1.82
10.35	20.63	51.75	73.16	87.06	77.52	76.55	19.73
Rb 37	Sr 38	Y 39	Zr 40	Nb 41	Tc 43	Re 45	Fe 26
.426 1.85	.437 1.72	.443 4.37	.455 6.25	.455 6.25	.453 7.57	.453 6.74	.453 2.95
.064 1.84	.079 1.84	.079 1.84	.1031 1.84	.1237 1.85	.1406 1.85	.1406 1.85	.1657 1.85
7.736	18.13	42.45	56.27	70.51	77.16	69.39	19.73
Ca 55	Ba 56	La 57	Hf 52	Ta 73	W 74	Re 75	Fe 26
.665 1.8	.685 1.9	.693 4.47	.69 6.14	.902 8.1	.917 8.9	.929 8.03	.939 6.94
.0595 1.85	.0799 1.85	.0799 1.85	.1058 1.85	.1594 1.83	.1714 1.82	.1771 1.82	.1823 1.82
O	12.64	32.23	40.68	54.94	31.82	0	19.73
Fr 87	Ra 88	Ac 89	Ce 58	Pr 59	Nu 60	Fm 61	Sn 62
1.112 0	1.127 1.66	1.132 4.25	.699 4.32	.703 3.7	.719 3.4	.723 0	.723 0.85
0 1.79	.0806 1.79	.1175 1.79	.1106 1.85	.1111 1.85	.1119 1.85	.1142 1.85	.1147 1.85
46.16		0	40.45	46.16		46.16	46.16
Th 90		Pa 91	U 92	Th 90		Pa 91	U 92
1.157 6.2		1.152 0	1.167 5.55	1.157 6.2		1.146 1.79	1.149 1.78
.1224 1.79		.1406 1.79	.1549 1.78	.1224 1.79		.1221 1.83	.124 1.83

**TABLE 19** PARAMETERS OF THE THIRD MOTSUNAMI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
2 - NUMBER.....  
MASS-NUMBER.....  
1.008

**TABLE 20** PARAMETERS OF THE THIRD MATSUBANI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
 PROJECTILE NUMBER.....D  
 Z - NUMBER.....1  
 MASS-NUMBER.....2,014

H 1 0 .21 0 .066	.209 L <sub>1</sub> 3 3532 .42 5.1907 .209	.282 Symbol P Threshold Energy(eV) 1.897 Na 11 .99 .85 5.326 .628	.282 Atomic Number Alpha Inelastic Coefficient k in LSS Unit 1.979 Ca 20 .8392 1.31 13.91 1.08	.215 T <sub>1</sub> 22 1.973 1.53 4047 1.44 32.65 1.21	2.096 V 23 2.762 1.61 2.96 1.37	2.462 Cr 24 5.312 1.64 39.35 1.4	2.589 Mn 25 2.728 1.75 44.02 1.5	2.714 Fe 26 4.764 1.64 47.61 1.58	2.846 Co 27 4.747 1.64 47.93 1.58	2.971 Ni 28 4.737 1.64 40.64 1.58	3.103 Cu 29 4.725 2.16 36.16 1.76	3.232 Zn 30 4.725 2.16 16.26 1.76	3.365 Ga 31 4.725 2.16 31.61 1.87	3.5 As 32 4.528 2.25 51.68 1.75	3.773 Br 35 35.01 2.12	3.909 Kr 36 18.13 2.14
K 19 1.604 1.28 6.878 1.06	.204 Ca 20 .8392 1.31 13.91 1.08	.282 Symbol P Threshold Energy(eV) 1.897 Mg 12 .7666 .68 7.783 .664	.215 T <sub>1</sub> 22 1.973 1.53 4047 1.44 32.65 1.21	2.096 V 23 2.762 1.61 2.96 1.37	2.339 Cr 24 5.312 1.64 39.35 1.4	2.462 Mn 25 2.728 1.75 44.02 1.5	2.589 Fe 26 4.764 1.64 47.61 1.58	2.714 Co 27 4.747 1.64 47.93 1.58	2.846 Ni 28 4.737 1.64 40.64 1.58	2.971 Cu 29 4.725 2.16 36.16 1.76	3.103 Zn 30 4.725 2.16 16.26 1.76	3.232 Ga 31 4.725 2.16 31.61 1.87	3.365 As 32 4.528 2.25 51.68 1.75	3.773 Br 35 35.01 2.12	3.909 Kr 36 18.13 2.14	
Rb 37 2.706 2.64 13.57 2.29	.205 Sr 38 2.61 2.22 2.61 2.25	.282 Symbol P Threshold Energy(eV) 1.897 Y 39 72.84 2.35	.215 T <sub>1</sub> 40 2.609 2.82 107.1 2.45	2.096 V 41 3043 2.97 132.4 2.58	2.339 Cr 42 3.765 2.97 123.5 2.66	2.462 Mn 43 3.765 2.97 123.5 2.66	2.589 Fe 44 5.501 3.13 129.2 2.71	2.714 Co 45 5.501 3.13 112.2 2.77	2.846 Ni 46 5.501 3.13 79.03 2.86	2.971 Cu 47 5.501 3.13 112.2 2.77	3.103 Zn 48 5.501 3.13 55.75 3.09	3.232 Ga 49 5.501 3.13 72.07 3.19	3.365 As 50 5.501 3.13 64.99 3.27	3.773 Br 51 55.61 3.43 27.51 3.41	3.909 Kr 52 27.51 3.41 4.123 3.53	
Cs 55 3.685 4.18 20.9 3.57	.206 Ba 56 1.661 4.33 51.55 3.69	.282 Symbol P Threshold Energy(eV) 1.897 La 57 71.57 4.39 122.9 3.74	.215 T <sub>1</sub> 72 4.142 5.78 236.7 4.81	2.096 V 73 3.627 5.87 302.7 4.88	2.339 Cr 74 4.444 5.98 316.4 5.02	2.462 Mn 75 4.444 5.98 316.4 5.02	2.589 Fe 76 5.578 6.06 323.8 4.95	2.714 Co 77 5.578 6.06 323.8 4.95	2.846 Ni 78 5.578 6.06 323.8 4.95	2.971 Cu 79 5.578 6.06 323.8 4.95	3.103 Zn 80 5.578 6.06 28.26 5.41	3.232 Ga 81 5.578 6.06 28.26 5.41	3.365 As 82 5.578 6.06 28.26 5.41	3.773 Br 83 5.578 6.06 28.26 5.41	3.909 Kr 84 28.26 5.41 4.123 3.53	
Fr 87 0 7.44	.207 Ra 88 2.765 7.56 80.71 6.1	.282 Symbol P Threshold Energy(eV) 1.897 Ac 89 1.089 7.6 207.7 6.13	.215 T <sub>1</sub> 88 1.750 4.45 119.9 3.77	2.096 V 89 1.886 4.45 103.4 3.79	2.339 Cr 90 1.886 4.45 103.4 3.79	2.462 Mn 91 1.886 4.45 103.4 3.79	2.589 Fe 92 1.886 4.45 103.4 3.79	2.714 Co 93 1.886 4.45 103.4 3.79	2.846 Ni 94 1.886 4.45 103.4 3.79	2.971 Cu 95 1.886 4.45 103.4 3.79	3.103 Zn 96 1.886 4.45 100.2 4.38	3.232 Ga 97 1.886 4.45 100.2 4.38	3.365 As 98 1.886 4.45 100.2 4.38	3.773 Br 99 1.886 4.45 100.2 4.38	3.909 Kr 100 100.2 4.38 4.123 3.53	
He 2. 0 .33 0 .141	.208 Ne 10 52.76 .78 .092 .556	.282 Symbol P Threshold Energy(eV) 1.897 Ar 18 17.9 3.1 1.871 .558	.215 T <sub>1</sub> 101 1.391 5.95 10.74 .447	2.096 V 102 1.391 5.95 10.74 .447	2.339 Cr 103 1.391 5.95 10.74 .447	2.462 Mn 104 1.391 5.95 10.74 .447	2.589 Fe 105 1.391 5.95 10.74 .447	2.714 Co 106 1.391 5.95 10.74 .447	2.846 Ni 107 1.391 5.95 10.74 .447	2.971 Cu 108 1.391 5.95 10.74 .447	3.103 Zn 109 1.391 5.95 10.74 .447	3.232 Ga 110 1.391 5.95 10.74 .447	3.365 As 111 1.391 5.95 10.74 .447	3.773 Br 112 1.391 5.95 10.74 .447	3.909 Kr 113 10.74 .447 4.123 3.53	

PARAMETERS OF THE THIRD MATSUNAMI EMPIRICAL FORMULA AT NORMAL INCIDENCE	
PROJECTILE	.....
Z - NUMBER	..... 1
KOSS-NUMBER	..... 3.016

TABLE 22 PARAMETERS OF THE THIRD MATSUMI EMPIRICAL FORMULA AT NORMAL INCIDENCE

TABLE 23 PARAMETERS OF THE THIRD MOTSUNAMI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
PROJECTILE  
Z - NUMBER..... 6  
MASS NUMBER..... 12.01

**TABLE 24.** PARAMETERS OF THE THIRD MATSUBANI EMPIRICAL FORMULA AT NORMAL INCIDENCE

PROJECTILE.....  
Z NUMBER..... O  
MASS-NUMBER..... 20.10

15.35		10.65		10.65		10.65		10.65		10.65		10.65		10.65			
H 1	0 .15	Li 3	Be 4	Sc 21	Cr 24	Mn 25	Fe 26	Co 27	Ni 28	Cu 29	Zn 30	Ga 31	Ge 32	As 33	Se 34	Br 35	
0 .107	3.586 .19	4.658 .2	3.586 .19	34.72 .097	21.16 .09	14.38 .27	11.23 .28	3.944 .37	7.577 .37	10.3 .38	6.659 .39	10.19 .4	9.746 .42	6.05 .3	12.59 .45	24.46 .45	
Na 11	Mg 12	Ca 20	Sr 38	Ba 56	La 57	Hf 72	Ta 73	W 74	Re 75	Os 76	Pt 78	Au 79	Hg 80	Tl 81	Pb 82	Bi 83	
5.985 .146	7.689 .151	15.47 .222	22.57 .388	24.75 .405	24.91 .416	24.98 .257	15.61 .247	10.98 .257	16.04 .261	16.28 .271	16.47 .272	12.78 .288	10.18 .309	13.91 .319	10.67 .328	8.097 .341	
30.37	32.03	32.74	33.97	35.22	36.87	38.16	39.85	41.15	43.06	44.07	45.45	46.8	48.23	49.75	51.05		
K 19	Ca 20	Sc 21	Ti 22	V 23	Cr 24	Mn 25	Fe 26	Co 27	Ni 28	Cu 29	Zn 30	Ga 31	Ge 32	As 33	Se 34	Br 35	
25.46 .35	12.38 .33	2.845 .36	5.683 .35	3.944 .37	7.577 .37	10.3 .38	6.676 .38	6.657 .39	6.659 .39	10.19 .4	20.16 .41	4.926 .295	10.18 .309	13.91 .319	10.67 .328	8.097 .341	
3.874 .203	7.594 .207	15.47 .222	18.68 .232	20.35 .242	15.61 .247	10.98 .257	16.04 .261	16.28 .271	16.47 .272	12.78 .288	10.18 .309	13.91 .319	10.67 .328	8.097 .341	4.38P .346	.432 .359	
55.78	57.38	59.1	60.69	62.37	63.9	65.45	67.11	68.8	70.33	72.09	73.33	75.2	76.75	78.38	81.76	84.13	
Rb 37	Sr 38	Y 39	Zr 40	Nb 41	Mo 42	Tc 43	Ru 44	Rh 45	Pd 46	Ag 47	Cd 48	In 49	Sn 50	Sb 51	Te 52	I 53	
34.73 .47	17.39 .37	6.949 .48	3.294 .48	3.825 .49	4.191 .49	4.626 .5	6.752 .51	6.879 .51	8.812 .52	12.66 .53	13.29 .55	12.253 .56	12.35 .56	15.24 .58	31.11 .58	216.8 .59	
3.06 .366	6.197 .374	15.75 .379	22.57 .388	27.37 .394	24.75 .405	24.91 .416	24.98 .257	21.02 .431	14.29 .443	10.86 .449	9.387 .474	11.73 .487	10.38 .498	8.519 .516	4.234 .517	.616 .533	
85.11	86.69	88.5	115.4	117.3	119.1	121	122.8	124.7	126.6	128.5	130.4	132.2	134.1	136.1	139.1	140.2	
Cs 55	Ba 56	La 57	Hf 72	Ta 73	W 74	Re 75	Os 76	Ir 77	Pt 78	Au 79	Hg 80	Tl 81	Pb 82	Bi 83	Po 84	At 85	
43.82 .59	18.53 .61	7.958 .61	4.25 .71	3.5 .72	4.515 .73	5.814 .73	6.468 .74	7.245 .75	10.67 .76	5.24 .77	22.29 .78	19.47 .79	28.52 .8	0 .8	215 .83	Rn 86	
3.091 .559	7.416 .555	17.51 .551	27.88 .709	33.29 .719	39.08 .729	35.49 .739	36.5 .739	31.17 .761	28.35 .771	17.33 .779	3.077 .772	8.123 .806	9.49 .817	10.24 .824	7.065 .829	0 .829	.616 .533
143.7	145.6	147.7	90.36	92.25	93.95	95.85	97.41	99.27	101.9	102.7	104.4	106.3	108.1	110	111.7	113.6	
Fr 87	Ra 88	Ac 89	Ce 98	Pr 99	Nd 100	Pm 101	Sm 102	Eu 103	Gd 104	Tb 105	Dy 106	Ho 107	Er 108	Tm 109	Yb 110	Lu 111	
0 .83	26.24 .84	10.33 .86	14.52 .87	10.76 .82	11.74 .84	10.64 .82	20.12 .84	9.064 .66	9.357 .66	12.52 .67	12.21 .68	11.74 .68	16.1 .69	24.46 .7	8.904 .7	.5676	
0 .876	6.166 .887	20.76 .892	17.51 .892	14.56 .877	15.49 .857	10.76 .82	0 .596	8.616 .611	7.518 .605	16.96 .636	12.62 .649	13.83 .659	13.12 .649	10.22 .674	6.827 .689	19 .674	
149.5	151.7	153.5	Th 90	Pa 91	U 92	9.269	He 2	0 .17	0 .086	0 .17	0 .086	0 .17	0 .086	0 .17	0 .086	0 .086	

TABLE 25  
PARAMETERS OF THE THIRD MATSUBORI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
PROJECTILE:  $\alpha$   
 $Z$  - NUMBER: 18  
MASS-NUMBER: 39-94

63.05		35.54		36.83		40.64		45.79		48.39		51.02		51.48		55.92	
H	1	Li	3	Be	4	B	5	C	6	N	7	O	8	F	9	Ne	10
0	.12	0	.119	0	.091	2.513	.18	6.889	.18	3.987	.19	8.465	.2	26.84	.21	1323	.21
0	.09	0	.09	0	.09	62.13	.093	107.4	.1	62.83	.103	61.351	.109	119	.113	0	.113
57.25		61.08		62.81		66.81		68.38		72.28		75.44		73.82		73.82	
Na	11	Hg	12	Al	13	Si	14	P	15	S	16	Cl	17	Ar	18	Ar	18
25.64	.22	20.21	.22	10.49	.25	5.552	.23	10.47	.24	13.24	.24	27.94	.25	502.9	.26	502.9	.26
9.509	.113	12.41	.12	25.79	.124	34.22	.127	25.66	.131	19.2	.134	6.016	.139	.467	.144	.467	.144
79.49		83.36		83.5		85.64		87.8		91.5		93.8		97.59		99.84	
K	19	Cs	20	Sc	21	Tl	22	V	23	Cr	24	Hn	25	Fe	26	Co	27
45.42	.26	23.85	.26	11.47	.27	5.584	.27	7.79	.28	15.01	.28	13.32	.29	13.35	.3	13.37	.32
5.499	.146	10.71	.148	21.18	.155	25.4	.16	26.87	.165	20.32	.167	14.2	.172	20.63	.175	20.6	.18
127.3		130.5		134		137.1		140.5		143.3		146.1		149.4		152.7	
Rb	37	Sr	38	Y	39	2	40	Nb	41	No	42	Tc	43	Ru	44	Rh	45
71.47	.24	35.85	.34	14.34	.35	6.633	.35	7.909	.35	8.676	.36	9.586	.36	14	.37	18.3	.37
3.417	.228	6.898	.232	17.34	.235	29.64	.243	28.66	.239	26.35	.248	25.79	.258	21.9	.261	14.7	.268
182.8		185.5		189.1		239.7		243.2		246.7		250.2		253.4		257.1	
Cs	55	Ba	56	La	57	Hf	72	Ta	73	H	74	Re	75	Os	76	Ir	77
91.19	.31	38.56	.42	16.56	.42	8.799	.48	7.245	.48	9.339	.49	12.08	.49	13.36	.49	15.23	.5
2.91	.317	6.887	.324	16.19	.328	23.24	.404	29.25	.409	32.18	.415	29.06	.419	29.62	.427	25.19	.431
292.2		295.8		299.8		302.8		306.6		309.7		303.6		306.1		309.7	
Fr	87	Re	88	Ac	89	Pr	59	Nd	60	Pm	61	Sm	62	Eu	63	Gd	64
0	.54	53.72	.54	21.14	.35	17.32	.42	20.45	.43	22.39	.43	0	.33	36.03	.44	41.84	.44
0	.49	6.177	.496	15.83	.498	15.63	.371	13.38	.333	12.28	.339	0	.341	7.71	.35	6.699	.354
303		307.4		310.3		313		316		319.1		322.6		325.8		326.5	
Th		90		91		92		93		94		95		96		97	
0		13.34		15.35		23.12		35.08		0		.25		11.79		.56	
0		20.89		20.89		.307		.307		.307		.307		.307		.307	

**TABLE 26** PARAMETERS OF THE THIRD MATSUBANI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
 PROJECTILE NUMBER.....Al  
 Z - NUMBER.....13  
 M&S-NUMBER.....26.98

28.35	H 1 O .12 O .113	16.16 Li 3 Be 4 4.367 .18 5.997 .19 27.21 .068 44.19 .094	18.11 Symbol P Threshold Energy (ev) 5.997 .19 44.19 .094	16.11 El / 1000 Atomic Number Alpha Inelastic Coefficient k in LSS Unit	20.31 B 5 C 6 5.292 .2 5.292 .2 65.94 .099 77.28 .105 45.64 .11	23.13 N 7 0 8 F 9 Ne 10	24.81 3.038 .21 6.395 .22 21.48 .23 6.202 .12	26.51 45.64 .11 21.78 .115 11.47 .512 12.5 .536	27.72 19.435 .27 19.77 .28 6.372 .164 6.375 .175	29.78 7.459 .26 4.001 .26 18.42 .152 15 .156	41.68 C1 17 Ar 18		
30.91	33.21	Na 11 Mg 12 18.79 .25 14.74 .25 7.179 .131 9.418 .135	K 19 Ca 20 Sc 21 V 23 Cr 24 Mn 25 Fe 26 Co 27 Ni 28 Cu 29 Zn 30 Ge 32 As 33 Se 34 Br 35 Kr 36 xe 54 Rn 86	48.02 48.68 50.27 51.88 54.21 55.89 58.28 59.95 62.72 63.87 65.99 67.42 69.29 71.33 72.97 75.36 77.69	16.11 Symbol P Threshold Energy (ev) 5.997 .19 44.19 .094	16.11 Be 4 Alpha Inelastic Coefficient k in LSS Unit	20.31 B 5 C 6 5.292 .2 5.292 .2 65.94 .099 77.28 .105 45.64 .11	23.13 N 7 0 8 F 9 Ne 10	24.81 3.038 .21 6.395 .22 21.48 .23 6.202 .12	26.51 45.64 .11 21.78 .115 11.47 .512 12.5 .536	27.72 19.435 .27 19.77 .28 6.372 .164 6.375 .175	41.68 C1 17 Ar 18	
45.64	81.48	83.83	85.96	88.23	90.24	92.27	94.5	96.77	101.1	103	105.2	107.2	
31.88 .29	Sr 38	Y 39	Zr 40	Nb 41	Ta 73	W 74	Tc 43	Ru 44	Rh 45	Pd 46	Cd 48	Sn 50	
47.92 .4	24 6.274	9.596 .31	3.865 .32	10.35 .33	14.07 .33	9.121 .34	9.114 .34	13.98 .35	27.69 .36	8.326 .38	13.09 .38	32.62 .39	
3.11 .297	15.91 .307	17.29 .168	20.92 .196	22.34 .203	17.11 .207	11.94 .214	17.4 .218	17.55 .226	13.61 .227	5.224 .224	14.51 .224	4.512 .222	
79.33	120.2	122.7	128.3	140.7	145.2	165.7	168	170.6	173	175.6	178	180.4	
Cs 55	Ba 56	La 57	Hf 72	Ta 73	W 74	Re 75	Os 76	Ir 77	Pt 78	Au 79	Hg 80	Tl 81	
60.5 .5	25.55 .51	10.98 .52	5.84 .59	4.809 .6	6.2 .61	8.874 .61	10.12 .62	9.962 .63	14.65 .63	85.28 .64	30.82 .65	28.42 .65	
2.911 .229	6.945 .44	16.36 .445	24.92 .558	31.47 .558	31.48 .558	31.48 .573	32.26 .591	27.5 .597	23.26 .603	15.23 .611	2.695 .621	7.616 .632	8.908 .645
195.5	198	200.8	205.2	127.8	130	132.6	135.5	137	139	141.5	145.6	148.7	
Fr 87	Ra 88	Ac 89	Ce 58	Pr 59	Nd 60	Pm 61	Sm 62	Eu 63	Gd 64	Tb 65	Dy 66	Ho 67	
0 .68	35.82 .69	14.09 .69	11.49 .52	13.36 .52	14.85 .53	0 .53	23.89 .54	27.74 .54	12.87 .55	17.24 .56	16.81 .57	16.16 .57	
0 .685	7.01 .693	17.98 .697	15.83 .449	13.37 .452	12.52 .461	0 .464	7.935 .478	6.914 .483	15.5 .497	15.2 .503	11.47 .512	12.5 .519	
46	7h 90	Pa 91	U 92	8.914 .7	0 .7	7.871 .71	.709	.728	208.3	208.3	208.3	208.3	

TABLE 27 PARAMETERS OF THE THIRD MATSUBAHI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
 PROJECTILE ..... Fe  
 Z - NUMBER ..... 26  
 MASS-NUMBER ..... 55.85

141	H 1	71.46	77.35	Symbol	77.35	EL/1000	86.29	94.16	98.37	102.6	102.6	110.3
L1 3	Be 4	9.856 .16	Alpha*	B 5	C 6	N 7	D 8	F 9	Ne 10	He 2	O .14	0 .094
7 .15	9.856 .16	9.854 .094	P	3.277 .17	9.017 .17	5.278 .18	11.3 .18	38.88 .19	1792 .19	0	0	0 .094
52.95 .091	81.54 .094	84.54 .094	Threshold Energy(eV)	124.3 .097	144.4 .101	84 .104	35.5 .106	11.01 .108	249 .111			
111.6	118.4		Inelastic Coefficient k in LSS Unit	120.6	127.7	129.5	135.4	137.3	135.4			
Na 11	Mg 12			A1 13	Si 14	P 15	S 16	C1 17	Cl 17	Ar 18		
35.02 .2	27.73 .2			14.5 .21	7.701 .21	14.61 .22	16.54 .22	39.41 .22	714.8 .23			
12.4 .113	16.43 .116			35.29 .118	44.06 .121	30.24 .124	24.47 .126	11.15 .129	.584 .173			
147	K 19	155.7	152.4	155.3	158.2	164.5	167.7	174.1	177.2	185.2	190.9	192.7
64.55 .23	35.98 .23	16.46 .24	8.05 .25	11.28 .25	21.77 .25	29.86 .26	19.43 .26	19.55 .26	19.57 .26	60.14 .27	29.3 .28	18.28 .28
6.896 .135	15.4 .137	26.22 .141	31.24 .144	32.85 .148	25.03 .15	17.21 .154	24.97 .156	24.97 .156	24.97 .156	7.167 .169	14.39 .174	14.58 .181
218	Rb 37	222.8	228.5	233.2	238.5	242.5	246.7	251.7	254.8	260.6	265.2	269.2
107 .3	55.71 .3	21.51 .3	10.22 .31	11.9 .31	15.07 .31	14.46 .32	21.15 .32	21.68 .32	21.7 .33	39.86 .33	41.98 .34	7.127 .34
3.919 .195	7.837 .198	19.78 .201	27.95 .204	33.58 .207	27.05 .211	29.58 .215	26.85 .218	24.45 .221	16.51 .225	4.766 .233	10.99 .246	4.377 .253
300.9	Cs 55	304.6	310.2	318.9	328.5	333.2	340.2	345.7	351.7	356.2	363.2	374.1
139.2 .36	Ba 56	58.91 .36	25.31 .36	13.35 .41	11.14 .41	14.37 .41	18.55 .41	20.56 .42	23.13 .42	33.69 .43	48.31 .44	58.69 .45
5.112 .262	7.324 .268	17.18 .27	23.54 .328	29.55 .332	32.41 .336	29.2 .339	29.64 .345	25.15 .348	21.14 .352	13.78 .355	6.783 .366	7.319 .37
463.4	Fr 87	445.7	474.9		316	322.1	326.6	332.7	336	341.6	345.1	355.1
0 .45	Ra 88	42.77 .45	32.57 .46	Ce 89	Fr 59	No 60	Pm 61	Sm 62	Eu 63	Tb 65	Er 68	Tm 69
0 .393	5.972 .397	15.29 .399	15.29 .399	26.48 .36	31.29 .37	34.26 .37	44.13 .38	35.21 .38	28.88 .38	39.9 .39	37.42 .39	51.3 .4
		16.56 .272	14.16 .274	12.94 .279	0	.37	.37	.37	.37	.37	.37	.37
						.28	8.066 .287	6.995 .29	15.46 .297	15.09 .3	11.28 .305	11.62 .308
							479.4	486.4	490.2			
							Th 90	Fr 91	U 92			
							20.58 .46	0 .46	18.16 .47			
							22.31 .405	0 .405	17.98 .47			

**TABLE 28** PARAMETERS OF THE THIRD MATSUNAMI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
PROJECTILE NUMBER ..... 11  
Z NUMBER ..... 28  
MASS-NUMBER ..... 59, 71

163	H 1	0 .11	0 .13	82.1	68.64	Symbol	68.64	Atomic Number	B 5	107.6	112.2	116.9	116.6	BB.66		
L 1	3	Be 4		1.3	4	P	Be 4	Alpha	B 5	C 6	N 7	O 8	F 9	He 2		
7.357	.15	10.37	.16	55.5	.092	BB.54	10.37	.16	5.454	.16	5.576	.17	11.95	.18		
126.6	134.2			12.3	14.1	Threshold Energy (ev)	BB.54	.095	150.1	.098	151	.102	41.18	.19		
Na 11	Mg 12			17.2	29.45	Inelastic Coefficient k in LSS Unit	BB.54	.095	15.42	.21	8.194	.21	19.76	.22		
37.17	.2	12.39	.116	12.39	.115	16.8	16.8	.116	34.65	.116	45.83	.111	25.43	.124		
165.4	172.8	171		174.1	177.3	184.2	187.7	198	207.4	212.9	214.7	218.9	223.8	233.2		
K 19	Ca 20	Sc 21	Ti 22	V 23	Cr 24	Mn 25	Fe 26	Co 27	Ni 28	Cu 29	Zn 30	Ga 31	Ge 32	As 33		
69.95	.23	36.31	.23	8.617	.24	32.33	.25	20.84	.25	32.5	.27	19.67	.28	31.03	.29	
7.15	.134	13.89	.137	17.14	.141	33.54	.147	25.85	.15	25.77	.153	19.4	.165	14.97	.179	
242.2	247.4	253.7		258.8	264.6	268.9	273.4	278.9	284.5	288.5	294.7	297.8	301.1	314.4		
Rb 37	Sr 38	Y 39	Zr 40	Nb 41	Ho 42	Tc 43	Ru 44	Rh 45	Pd 46	Ag 47	Cd 48	In 49	Sn 50	Sb 51	Te 52	
115.3	.29	57.89	.3	23.19	.3	11.02	.3	12.33	.3	15.61	.31	23.3	.32	45.57	.33	
4.015	.193	8.026	.196	20.25	.198	28.61	.201	30.15	.208	34.35	.204	29.46	.215	16.64	.222	
332.1	336.1	342.1		424.2	429.9	435.4	441.2	446.1	452.2	457.8	464	469.2	474.4	480.1		
Cs 55	Ba 56	La 57	Hf 72	Ta 73	W 74	Re 75	Os 76	Ir 77	Pt 78	Au 79	Hg 80	Tl 81	Pb 82	Bi 83	Po 84	
150.4	.35	63.74	.35	27.59	.36	14.66	.4	12.98	.4	15.57	.4	20.15	.4	25.41	.41	
3.169	.287	7.127	.263	17.52	.265	23.71	.321	29.76	.325	32.62	.333	29.81	.338	25.29	.341	
508.1	513.9	520.6		348.5	355.2	360	366.7	370.2	376.3	379.9	386	390.9	396.5	402.3		
Fr 87	Ra 88	Ac 89		Ce 58	Pr 59	Nd 60	Pm 61	Sm 62	Eu 63	Gd 64	Tb 65	Dy 66	Ho 67	Er 68	Tm 69	
0 .44	89.78	.44	35.53	.44	28.66	.36	33.87	.36	37.1	.36	39.79	.37	43.27	.38	47.16	.38
0 .384	5.976	.388	15.3	.39	36.79	.268	14.36	.269	15.11	.274	0 .275	8.162	.282	7.076	.295	
48	—	525.4	533.1		537.1									408.4	413.1	
Th 90		Pa 91		U 92									419.1			
22.33	.397	0 .396		19.7	.46								84.44	.39		
22.31	.397	0 .396		19.97	.405								5.922	.314		
—	48	—		16.37	.517								30.74	.59		
—	48	—		16.37	.517								5.922	.314		

TABLE 29  
PARAMETERS OF THE THIRD MATSUBA EMPIRICAL FORMULA AT NORMAL INCIDENCE

184.5	H 1	92.18	99.28	EL/1000	Symbol	99.28	Atomic Number	B 5	C +	N 7	I 20	I 28.3	I 38.8					
L 1 3	Be 4	10.58 .16	10.58 .16	P	Be 4	10.58 .16	Alpha	3.528 .16	9.727 .17	5.708 .17	12.25 .18	42.79 .18	1952 .19					
7.495 .15	7.495 .15	59.82 .092	59.82 .092	P	10.58 .16	9.727 .17	16.25 .101	94.26 .101	94.26 .101	44.25 .105	11.5 .106	-27.75 .106	-1.09					
139.9	148.2	139.9	148.2	Threshold Energy(eV)	95.31 .094	95.31 .094	Inelastic Coefficient k in LSS Unit	150.4	159	160.8	169	169.5	167.9					
Na 11	Mg 12	Sc 21	Ti 22	V 23	Cr 24	Mn 25	Fe 26	Co 27	Ni 28	Cu 29	Ag 31	P 15	S 16					
38.26 .19	38.26 .19	30.34 .2	30.34 .2	12.58 .24	12.58 .24	33.38 .25	21.73 .25	21.91 .25	35.95 .26	32.95 .26	16.09 .21	20.43 .21	43.33 .22	791.9 .22				
13.81 .111	14.72 .132	28.7 .136	34.12 .138	35.8 .141	27.26 .144	18.71 .147	27.13 .149	26.87 .152	27.24 .153	21.36 .157	7.739 .16	33.45 .12	27.05 .12	12.29 .125	.642 .128			
K 19	Ca 20	189	189.6	189.7	192.9	200.3	203.9	211.5	214.8	224.6	230.4	272.1	276.4	241.5	244.2	251.4	254.5	
71.5 .22	37.67 .22	18.3 .23	8.963 .24	12.58 .24	24.3 .24	35.8 .25	21.73 .25	21.91 .25	35.95 .26	32.95 .26	16.09 .21	20.43 .21	43.33 .22	81.64 .28	630.9 .28	630.9 .28	.596 .18	
7.581 .13	14.72 .132	28.7 .136	34.12 .138	35.8 .141	27.26 .144	18.71 .147	27.13 .149	26.87 .152	27.24 .153	21.36 .157	7.739 .16	33.45 .12	27.05 .12	12.29 .125	.642 .128	.596 .18		
260.6	266.2	272.8	278.1	284.2	288.7	293.4	299.1	305	309.1	315.6	318.7	324.2	328.4	333.3	335.7	344.1	348	
Rb 37	Sr 38	V 39	Zr 40	Nb 41	Hf 42	Tc 43	Ru 44	Rh 45	Pd 46	Ag 47	Cd 48	In 49	Sn 50	Sb 51	Te 52	I 53	x 54	
120.9 .29	40.73 .29	24.36 .29	11.57 .29	13.47 .29	14.81 .3	16.4 .3	23.99 .3	24.49 .31	31.46 .31	45.28 .31	102.6 .32	47.74 .32	81.09 .32	44.5 .33	55.03 .37	112.4 .33	784.5 .34	
4.181 .183	6.352 .185	21.06 .187	29.73 .189	35.68 .193	31.65 .196	31.33 .2	30.53 .203	25.82 .205	17.21 .209	12.19 .211	5.011 .216	10.1 .219	13.27 .224	11.51 .227	9.167 .234	4.5572 .234	.651 .39	
354.3	358.3	364.7	450.2	456.1	461.8	467.9	473	479.3	485.2	491.6	497	502.3	508.3	514.8	521.8	527.4	530.3	
Es 35	Ba 56	La 57	Hf 72	Ta 73	W 74	Re 75	Ds 76	Ir 77	Pt 78	Au 79	Hg 80	Tl 81	Pb 82	Bi 83	Po 84	At 85	Rn 86	
158.7 .34	47.18 .34	23.87 .34	15.48 .38	12.75 .39	16.44 .39	21.28 .39	23.54 .39	26.84 .4	26.43 .4	18.82 .4	22.62 .4	76.69 .41	103.5 .41	0 .41	77.77 .42	77.77 .42	.724 .34	
3.241 .241	7.644 .246	17.86 .249	24.06 .299	30.17 .303	33.05 .306	29.75 .309	30.16 .314	25.57 .317	21.43 .321	15.99 .323	2.483 .328	6.865 .332	7.401 .336	5.46 .34	0 .341	.724 .34	.724 .34	.754
537.3	543.3	550.4	555.3	563.4	571.4	578.5	585.5	590.5	594	400.4	404.1	410.5	415.5	421.4	427.4	433.8	444.9	
Fr 87	Ra 88	Ac 89	Fr 59	Nd 60	Pm 61	Sm 62	Eu 63	Gd 64	Tb 65	Dy 66	Ho 67	Er 68	Tm 69	Yb 70	Lu 71			
0 .42	94.87 .43	37.33 .43	30.22 .35	35.71 .35	39.13 .35	0 .35	63.06 .36	73.26 .36	33 .36	44.5 .37	45.61 .37	42.8 .37	58.68 .37	89.14 .38	32.45 .38			
0 .326	6 .36	15.36 .362	17.2 .251	14.7 .252	13.41 .256	0 .258	8.338 .264	7.225 .266	15.93 .272	11.54 .274	11.5 .279	12.47 .285	9.148 .287	6.016 .292	16.62 .295			

TABLE 30 PARAMETERS OF THE THIRD MATSUBUNAMI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
 2 - NUMBER.....  
 3 - NUMBER.....  
 4 - NUMBER.....  
 5 - NUMBER.....  
 6 - NUMBER.....

321.2		167		167		180.1		199.6		206.4		213.2		210.3		224.8																			
H	1	Li	3	Be	4	Cr	24	Mn	25	Fe	26	Cu	29	Zn	30	Ga	31	Ge	32	As	33	Se	34	Br	35	Kr	36								
0	.11	Li	3	Be	4	Cr	24	Mn	25	Fe	26	Cu	29	Zn	30	Ga	31	Ge	32	As	33	Se	34	Br	35	Kr	36								
0	.136	B	14	12.11	15	12.11	15	12.11	15	12.11	15	12.11	15	12.11	15	12.11	15	12.11	15	12.11	15	12.11	15	12.11	15	12.11	15								
0	.093	77.69	.093	123.6	.095	123.6	.095	123.6	.095	123.6	.095	123.6	.095	123.6	.095	123.6	.095	123.6	.095	123.6	.095	123.6	.095	123.6	.095	123.6	.095								
225	237.3																																		
280.6	292.4	286.4	289.9	293.4	304.1	308.2	319.1	322.8	337.4	335.6	343.4	344.3	349.5	356.1	358.7	368.8	372																		
K	19	Ca	20	Sc	21	Ti	22	V	23	Cr	24	Mn	25	Fe	26	Cu	29	Zn	30	Ga	31	Ge	32	As	33	Se	34	Br	35	Kr	36				
86.78	.21	45.8	.21	22.38	.21	11.78	.22	15.48	.22	29.75	.22	41.27	.23	26.9	.23	27.16	.23	27.22	.23	42.33	.24	41.29	.24	25.85	.25	40.37	.25	105.1	.25	106.4	.26				
9.391	.122	18.21	.124	35.28	.126	41.78	.128	43.67	.13	35.2	.131	22.71	.134	32.68	.135	32.44	.138	32.9	.139	24.45	.142	9.273	.144	24.64	.149	18.35	.151	13.63	.154	7.334	.155	.7			
380.4	387.7	396.8	403.7	412	417.4	423.2	430.6	435.4	435.5	435.2	435.3	435.4	435.5	435.3	435.2	435.3	435.4	435.3	435.2	435.1	435.2	435.1	435.2	435.1	435.2	435.1	435.2	435.1	435.2	435.1					
Rb	37	Sr	38	Y	39	Zr	40	Nb	41	Tc	43	Ru	44	Pd	46	Aq	47	Cd	48	In	49	Sn	50	Sb	51	Te	52	I	53	Xe	54				
153.2	.26	77.06	.26	30.91	.26	14.72	.27	17.15	.27	18.89	.27	20.94	.27	30.67	.28	31.38	.28	40.32	.28	131.8	.29	61.4	.29	10.44	.29	57.37	.29	71.08	.3	145.2	.3	101.5	.3	.7729	.202
4.899	.16	9.743	.162	24.58	.164	34.62	.166	41.48	.168	35.68	.171	36.2	.173	35.19	.175	29.71	.177	19.73	.178	14.86	.182	5.714	.185	12.38	.188	15.04	.191	10.31	.198	5.143	.198	.7			
499.8	504.3	512.8	512.8	621.9	629.6	635.8	644.6	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4	646.4				
Os	35	Ba	56	La	57	Hf	72	Ta	73	W	74	Os	75	Pt	77	Ru	78	Tl	81	Pd	82	Bi	83	Pb	84	At	85	Rn	86						
205.4	.3	87.04	.31	37.42	.31	20.35	.34	16.68	.34	21.52	.34	27.87	.35	20.54	.35	35.17	.35	34.65	.35	29.68	.36	10.63	.36	98.97	.36	92.82	.36	17.6	.36	102.2	.37	.757	.289		
3.627	.204	8.468	.208	19.86	.209	23.73	.207	32.47	.205	35.49	.205	31.89	.205	32.45	.205	27.29	.205	22.98	.205	14.87	.205	2.802	.205	7.814	.205	8.372	.205	5.753	.205	0	.279	.757	.289		
731.9	739.5	748.8				521.9	531.5	537.6	547.3	550.8	559.3	563.2	571.6	577.7	585.3	593	601.5	607.2	615.5																
Ft	87	Re	88	Ac	89	Ge	90	Pr	91	Nd	92	Fm	93	Eu	94	Id	94	Tb	95	Dy	96	Ho	97	Tm	98	Er	99	Yb	100	Lu	101				
0	.37	124.8	.78	49.1	.29	49.1	.29	49.1	.29	49.1	.29	39.19	.31	46.32	.31	50.8	.31	82.01	.32	42.98	.32	55.47	.33	58.05	.33	76.62	.33	116.5	.34	42.42	.34	6.512	.242		
0	.29	6.254	.203	16	.294	19.12	.211	16.34	.212	14.86	.215	0	.216	9.192	.221	7.954	.223	17.46	.227	17.01	.229	12.66	.232	13	.234	15.56	.237	9.934	.239	6.512	.242	17.96	.244		

**TABLE 31** PARAMETERS OF THE THIRD MATSUBAUMI EPIRICAL FORMULA AT NORMAL INCIDENCE  
Z - NUMBER ..... 54  
MASS-NUMBER ..... 131.3

**TABLE 32**  
PARAMETERS OF THE THIRD RATELIANI EMPIRICAL FORMULA AT NORMAL INCIDENCE  
2 - NUMBER .....<sup>149</sup><sub>80</sub>  
MASS-NUMBER .....<sup>200</sup><sub>5</sub>

2175	H 1	0 .1 0 .159	1126	He 2 .	0 .11 0 .112
1002	Li 3	Be 4	1114	1221	1245
13.71 .12	19.43 .13	13.71 .105	B 5	C 6	N 7
182 .287	287 .106	6.635 .13	18.5 .15	11.01 .14	23.96 .14
78.26 .15	62.67 .15	417.7 .108	481.6 .112	276.9 .112	84.24 .14
58.69 .112	50.23 .114	102.2 .115	134.5 .115	90.94 .114	35.29 .111
1275	Na 11	Mg 12	1325	1384	1395
85.09 .17	85.09 .17	35.36 .15	17.89 .16	34.55 .16	95.8 .16
19.91 .117	19.91 .117	102.2 .115	134.5 .115	73.18 .116	32.77 .115
1451	Ca 20	Sc 21	1443	1442	1486
42.19 .17	42.19 .17	71 .22	V 23	Cr 24	Mn 25
20.92 .117	20.92 .117	40 .31	57.76 .18	80.26 .18	52.51 .18
86.47 .118	86.47 .118	69 .43	57.97 .119	46.13 .12	65.23 .121
73.6 .117	73.6 .117	69 .43	57.97 .119	46.13 .12	65.23 .121
1679	1712	1730	1757	1747	1778
45.37 .2	45.37 .2	40 .42	Tc 43	Ru 44	Rh 45
162.5 .2	162.5 .2	40 .51	45.46 .21	66.4 .21	84.4 .19
18.31 .13	18.31 .13	67.48 .134	66.16 .135	53.84 .137	84.4 .19
45.96 .131	45.96 .131	76.85 .133	67.48 .134	53.84 .136	84.4 .19
1952	1979	2252	2272	2289	2307
199.8 .23	199.8 .23	48.56 .25	59.92 .25	66.98 .25	84.93 .25
14.71 .148	14.71 .148	50.46 .166	51.62 .167	49.11 .167	49.11 .167
44.6 .23	44.6 .23	53.95 .149	46.49 .145	50.46 .166	51.62 .167
6.171 .137	6.171 .137	53.95 .149	46.49 .145	50.46 .166	51.62 .167
2511	2529	2557	2008	2041	2053
Fr 87	Ra 88	Ac 89	Ce 88	Pr 59	Nd 60
0 .27	308.3 .27	121.4 .27	89.87 .23	106.4 .23	117.1 .23
0 .105	9.008 .184	23 .185	32.07 .15	27.36 .151	24.73 .152
2565	2604	2601	Th 90	Pa 91	U 92
76.57 .27	0	.27	48.18 .27	.187	29.23 .189
53.14 .187	0	.187			

### Captions of Figures

- Fig. 1 Best-fit values of  $f$  for light-ion sputtering, where the ratio of  $f$  to  $\sqrt{U_s}$  is plotted as a function of the mass ratio  $M_2/M_1$ , the solid line is calculated from eq.(8).
- Fig. 2 Best-fit values of  $\theta_{opt}$  for light-ion sputtering, where the best-fit  $\theta_{opt}$ 's are plotted against  $\eta$  and the solid line is the theoretical curve calculated from Eq. (12).
- Fig. 3 The best-fit values of  $f$  for relatively high-energy heavy ion sputtering, where the solid line corresponds to Sigmund  $f_s$  of  $m = 1/3$ .
- Fig. 4 The ratios of the best-fit  $f$ 's to Sigmund  $f_s$  as a function of  $\eta = 1 - (E_{th}/E)^{1/2}$ , where the solid line corresponds to Eq. (17).
- Fig. 5 The best-fit values of  $90^\circ - \theta_{opt}$  as a function of  $\psi$ , where the solid line corresponds to  
$$\theta_{opt} = 90^\circ - 286 \psi^{0.45}.$$
- Figs. 6 through 58  
The normalized sputtering yield  $Y(\theta)/Y(0)$  as a function of the angle of incidence, where the solid lines in these figures are best-fit curves to the present empirical formula, and the solid lines with x marks show the results calculated by putting the average values of  $f$  and  $\Sigma$  into the present empirical formula. The average parameters of  $f$  and  $\Sigma$  are easily calculated using the parameters listed in Table 5 through 18.

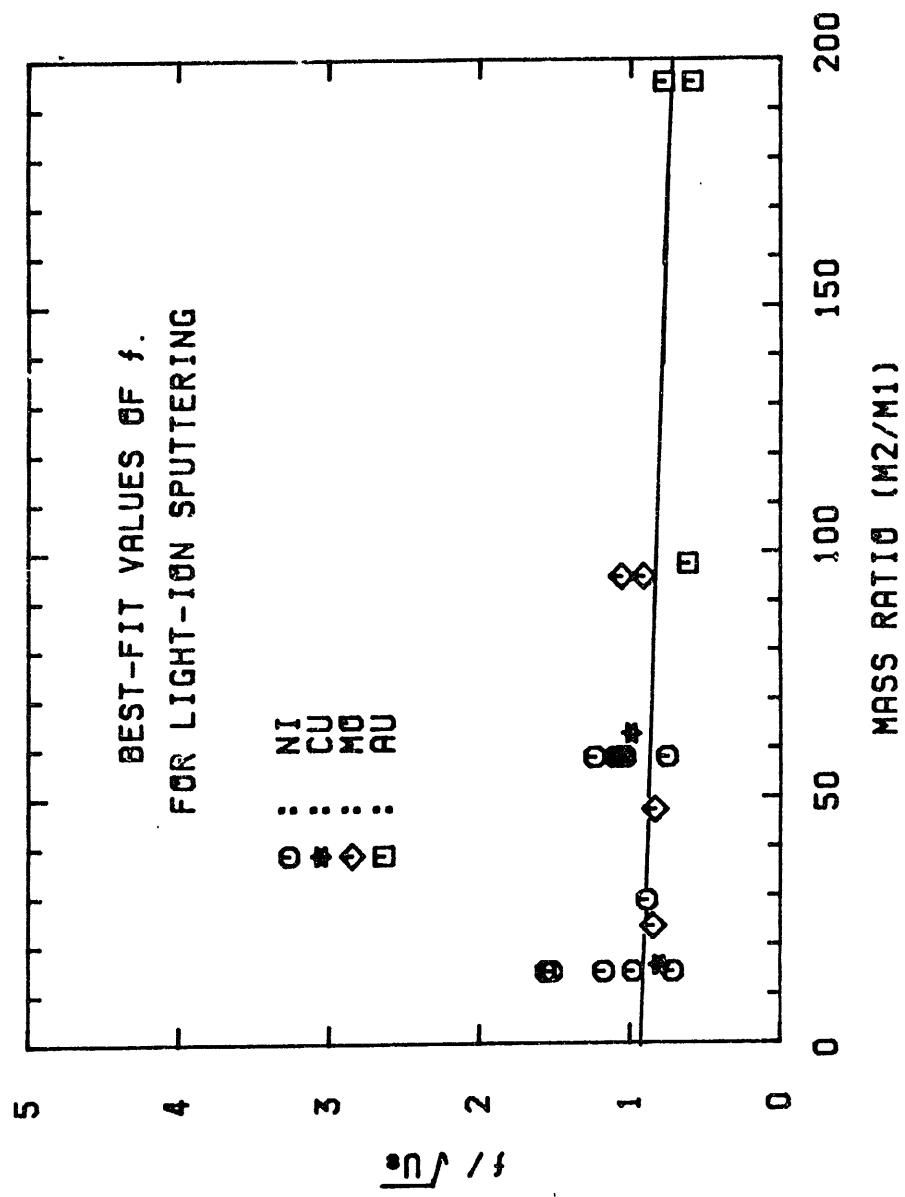


Fig. 1

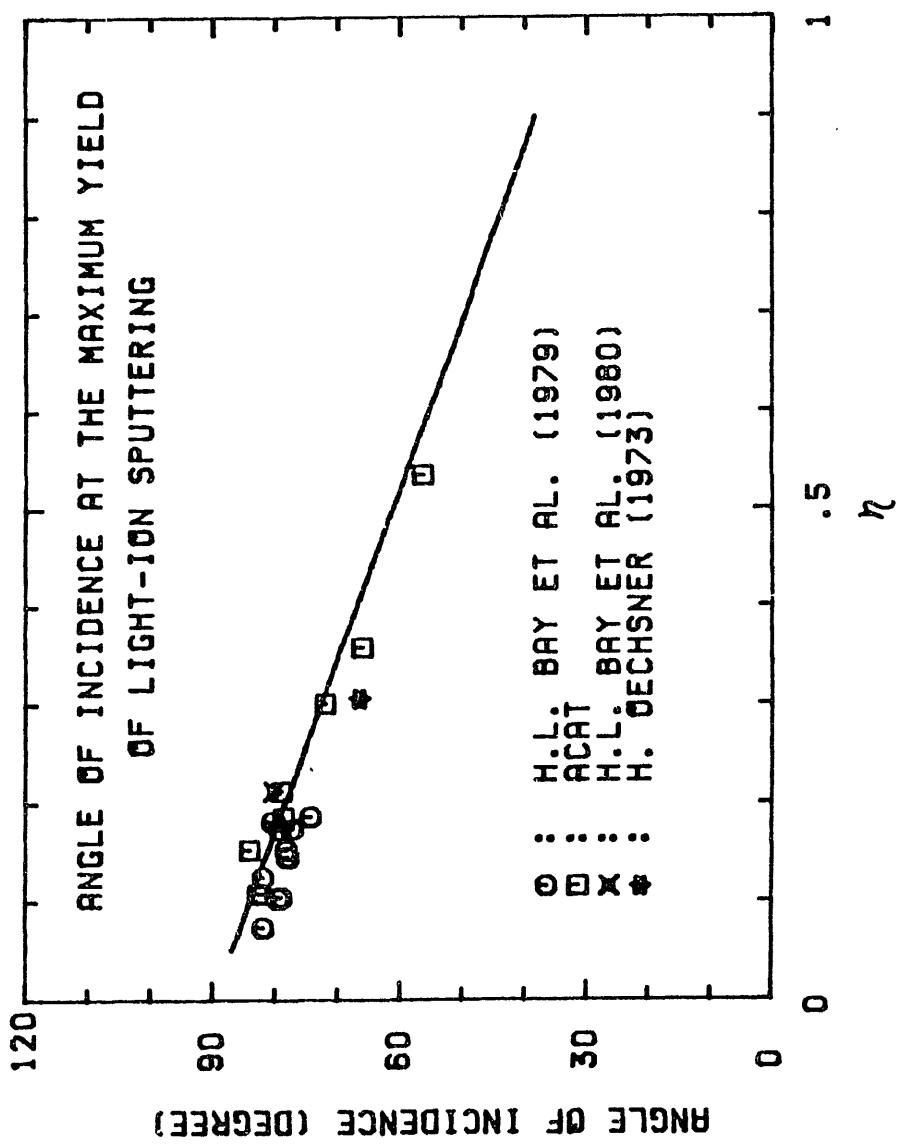


Fig. 2

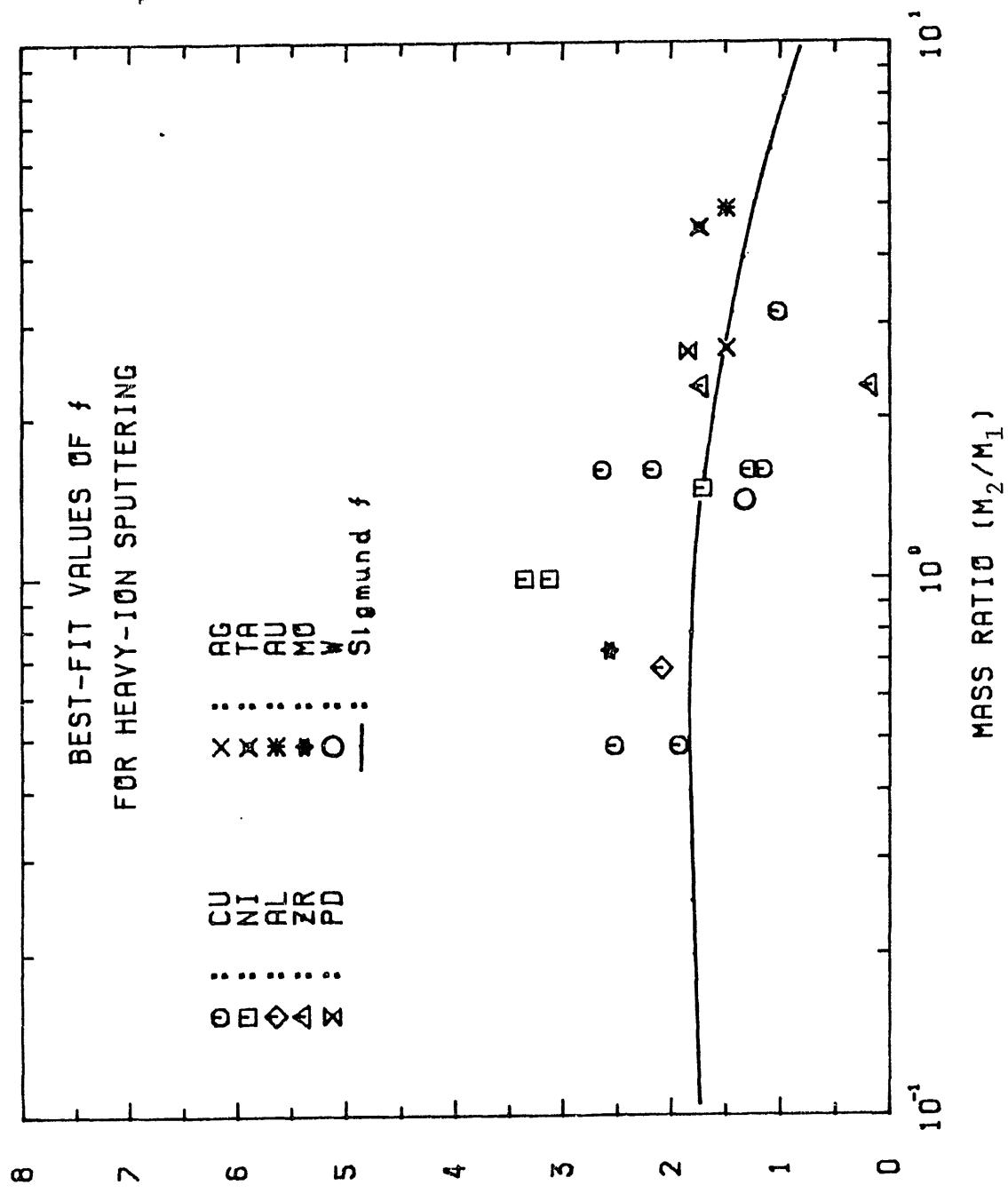


Fig. 3

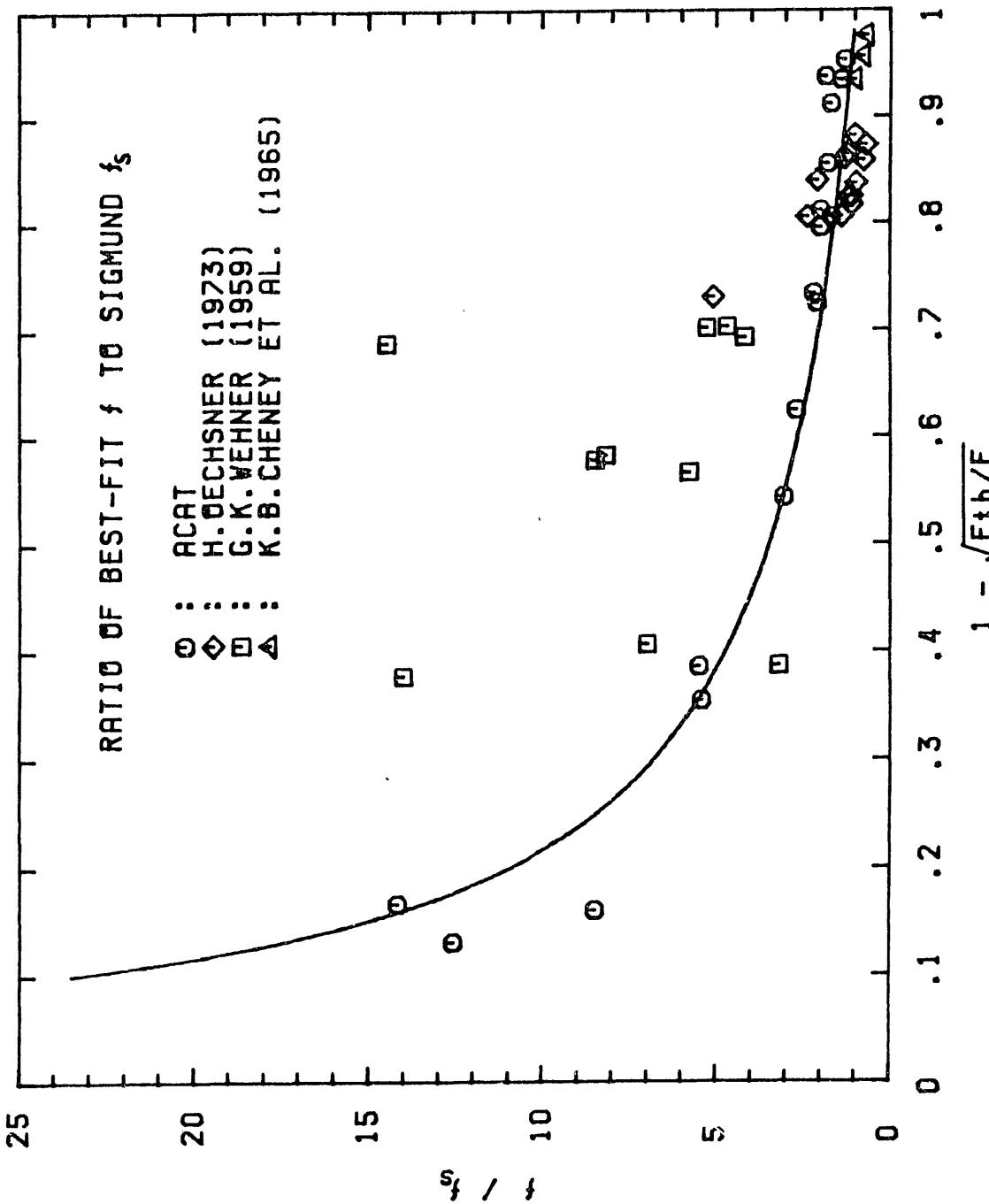


Fig. 4

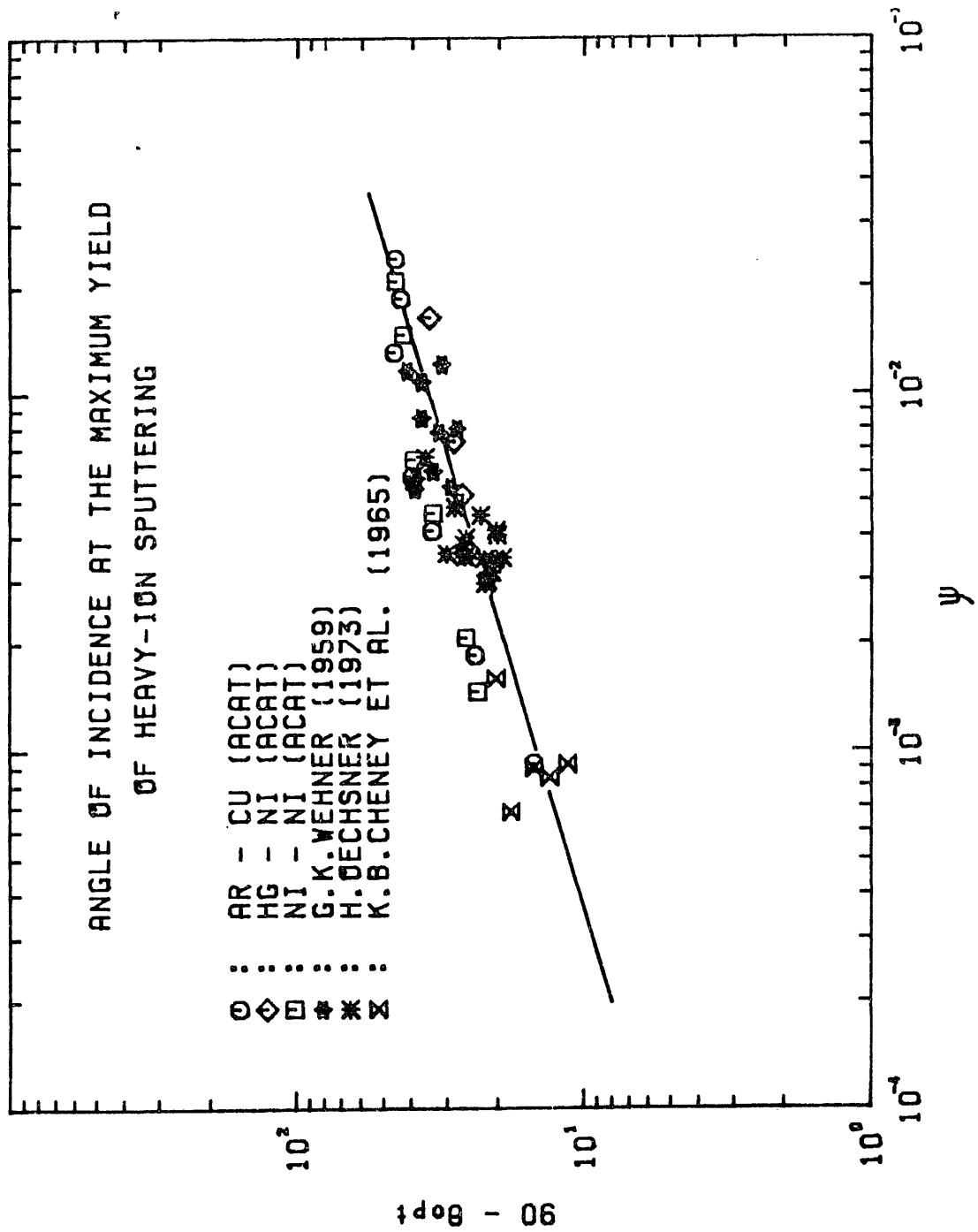


Fig. 5

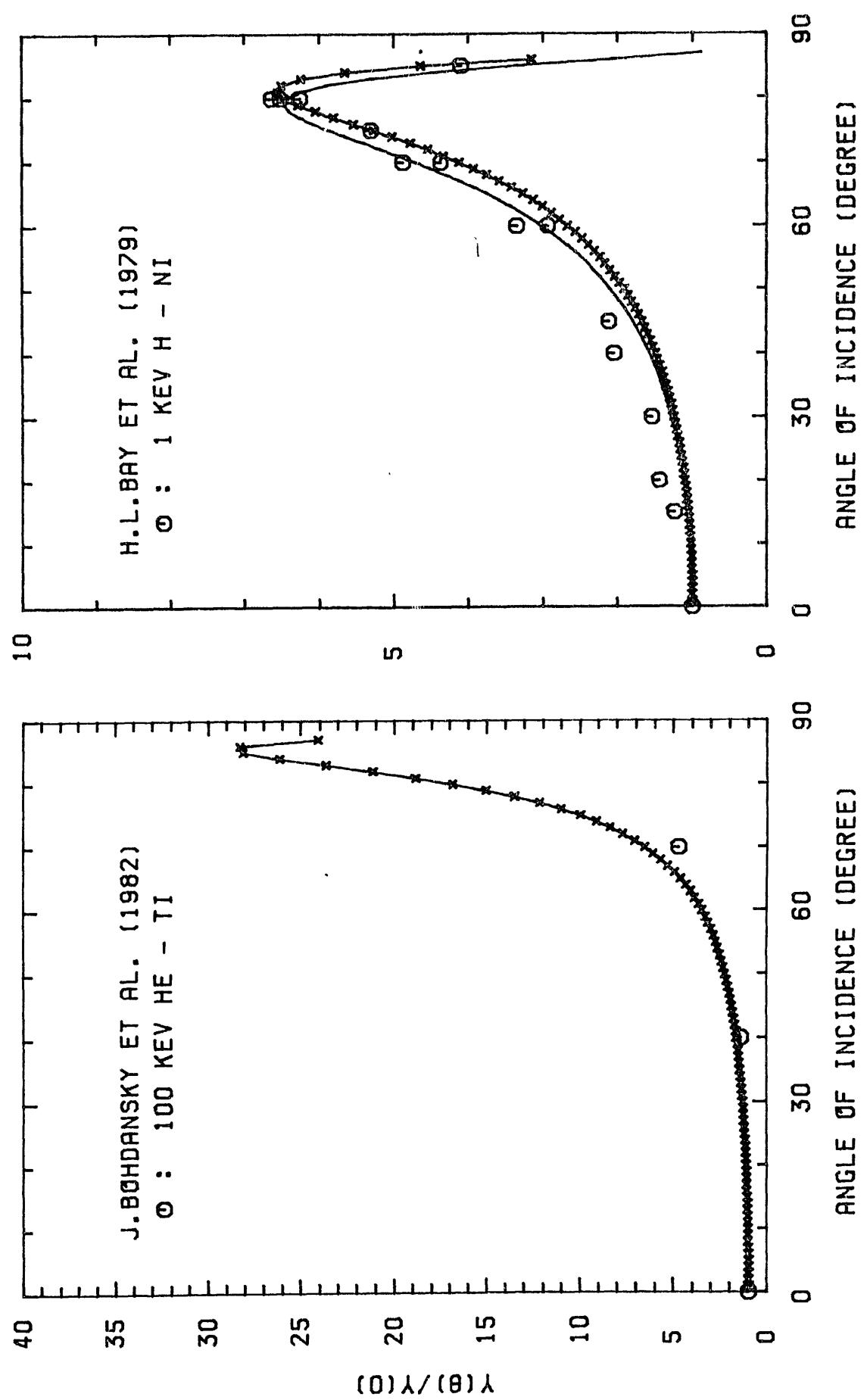


Fig. 6

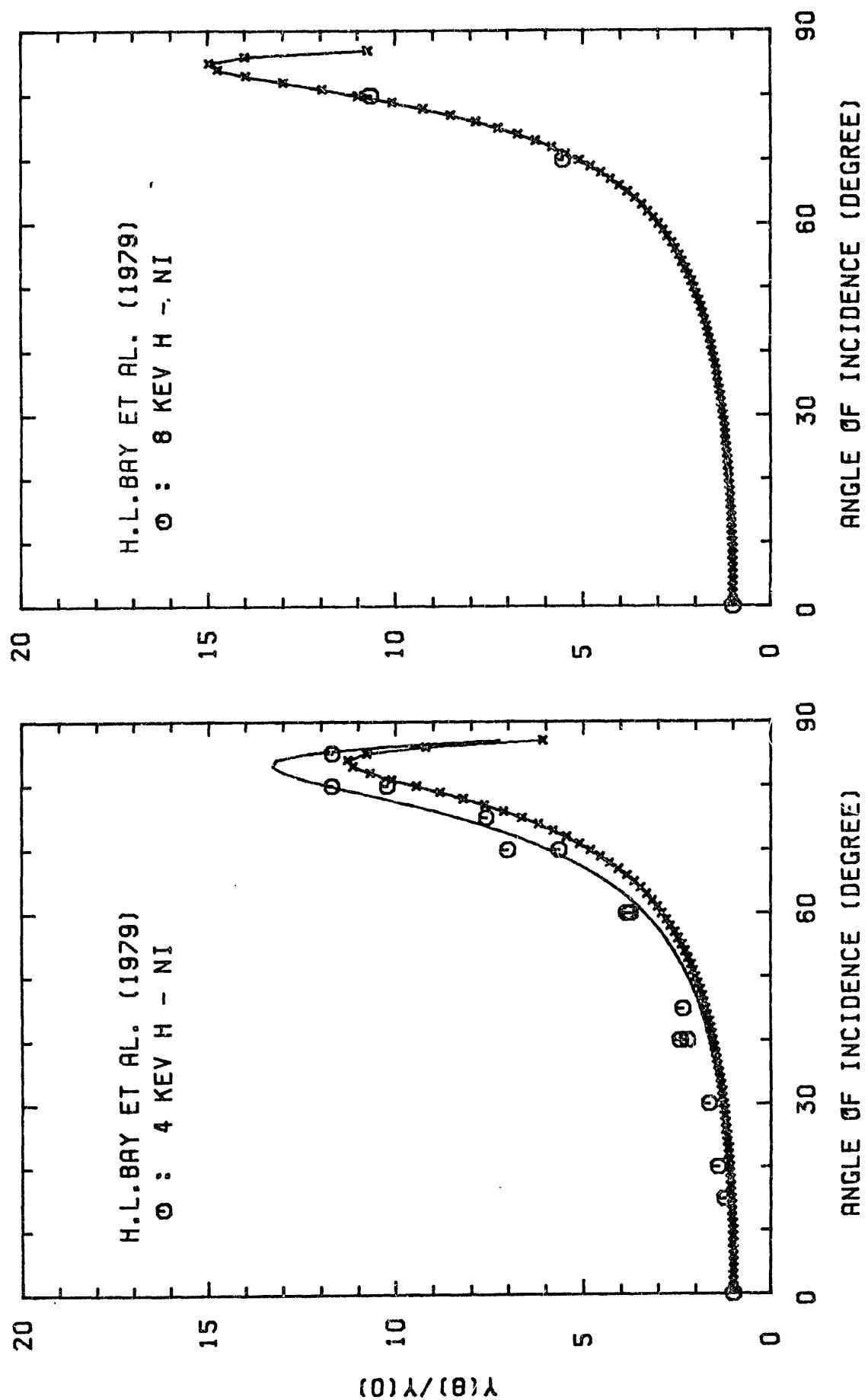


Fig. 7

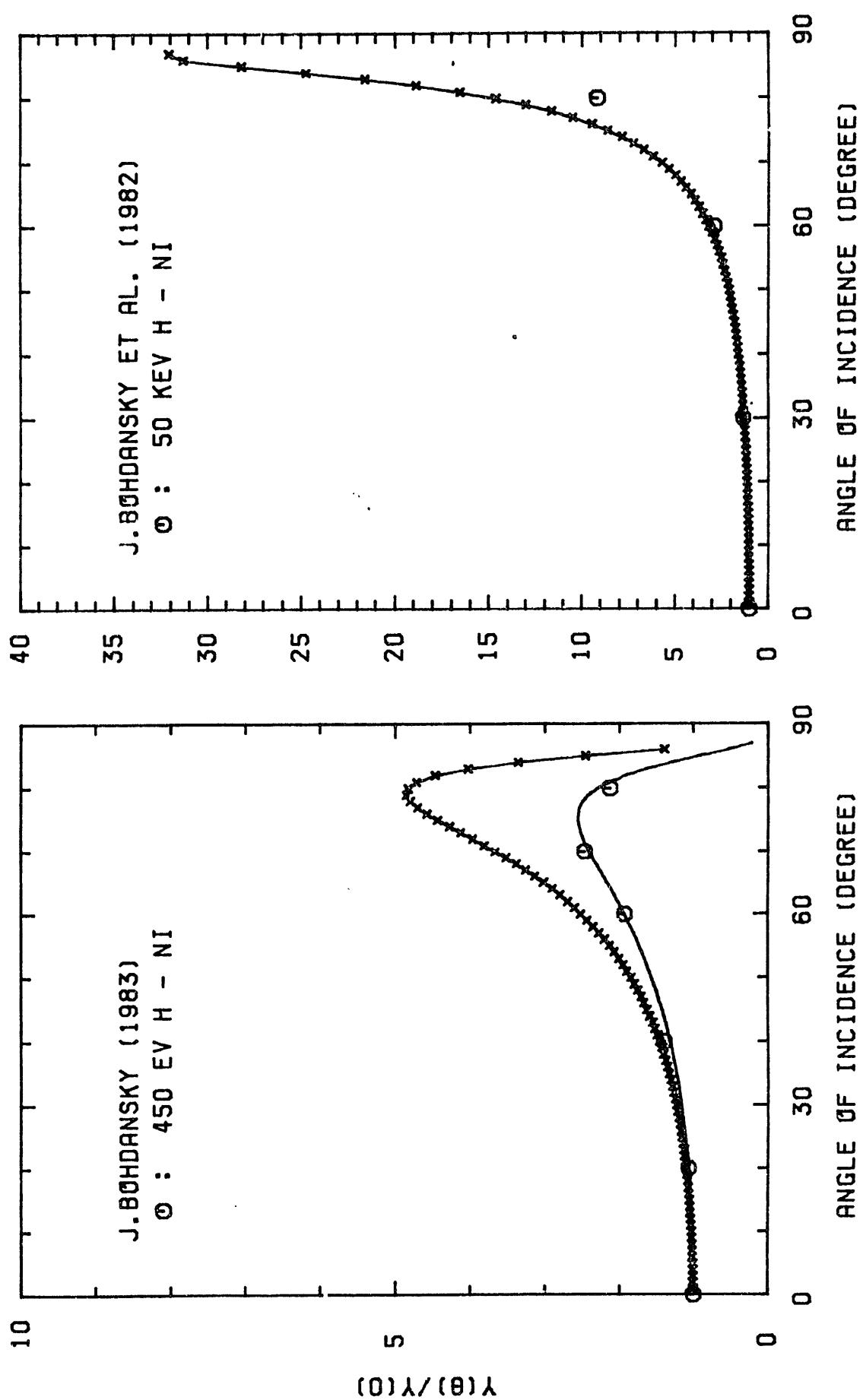


Fig. 8

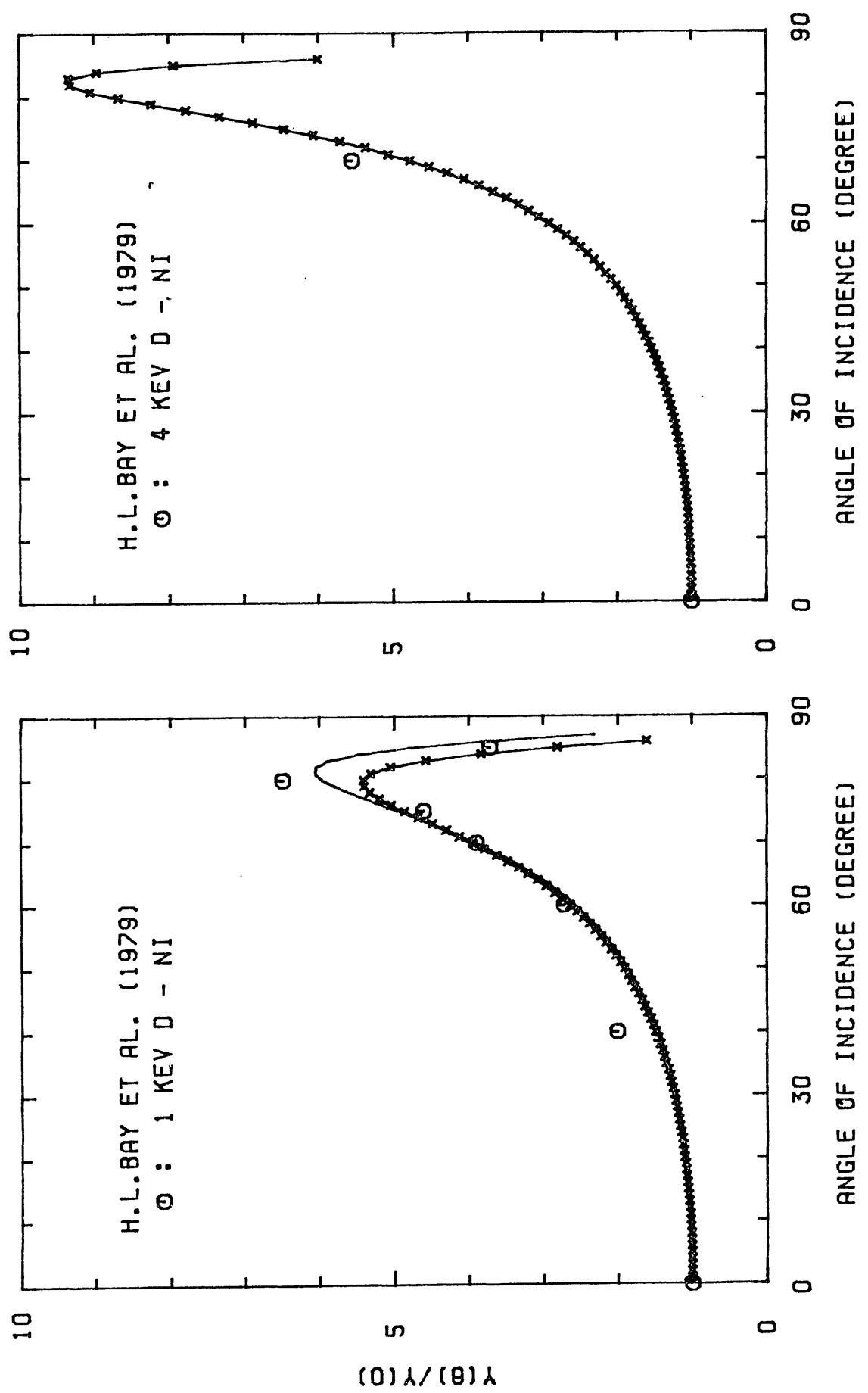


Fig. 9

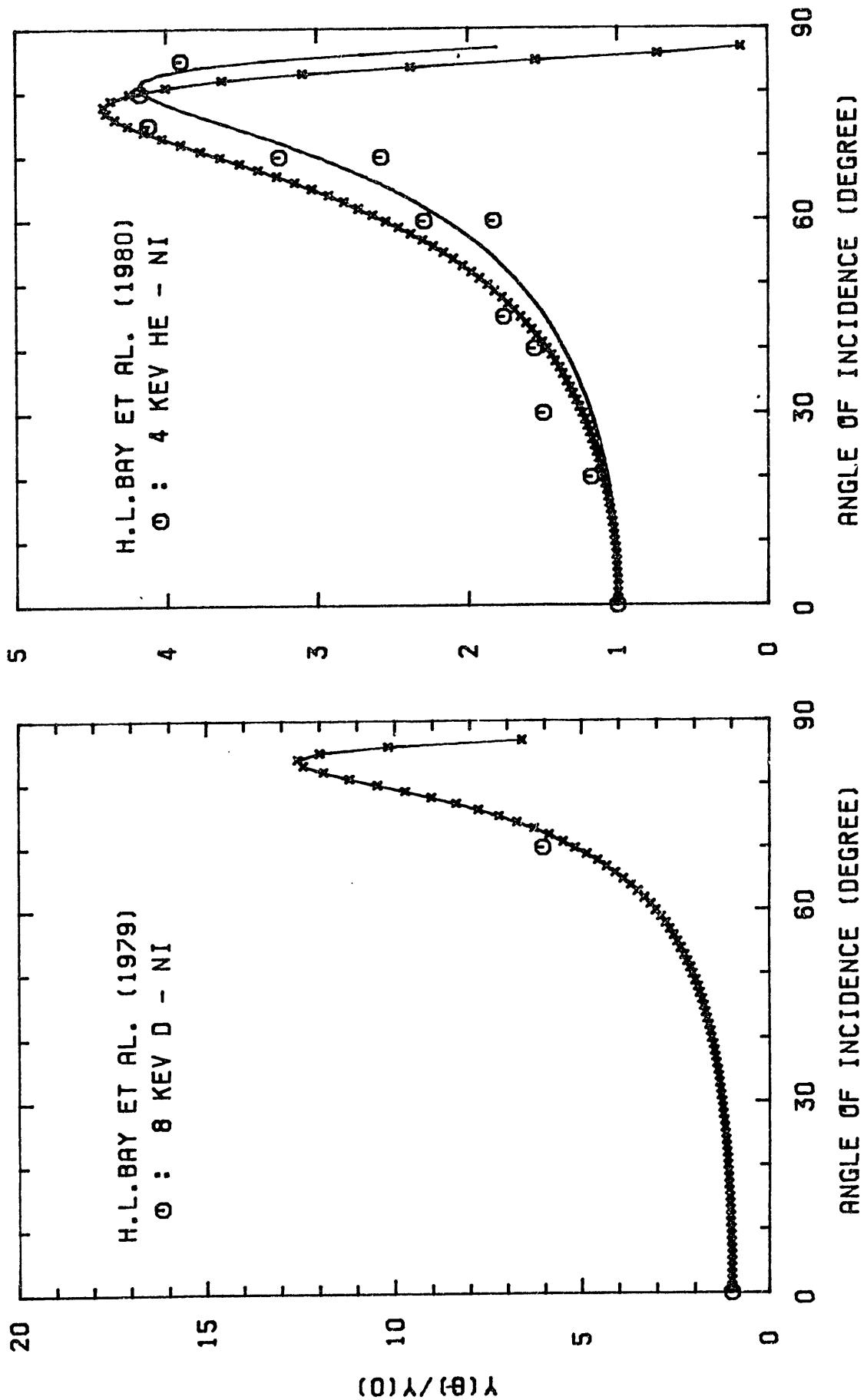


Fig. 10

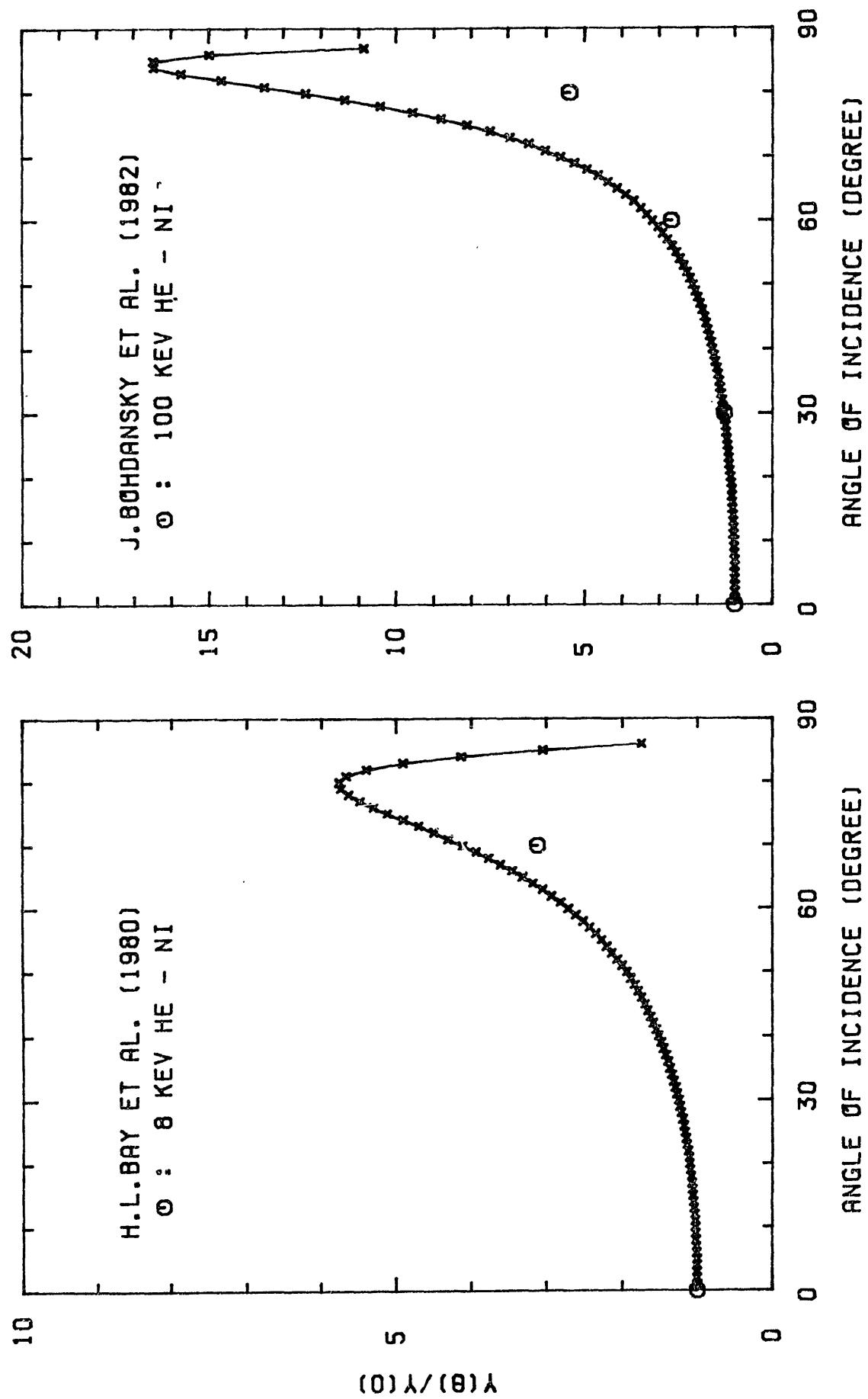


Fig. 11

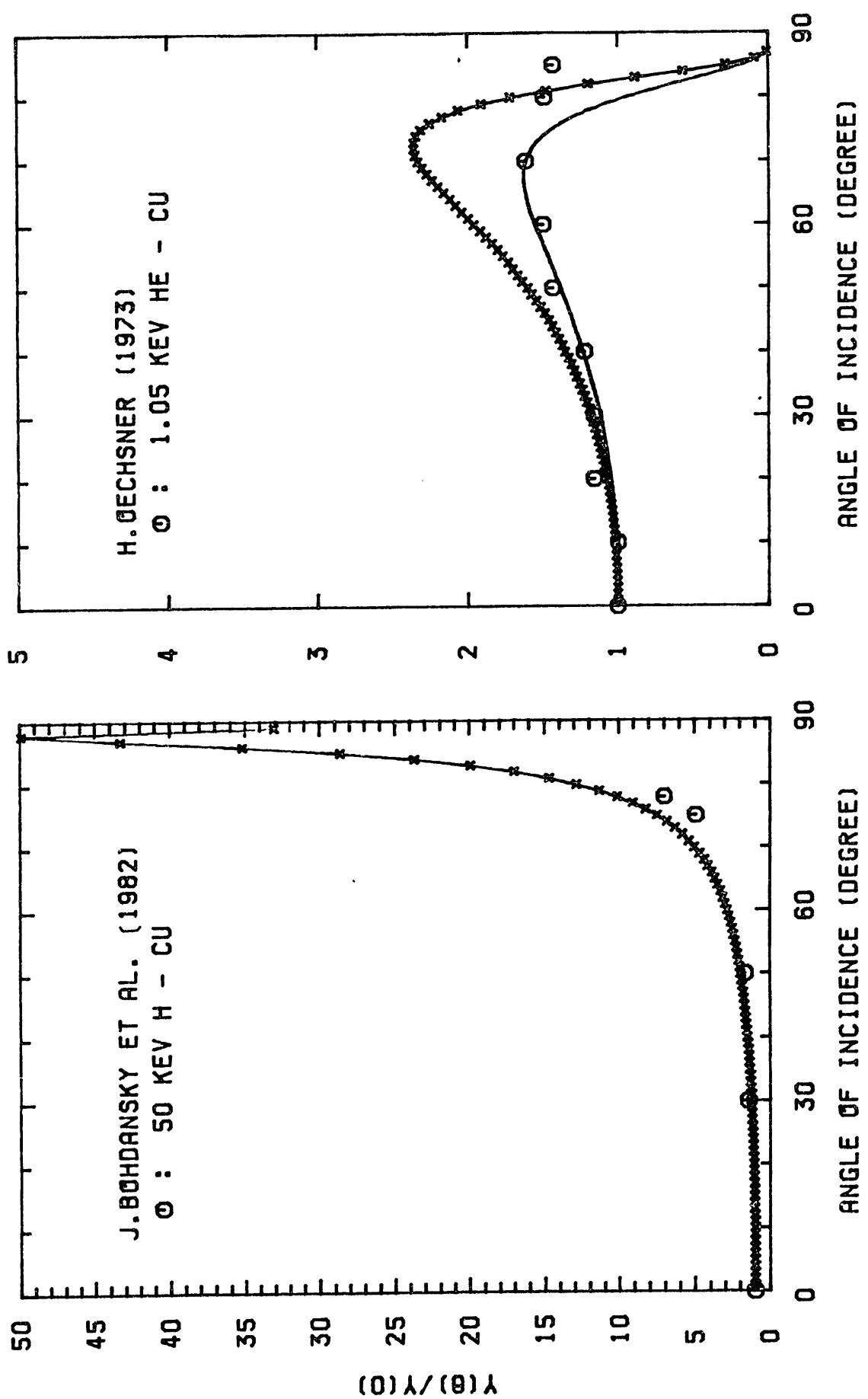


Fig. 12

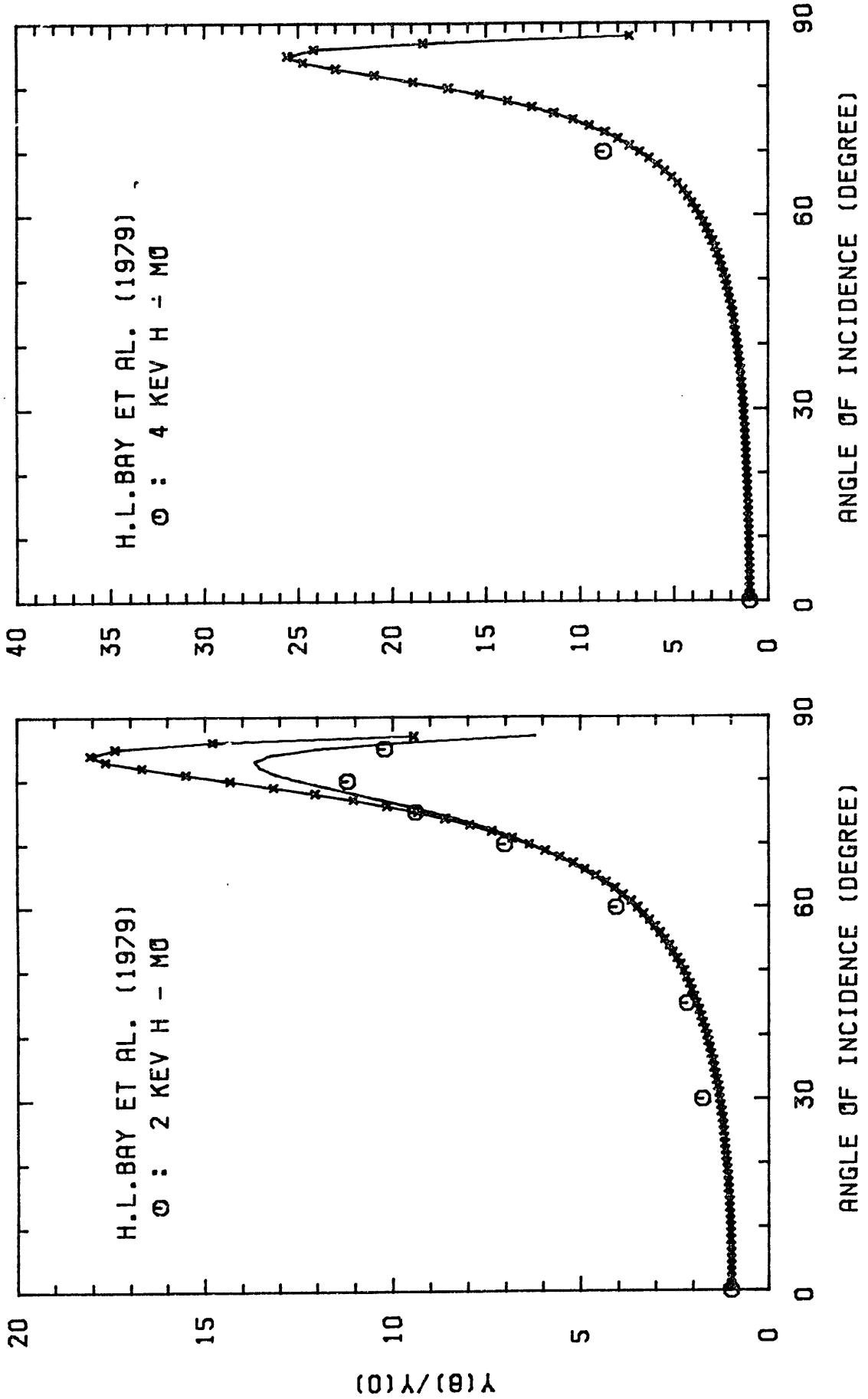


Fig. 13

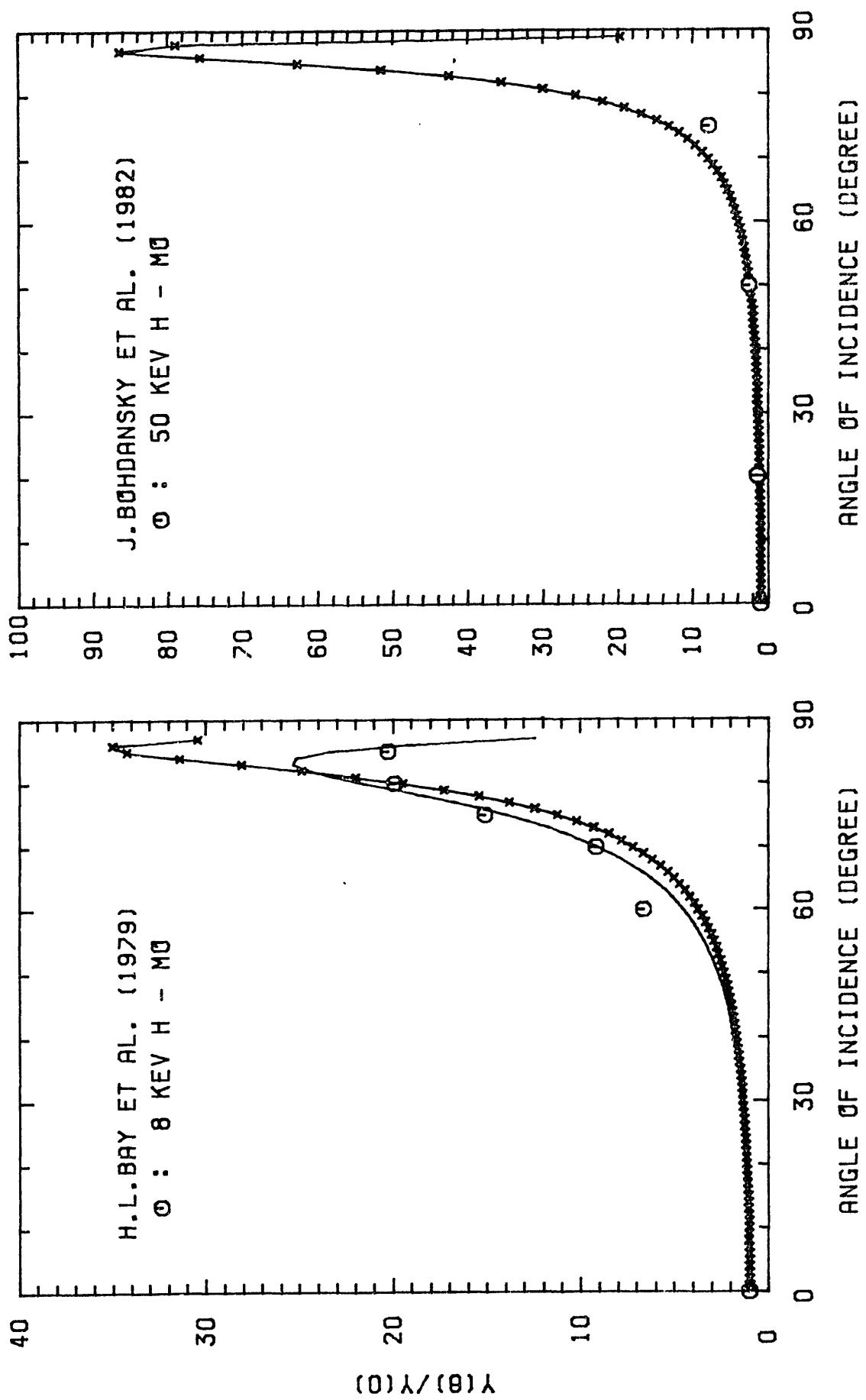


Fig. 14

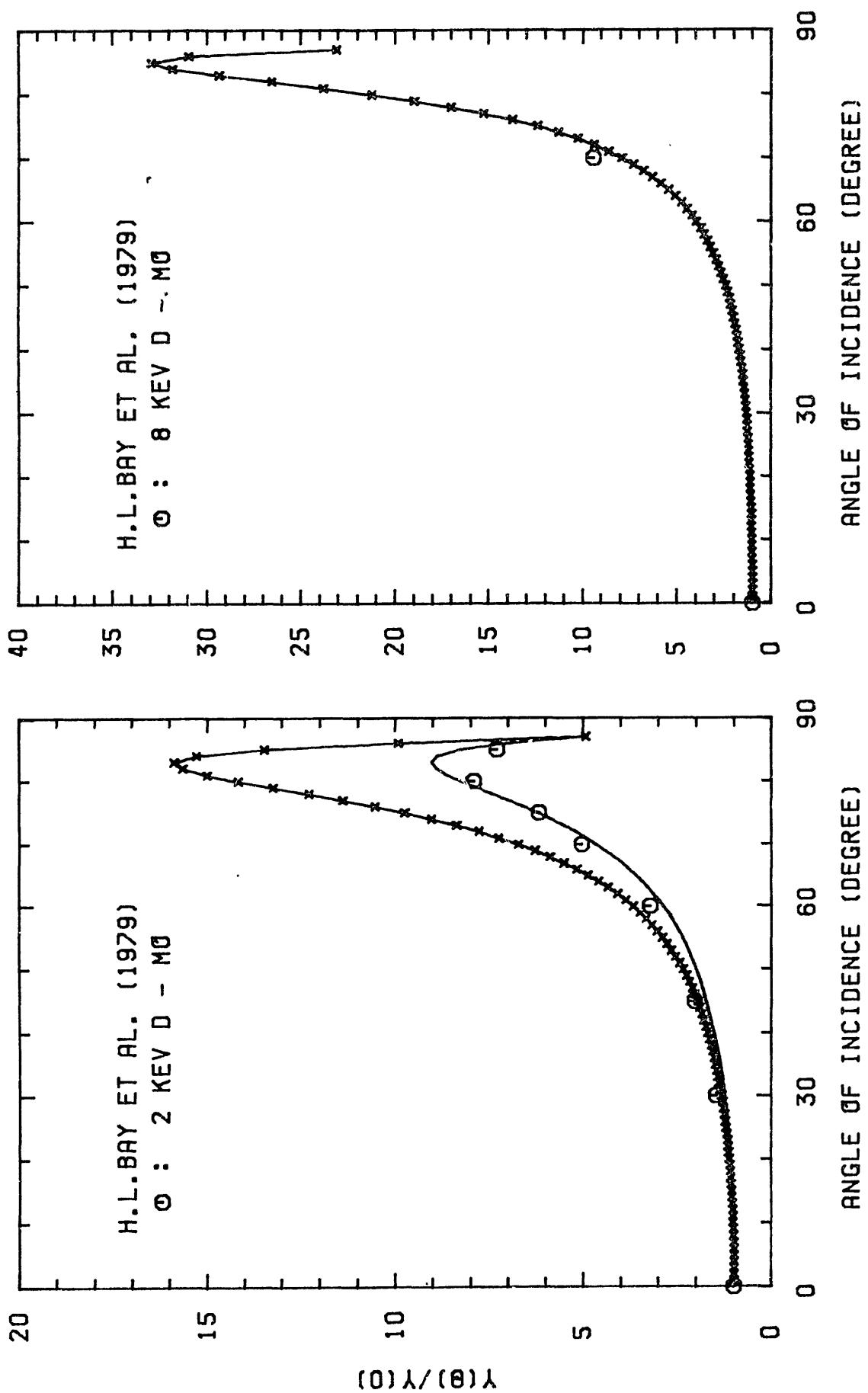


Fig. 15

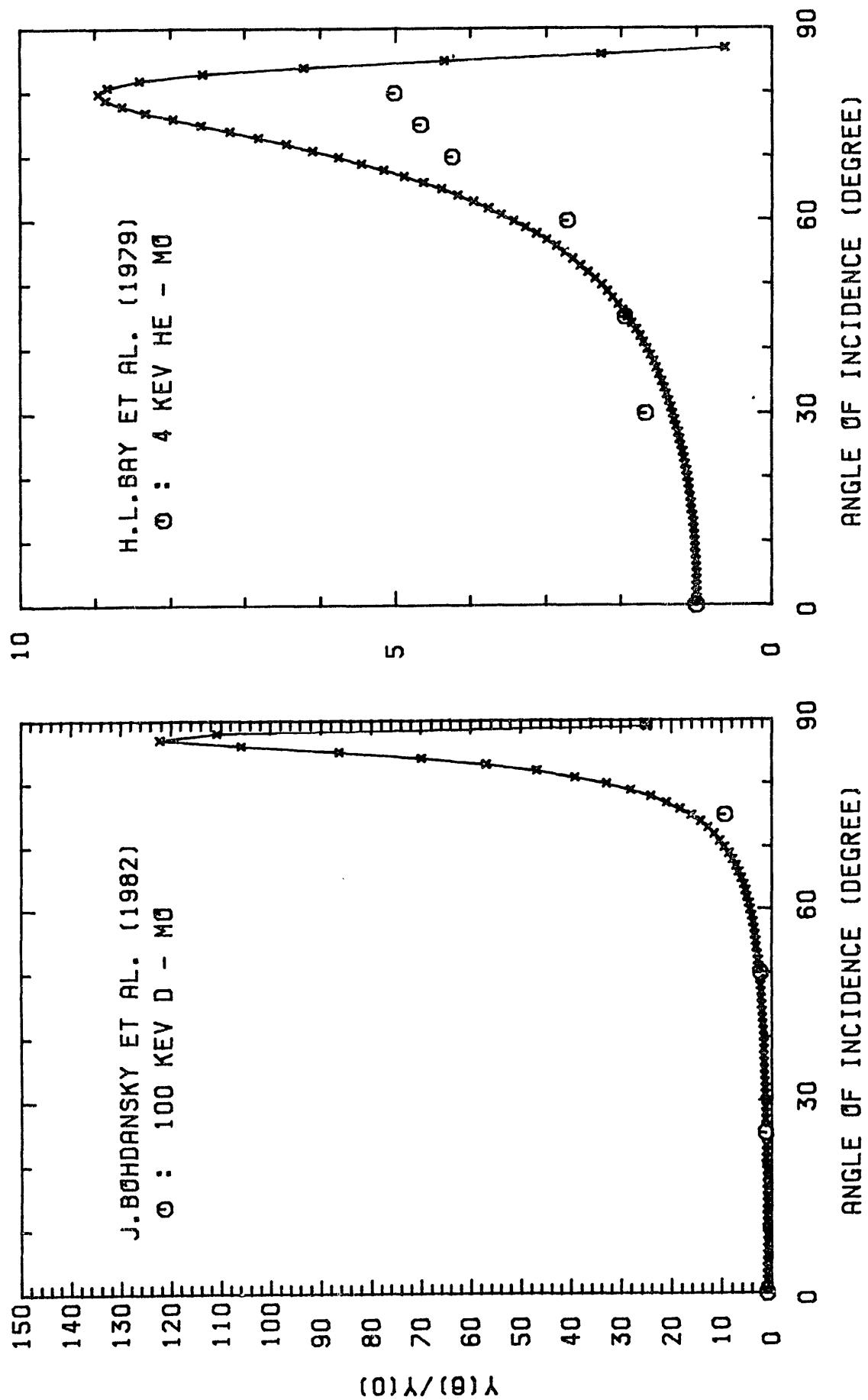


Fig. 16

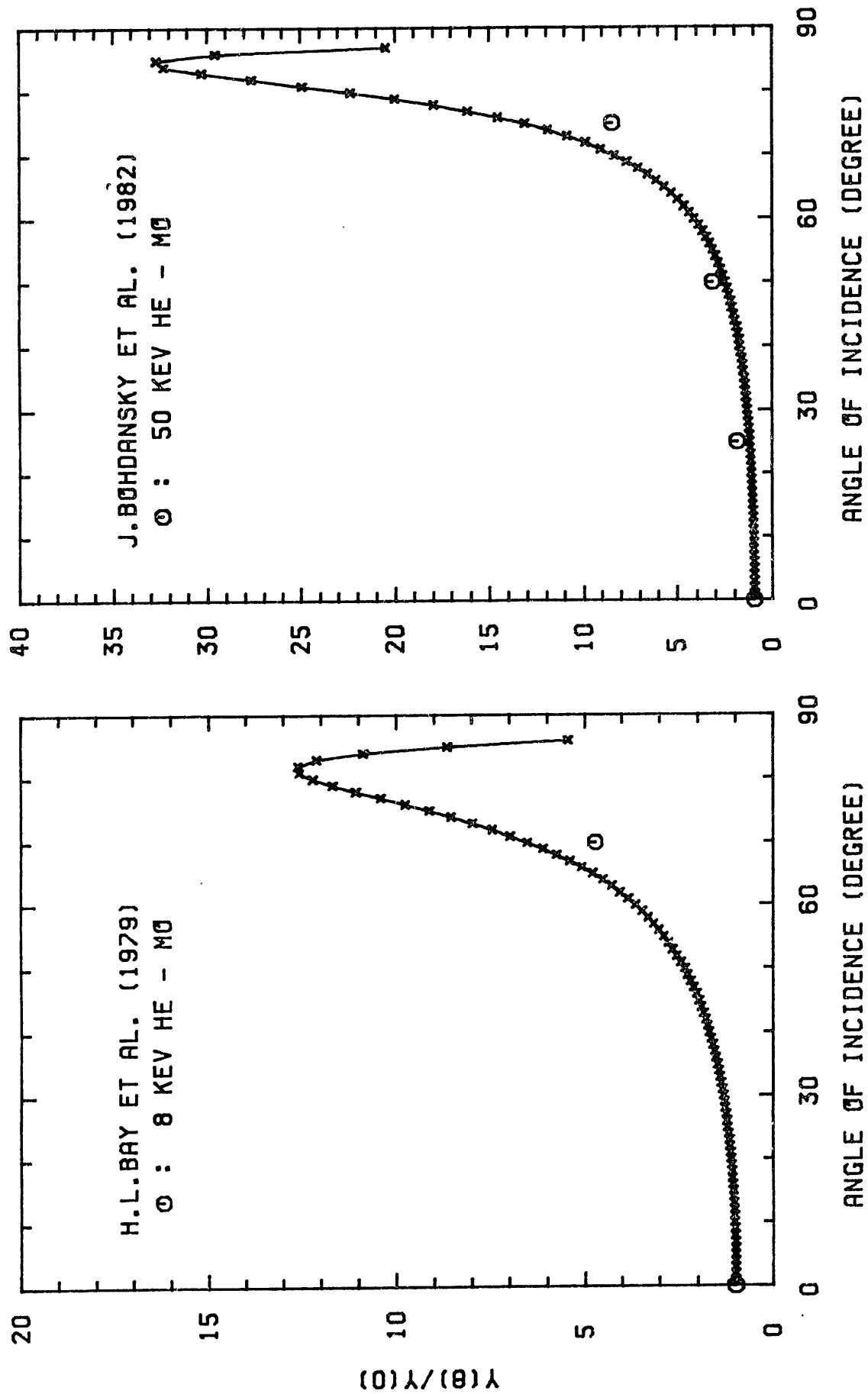


Fig. 17

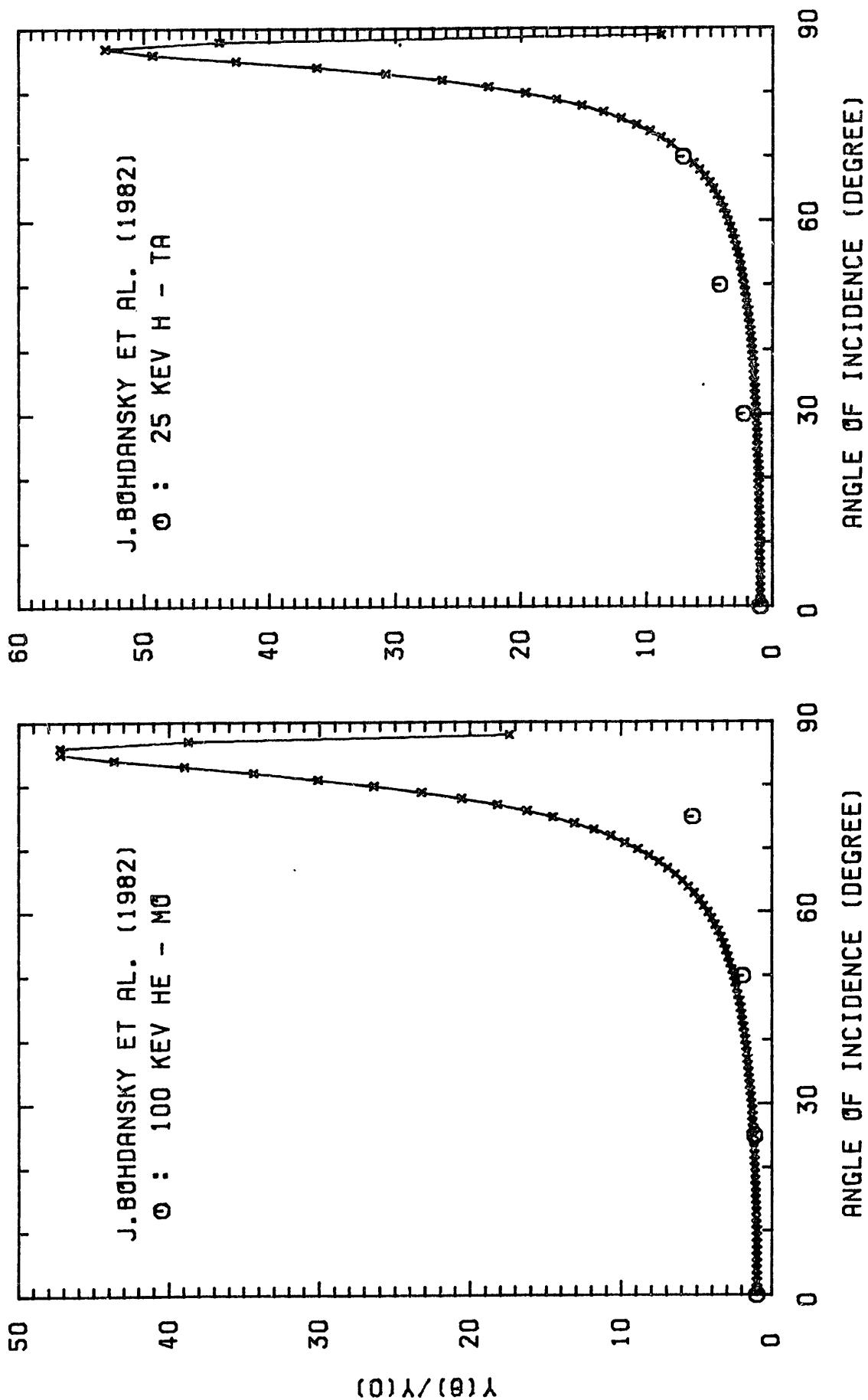


Fig. 18

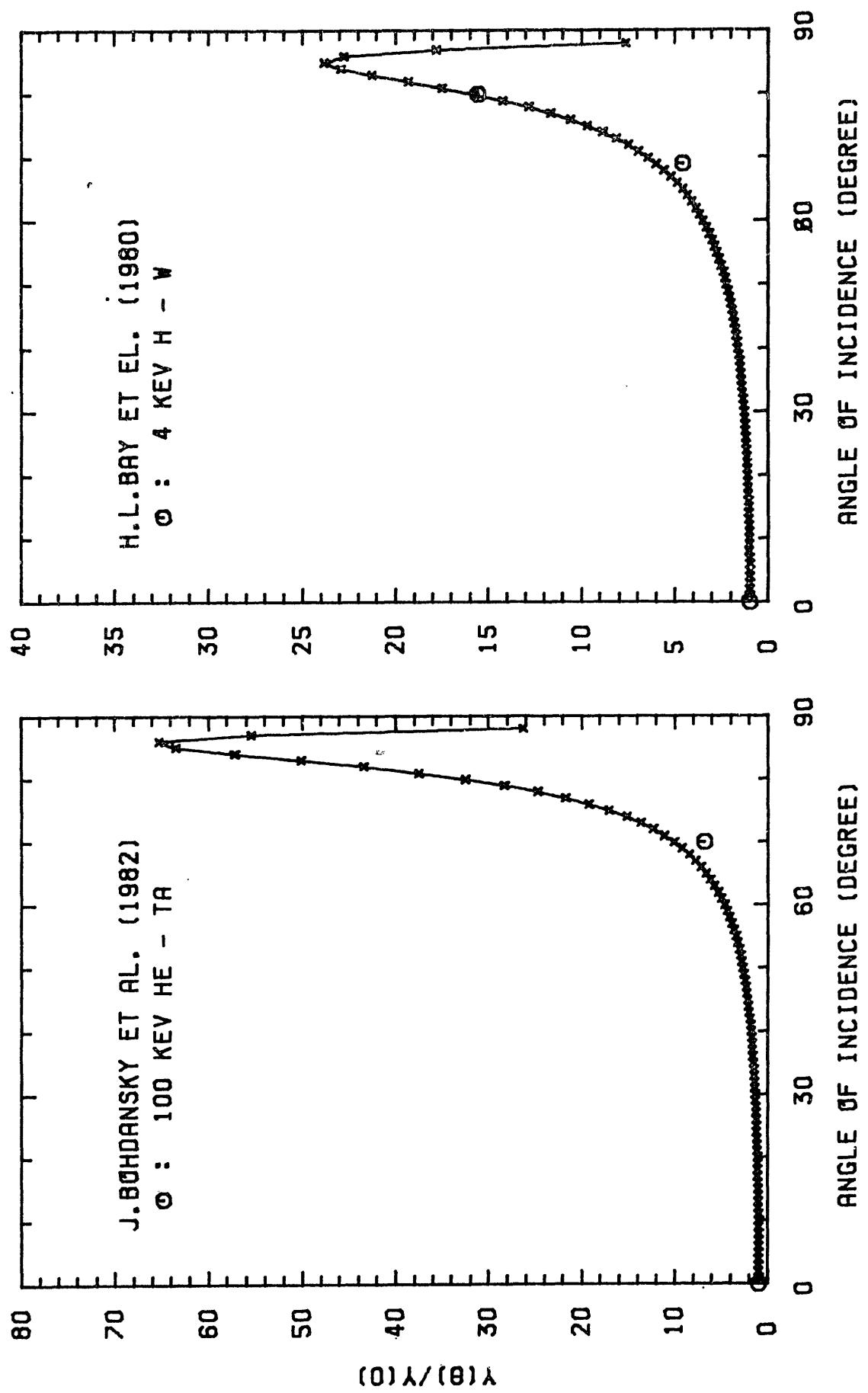


Fig. 19

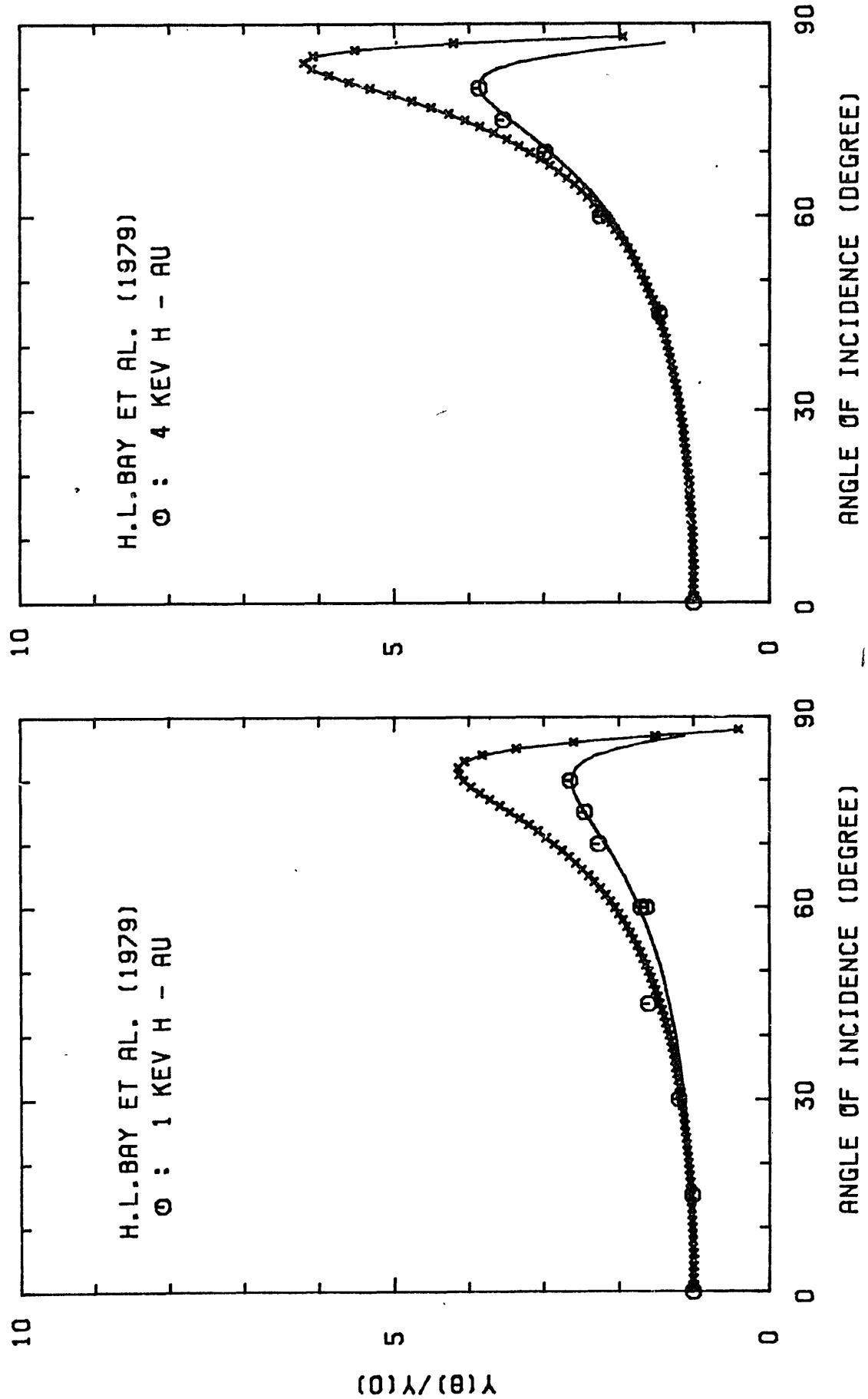


Fig. 20

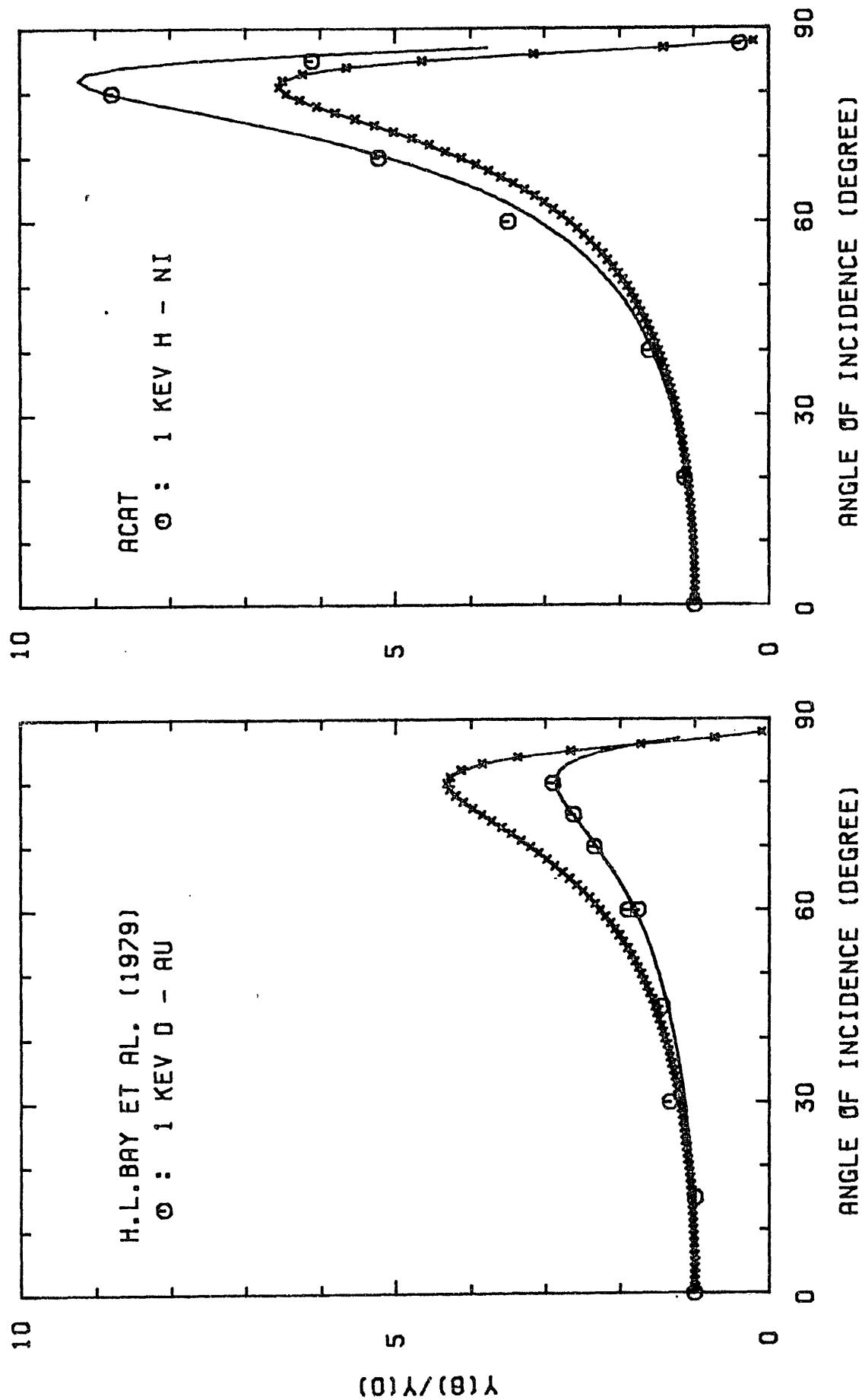


Fig. 21

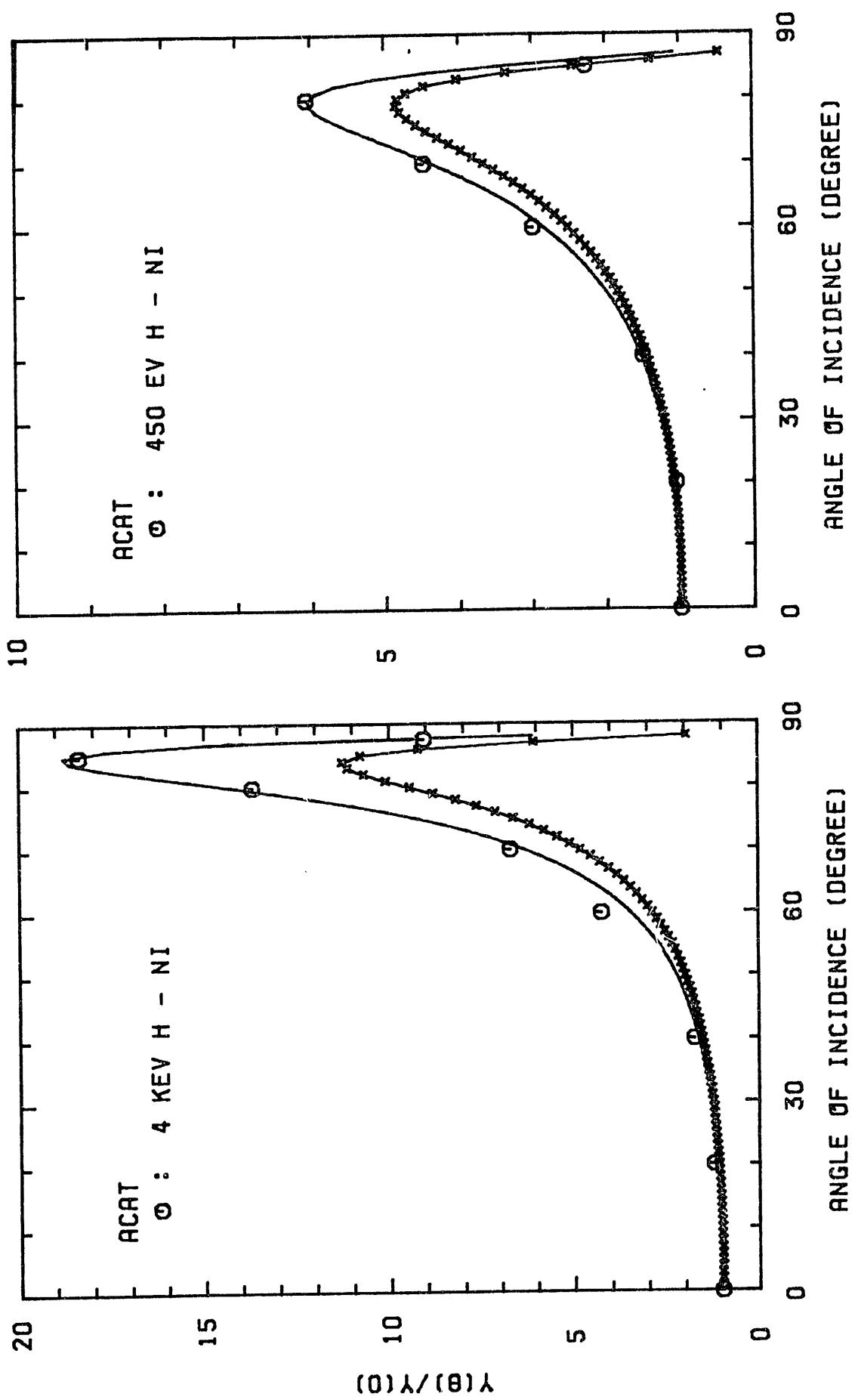


Fig. 22

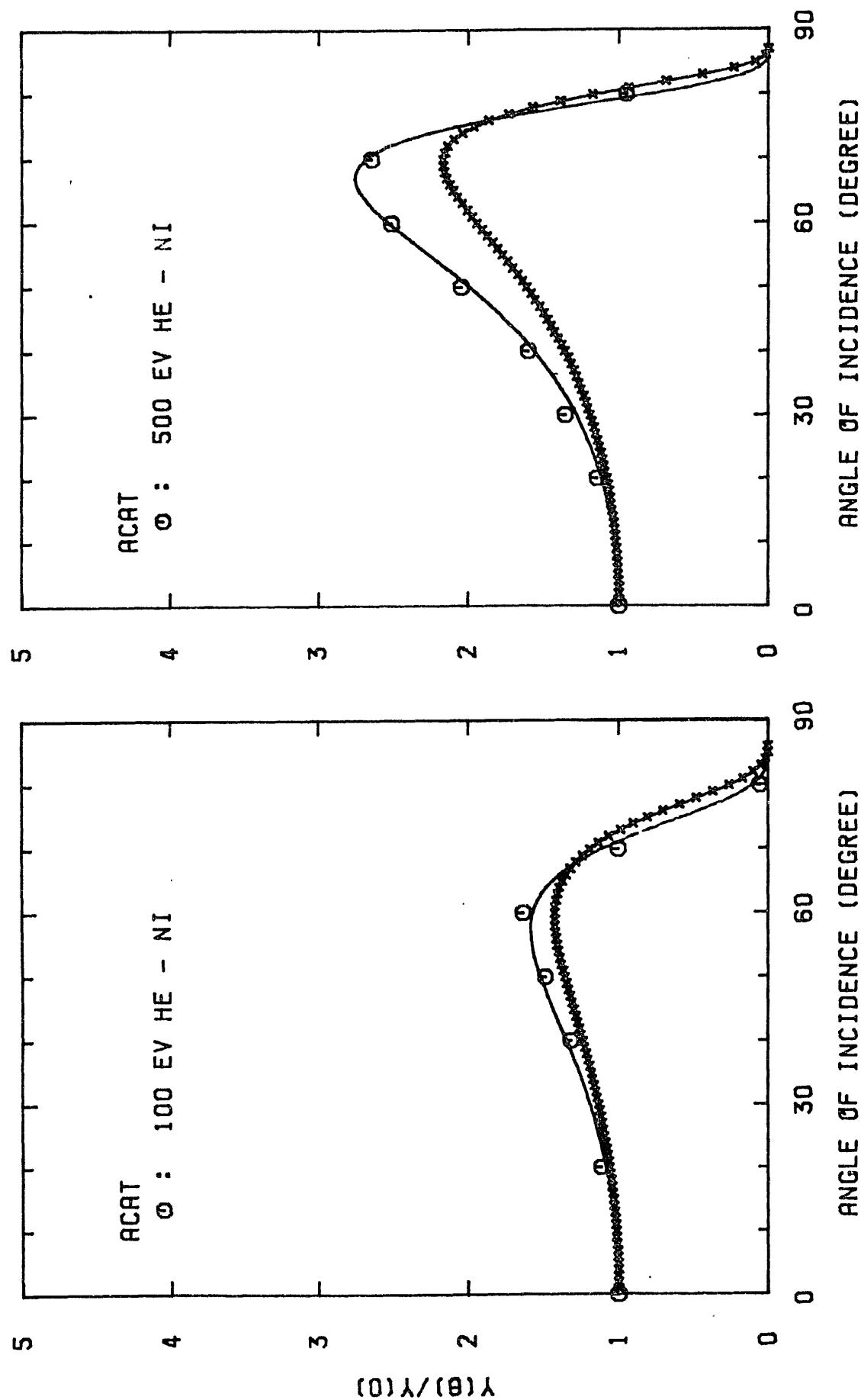


Fig. 23

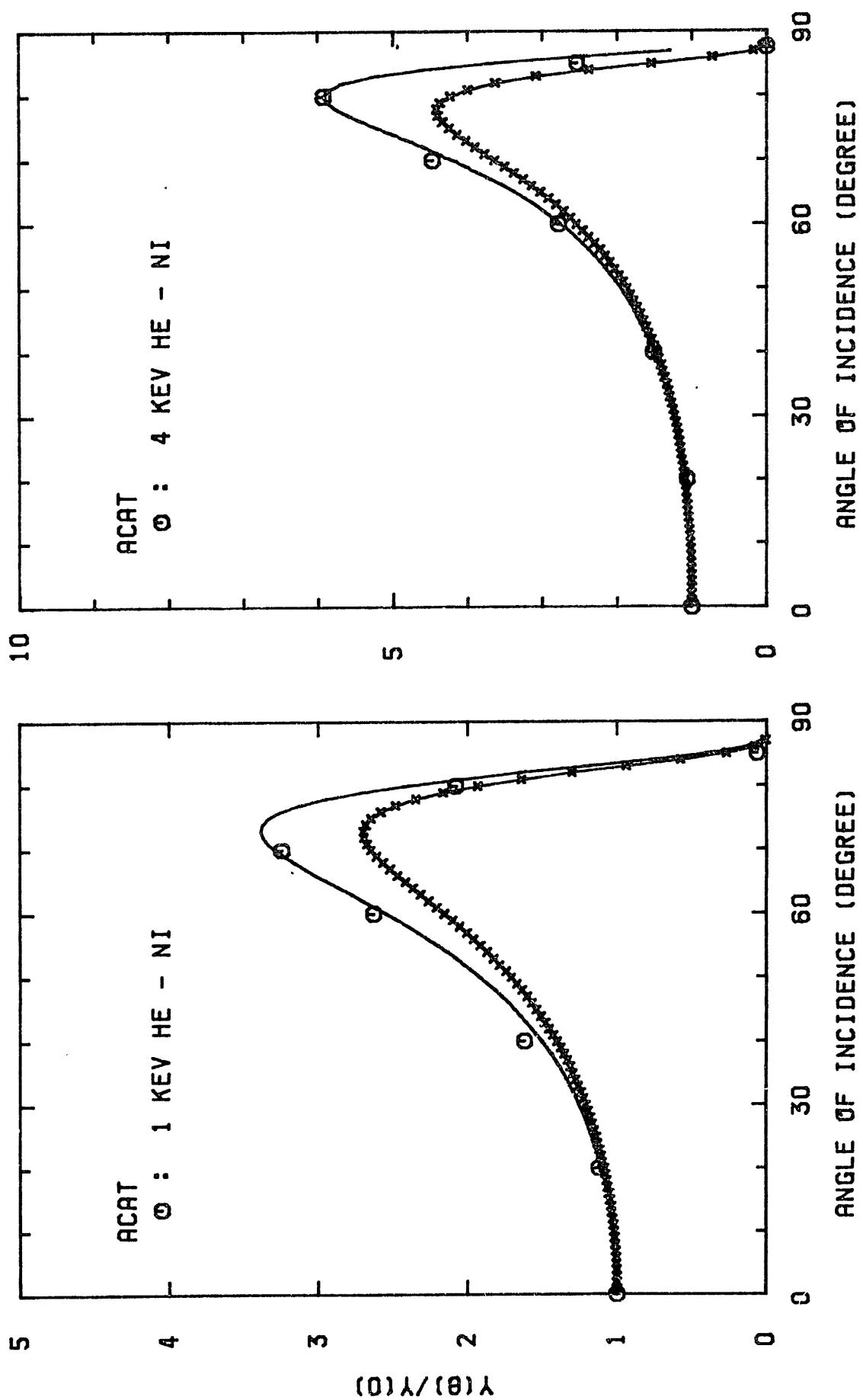


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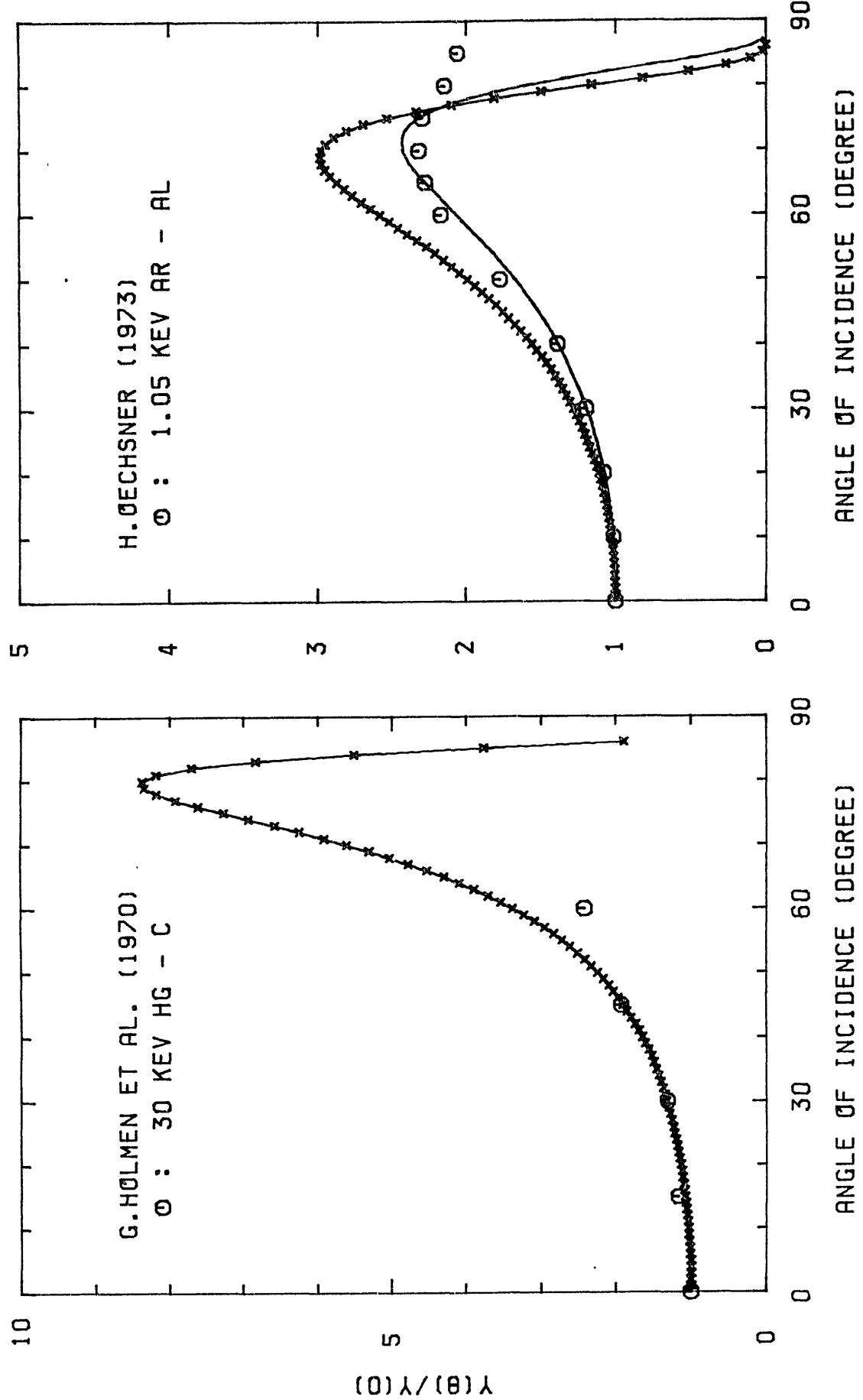


Fig. 25

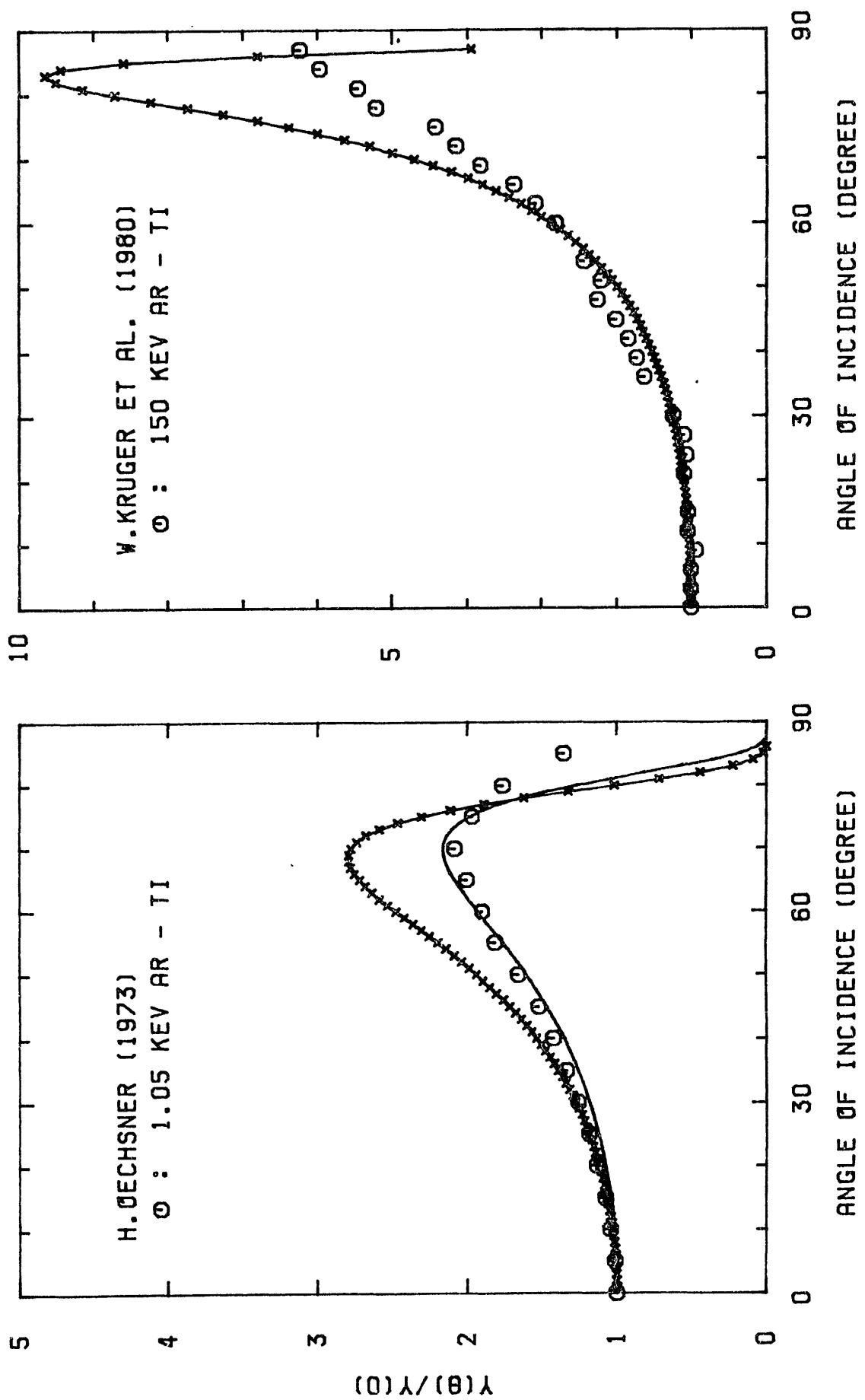


Fig. 26

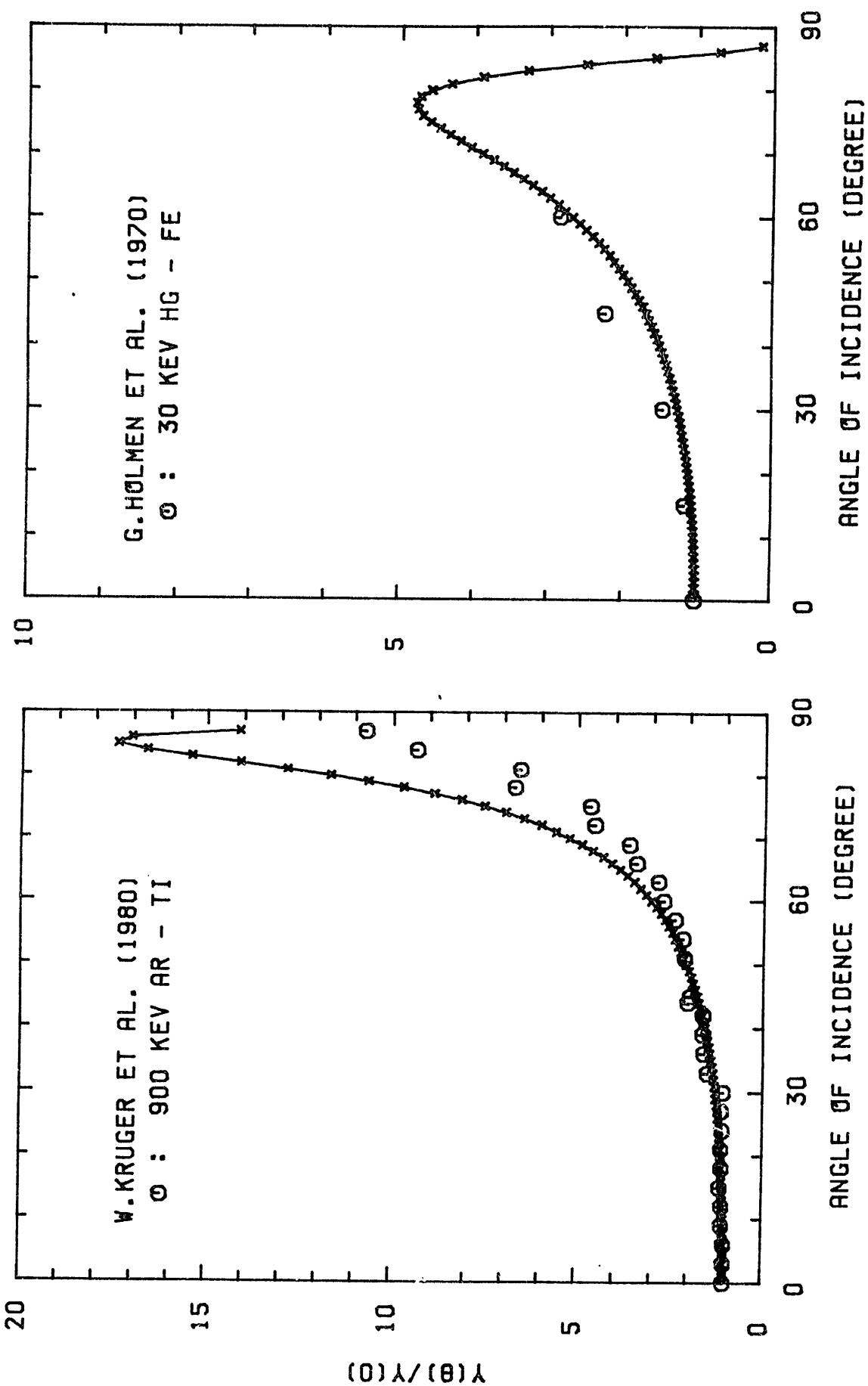


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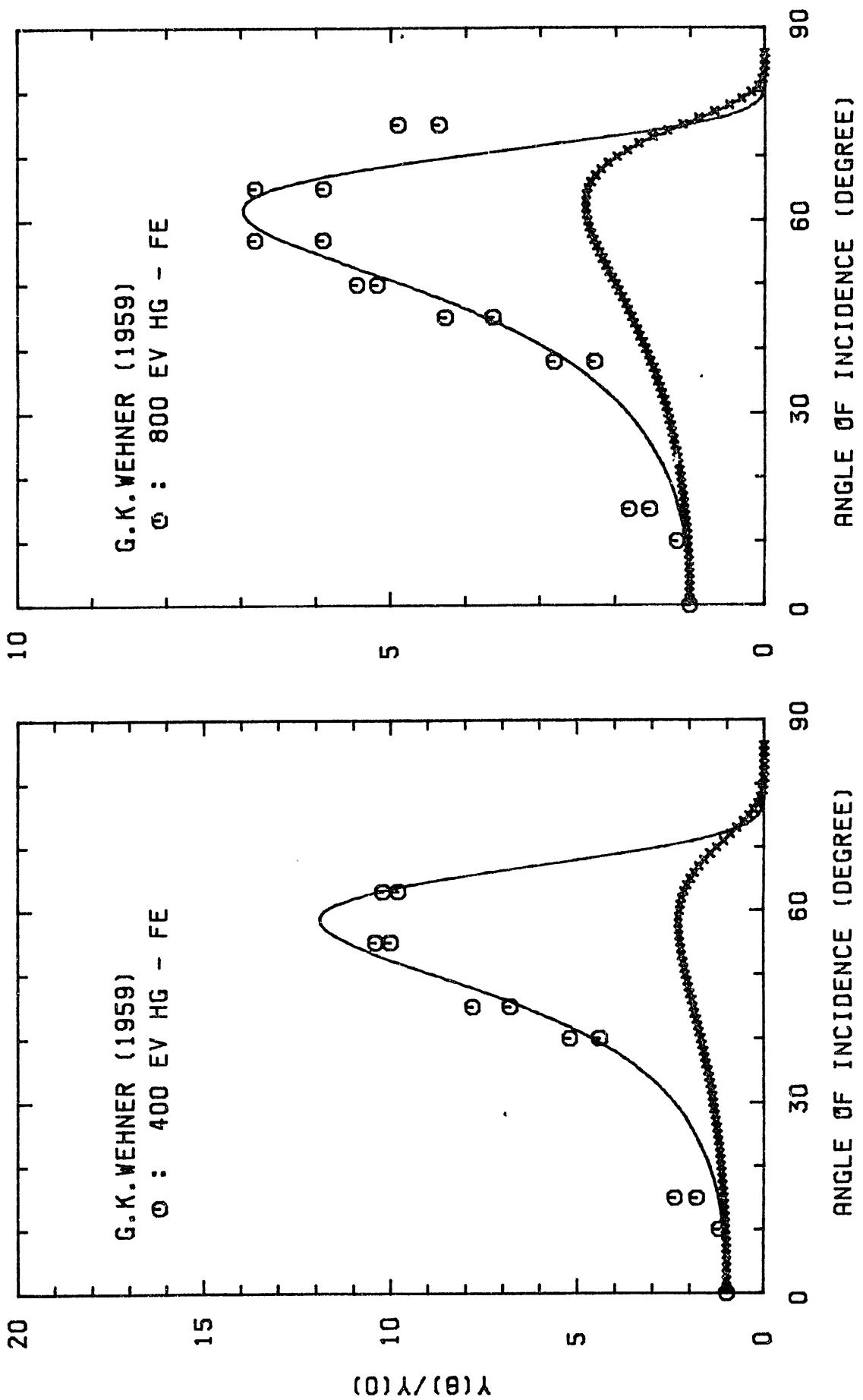


Fig. 28

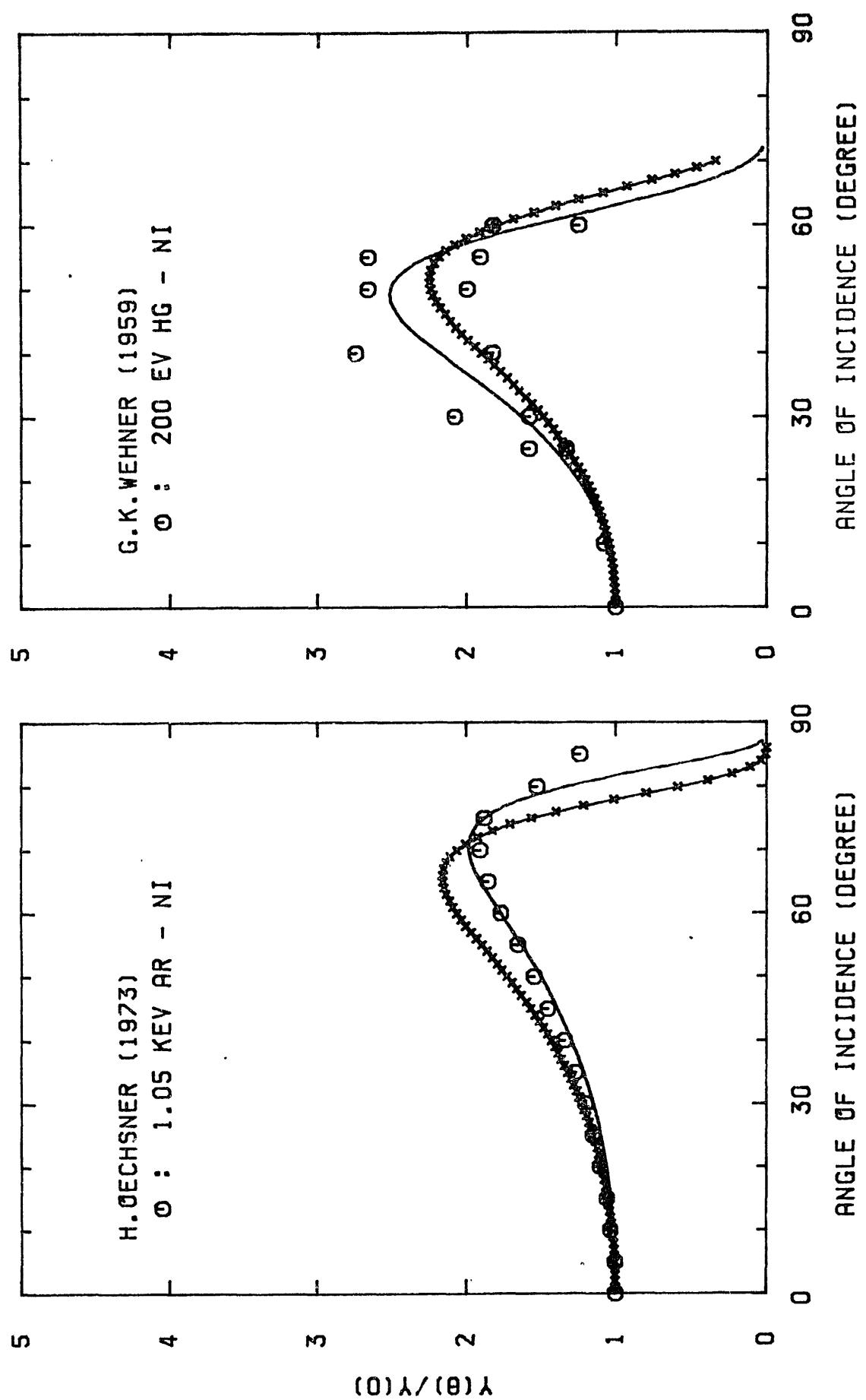


Fig. 29

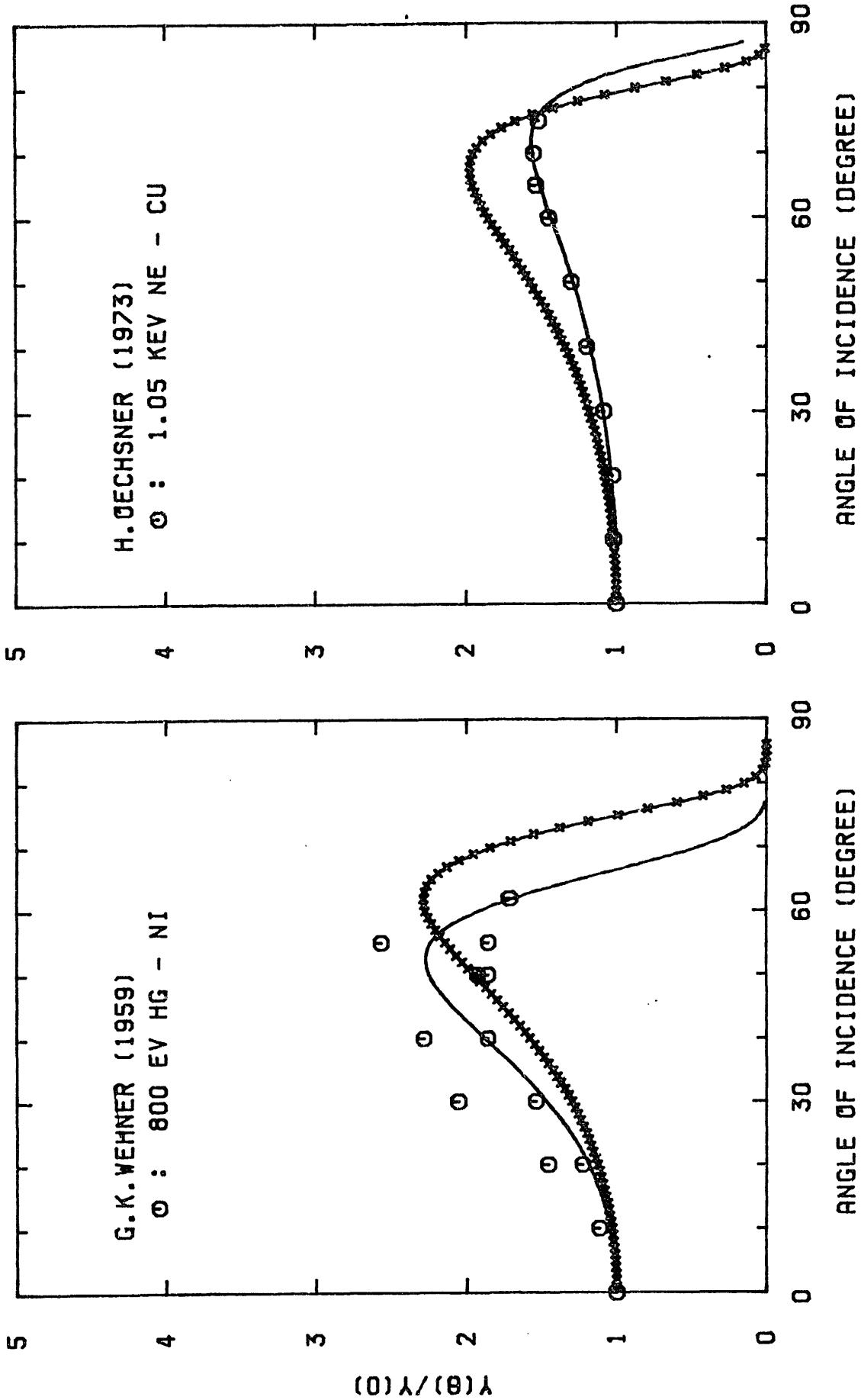


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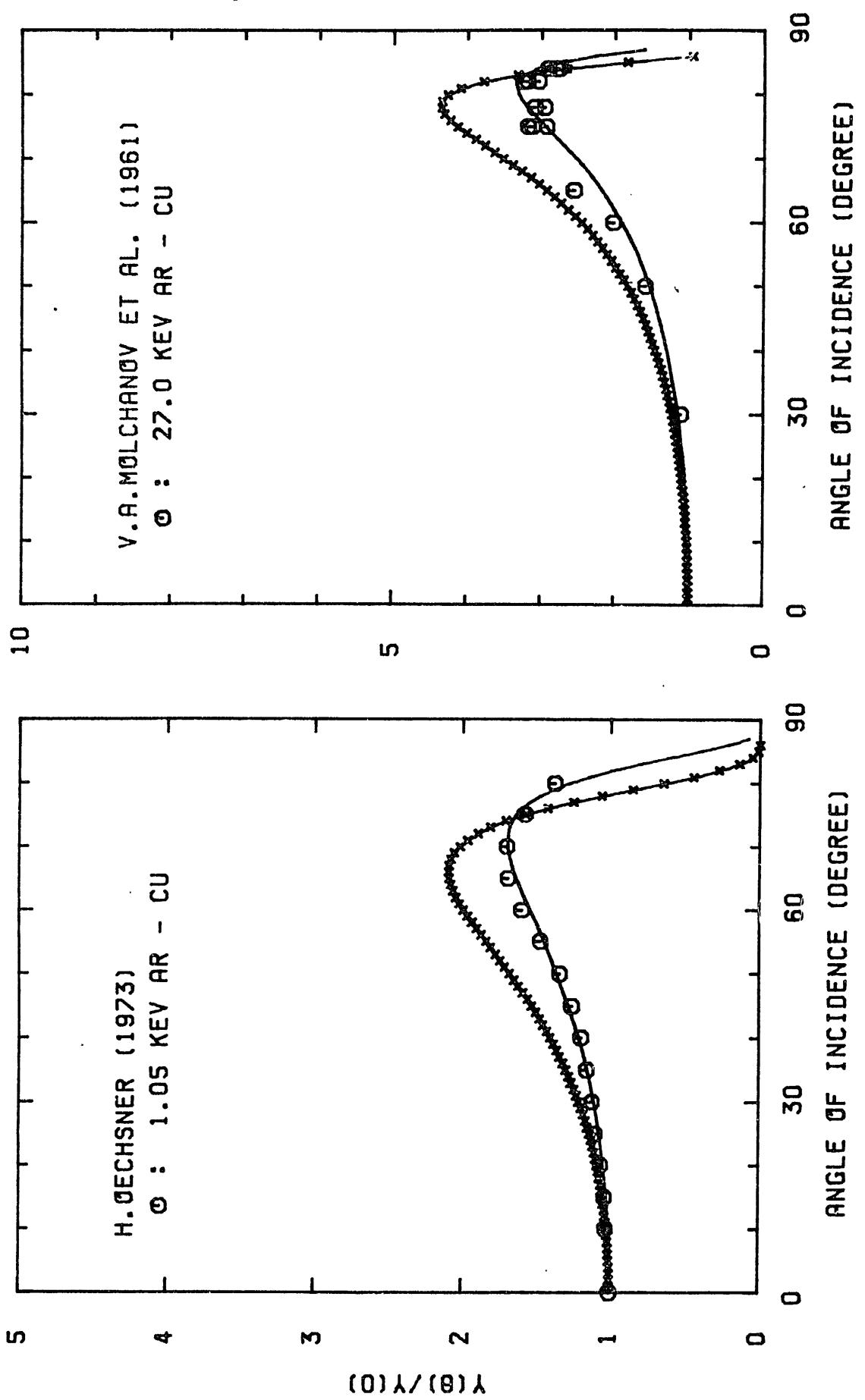


Fig. 31

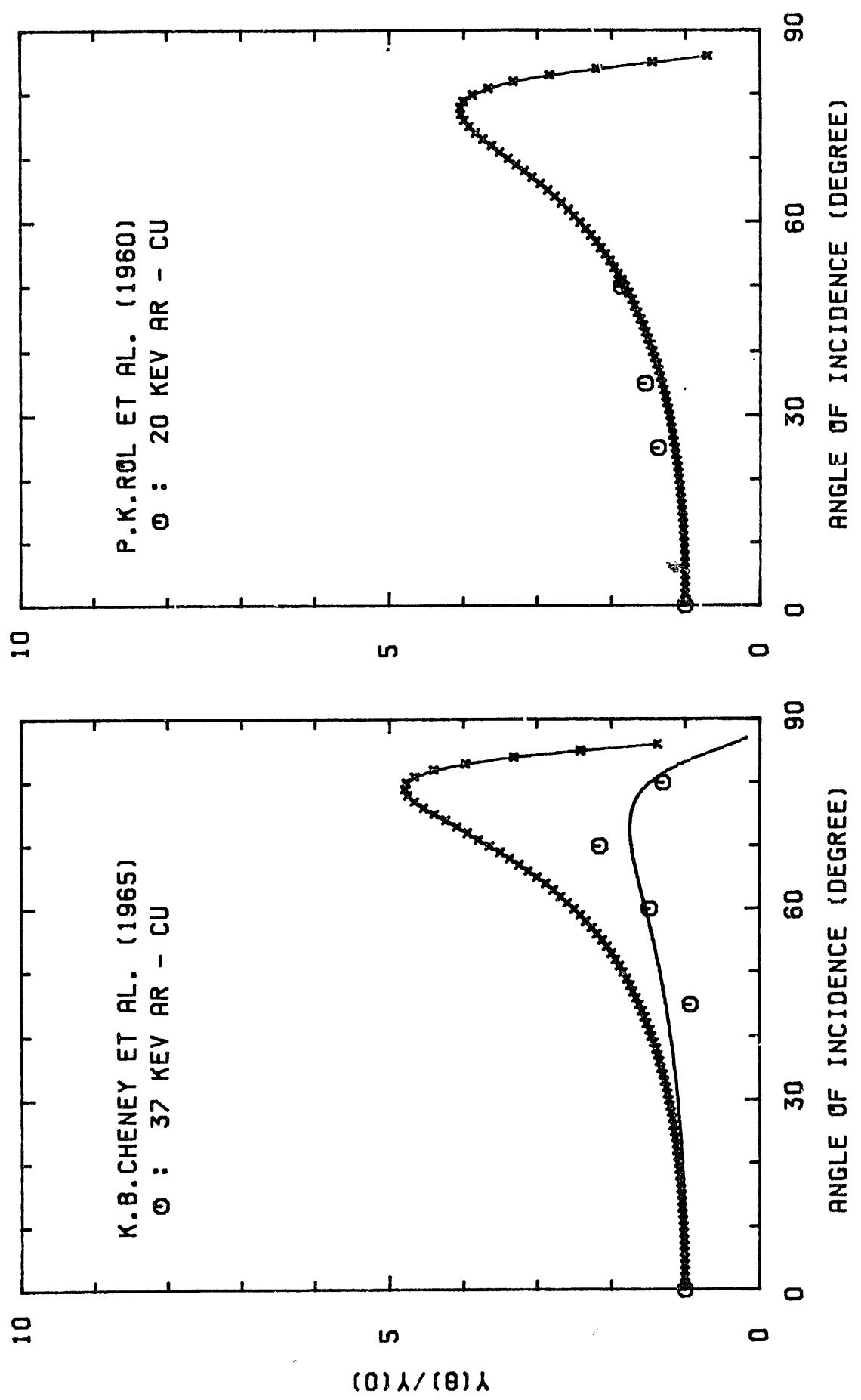
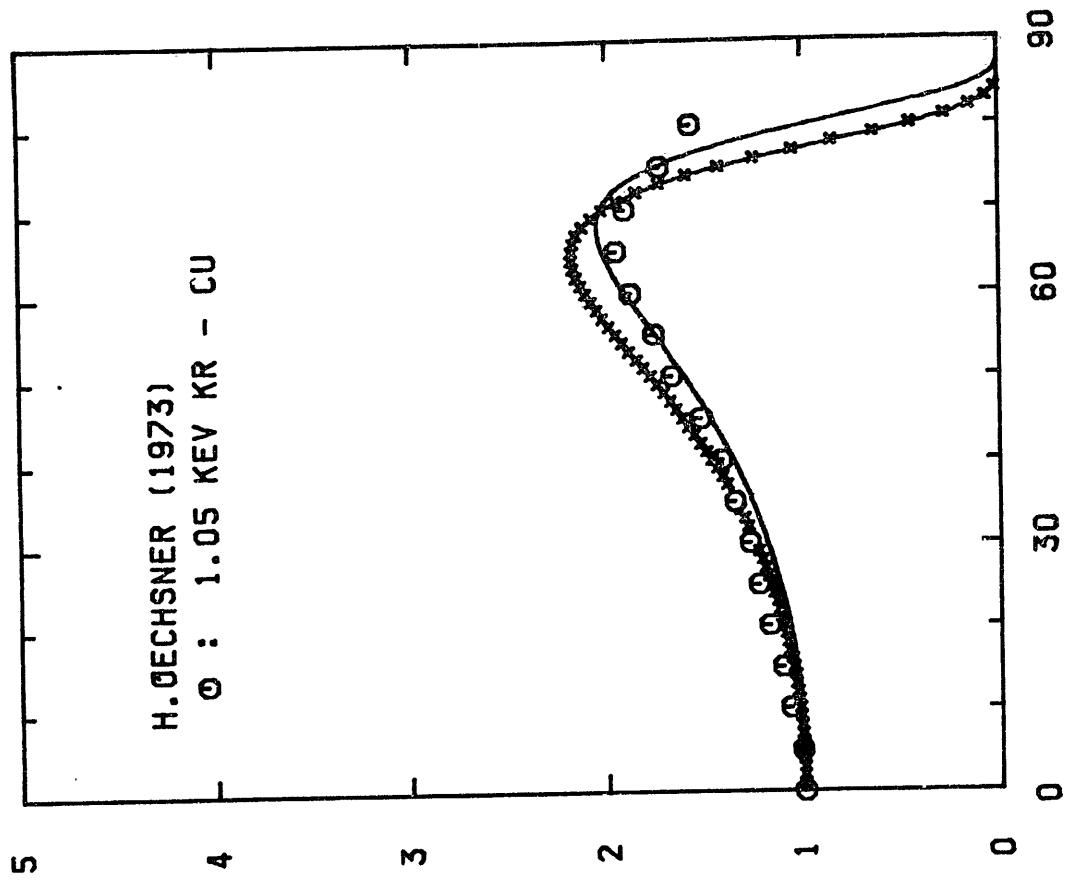


Fig. 32

H. OECHSNER (1973)

$\Theta$  : 1.05 KEV KR - CU



G. DUPP ET AL. (1966)

$\Theta$  : 100 KEV AR - CU

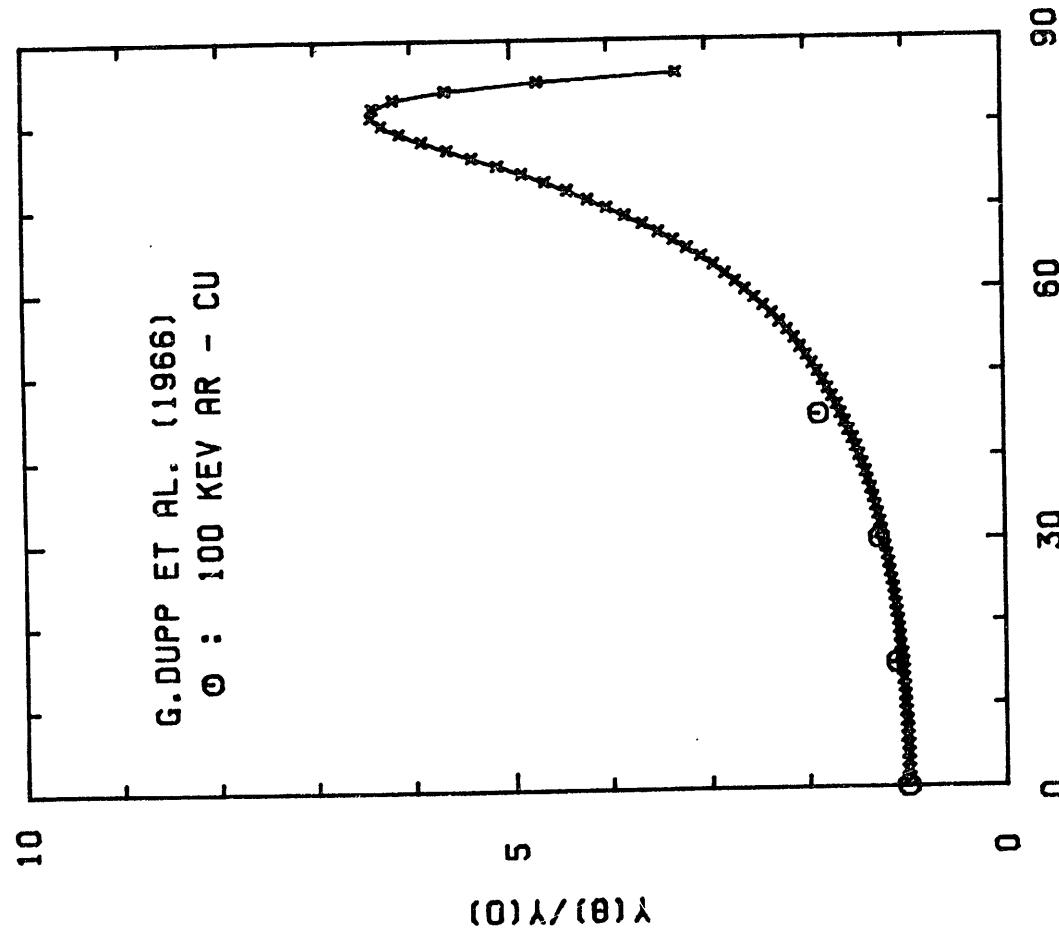


Fig. 33

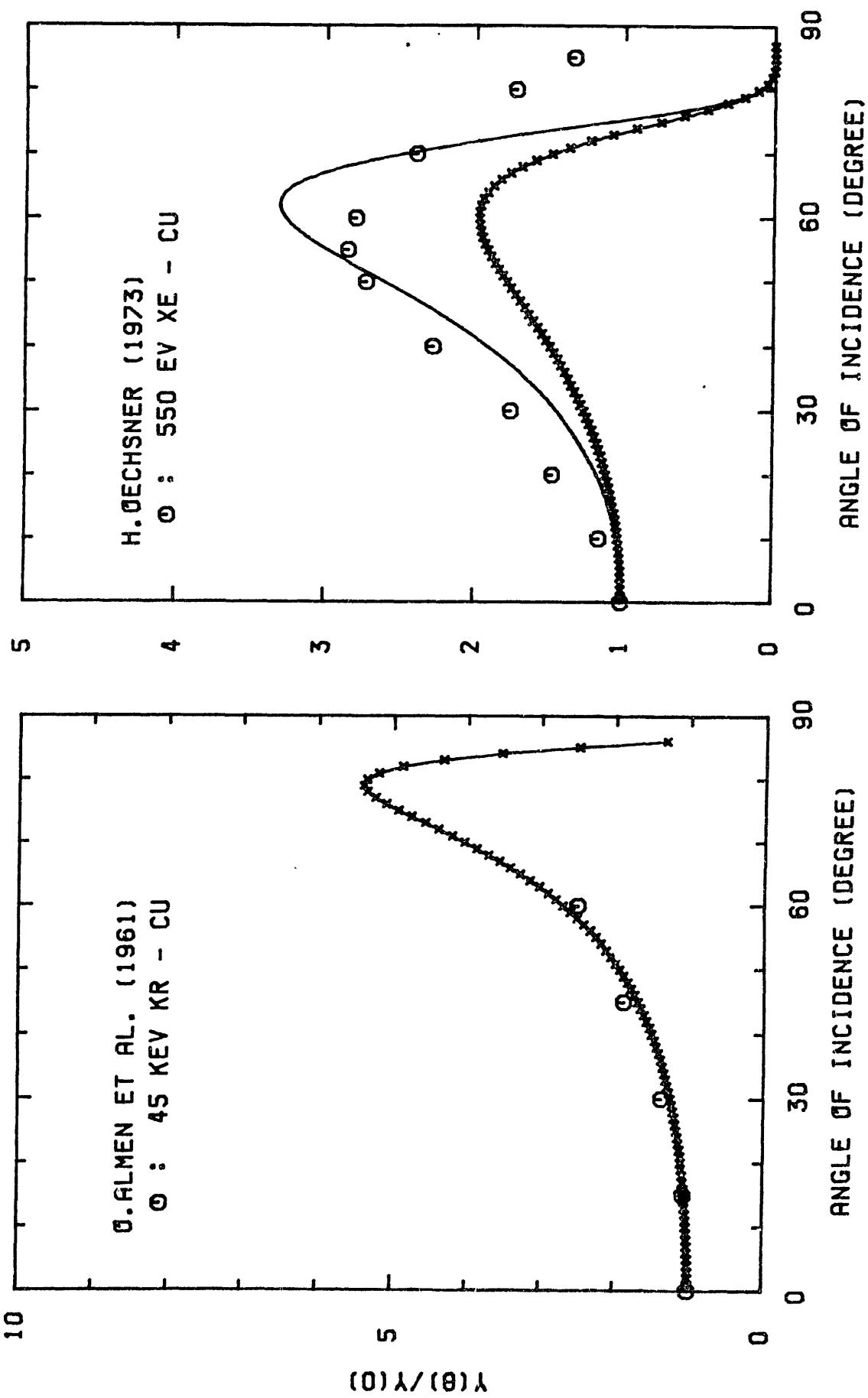


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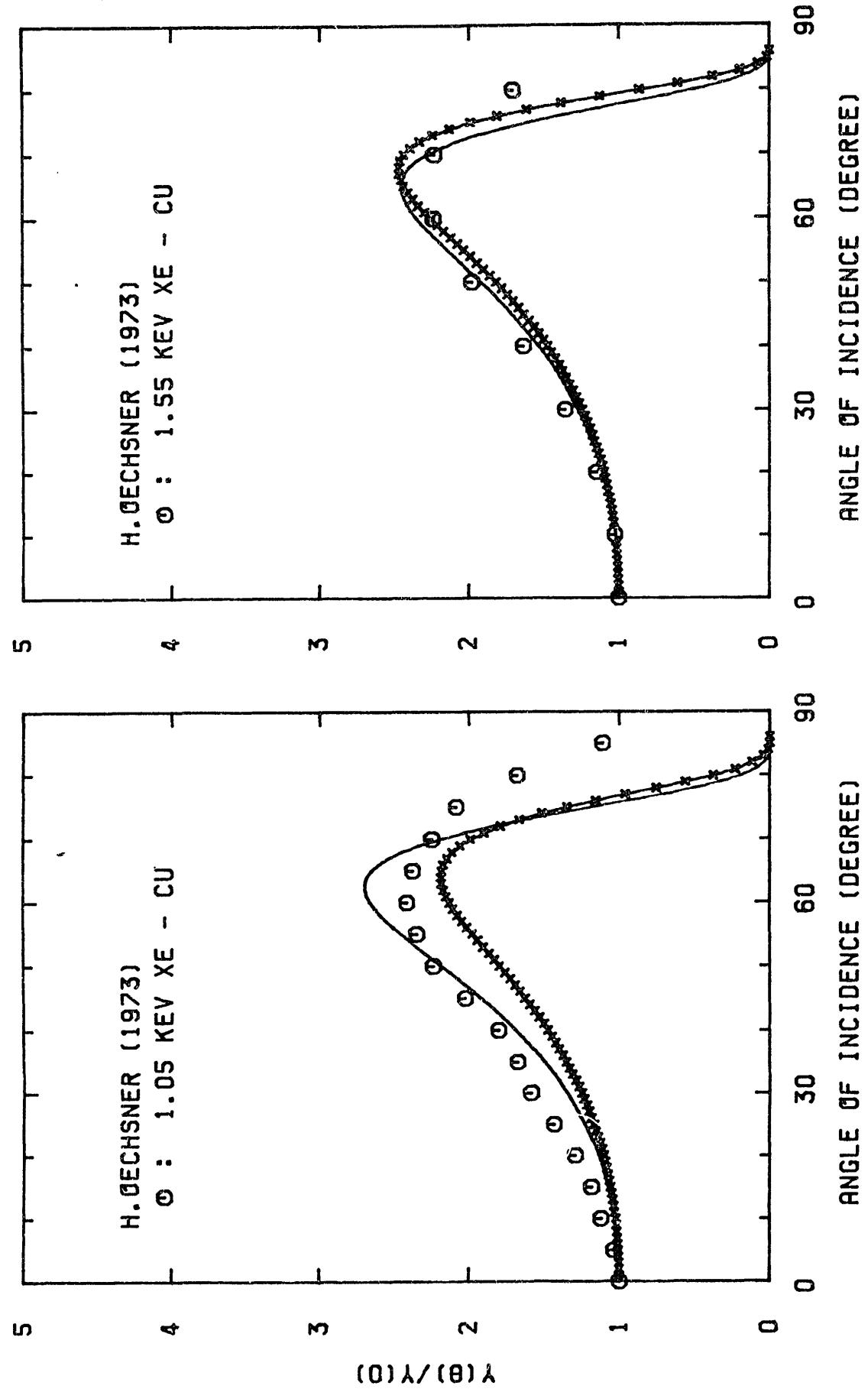


Fig. 35

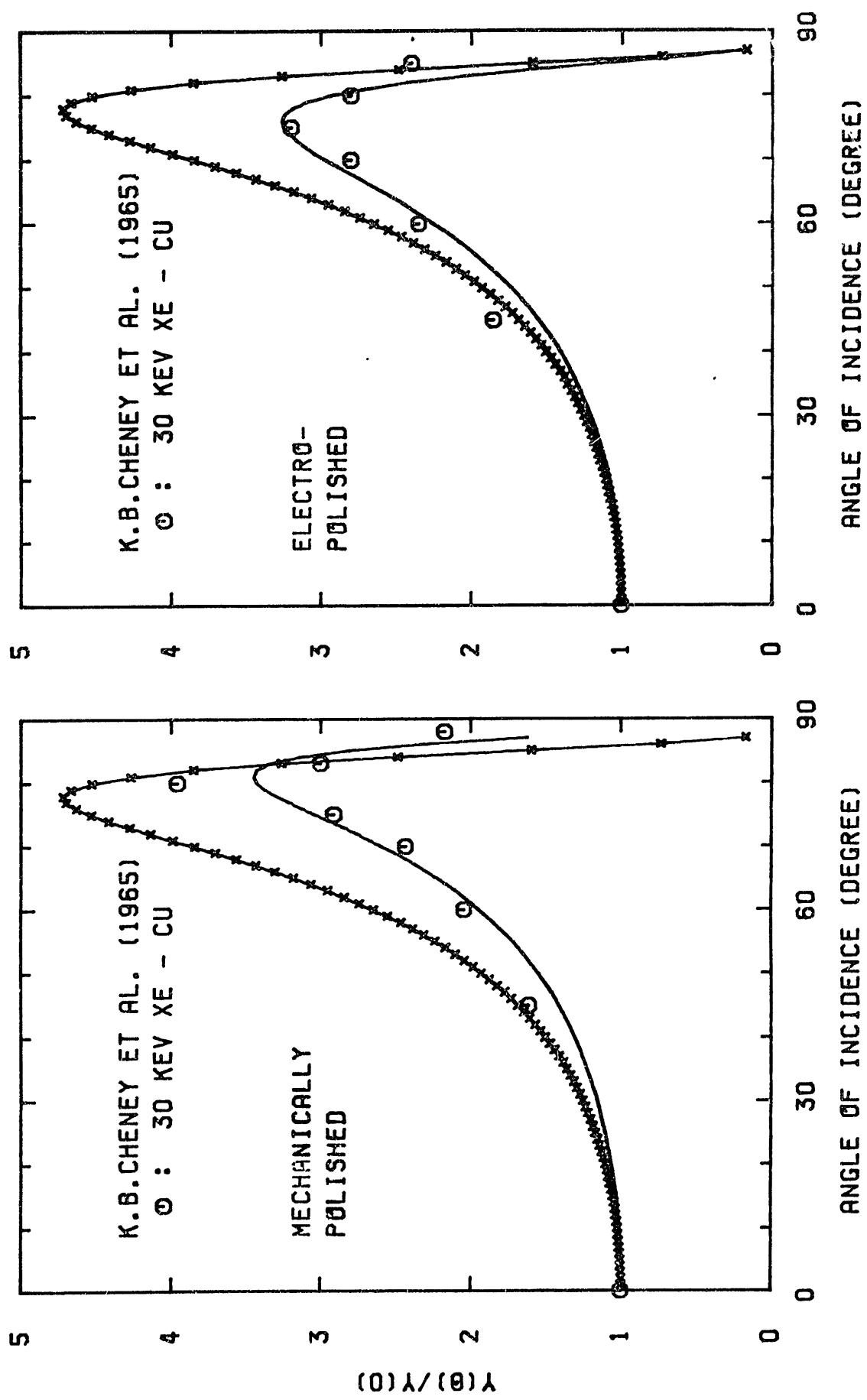


Fig. 36

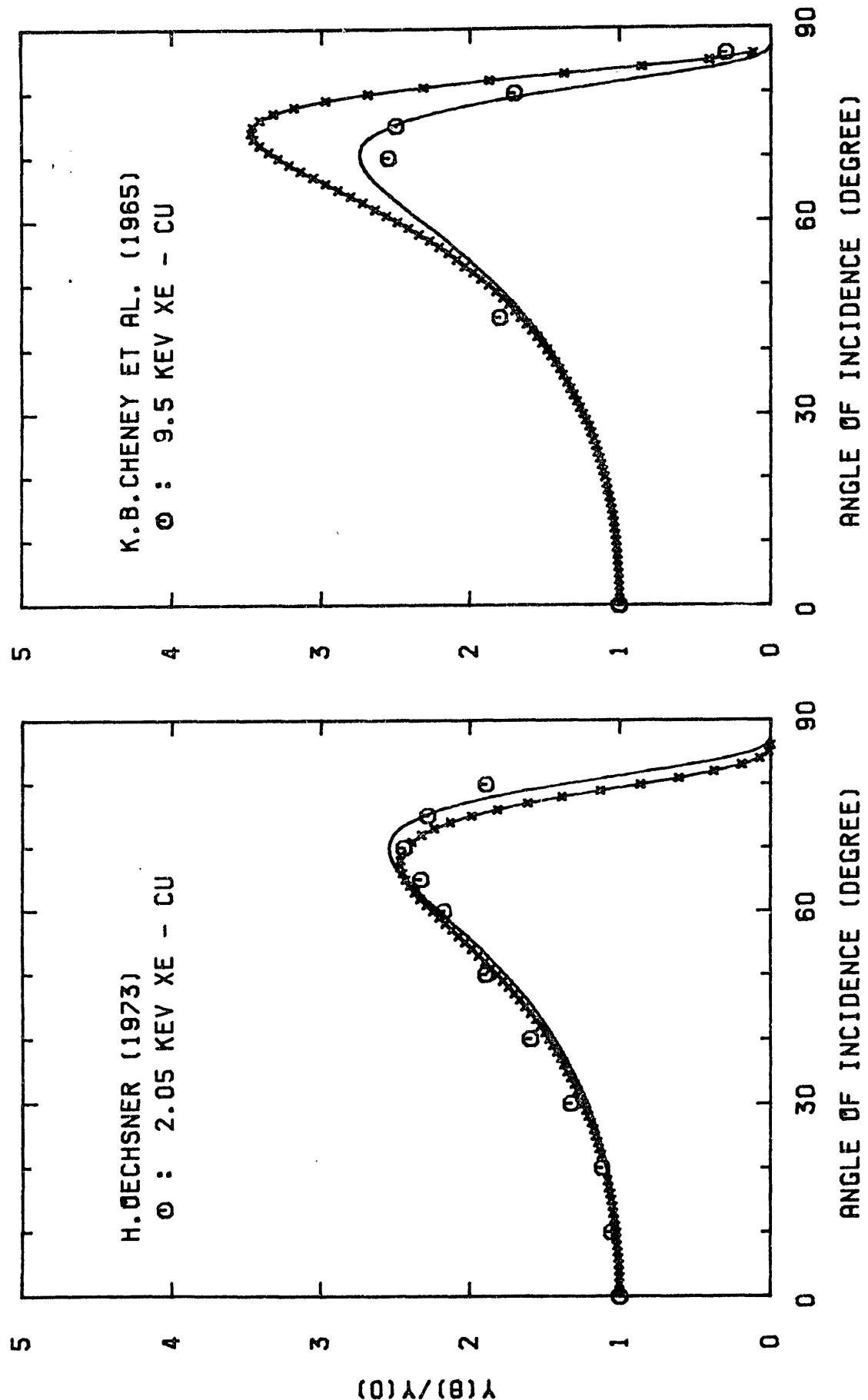


Fig. 37

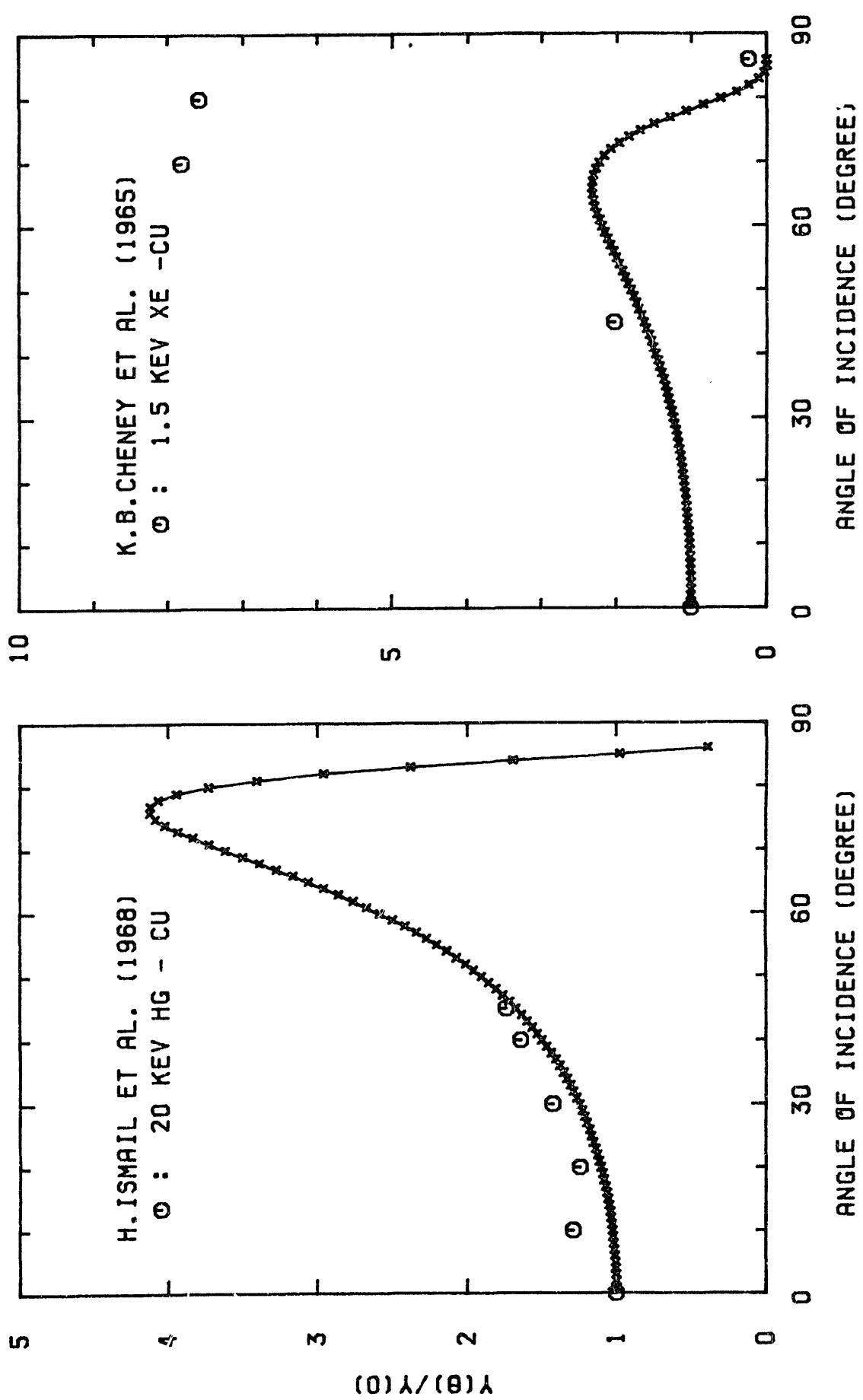


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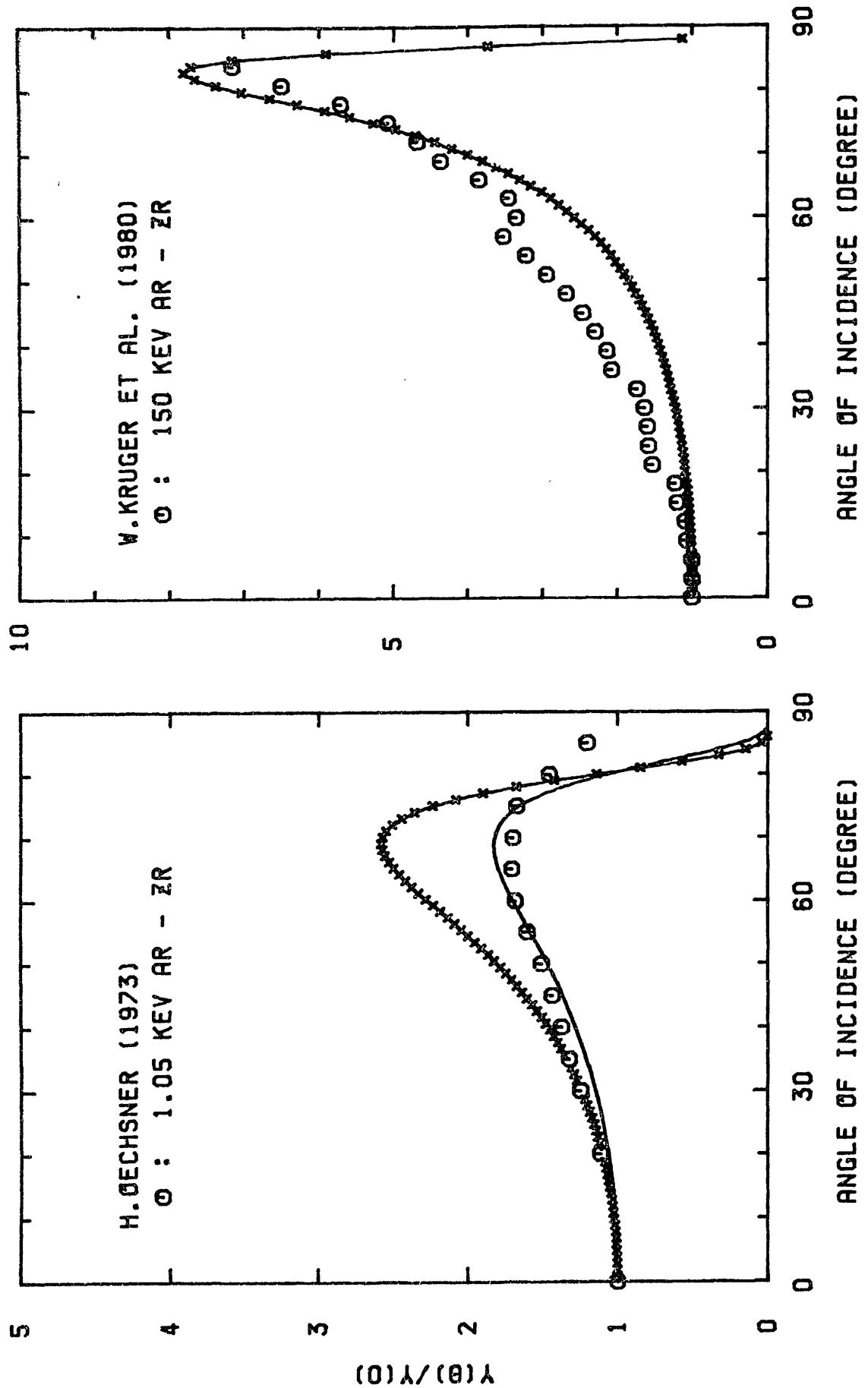


Fig. 39

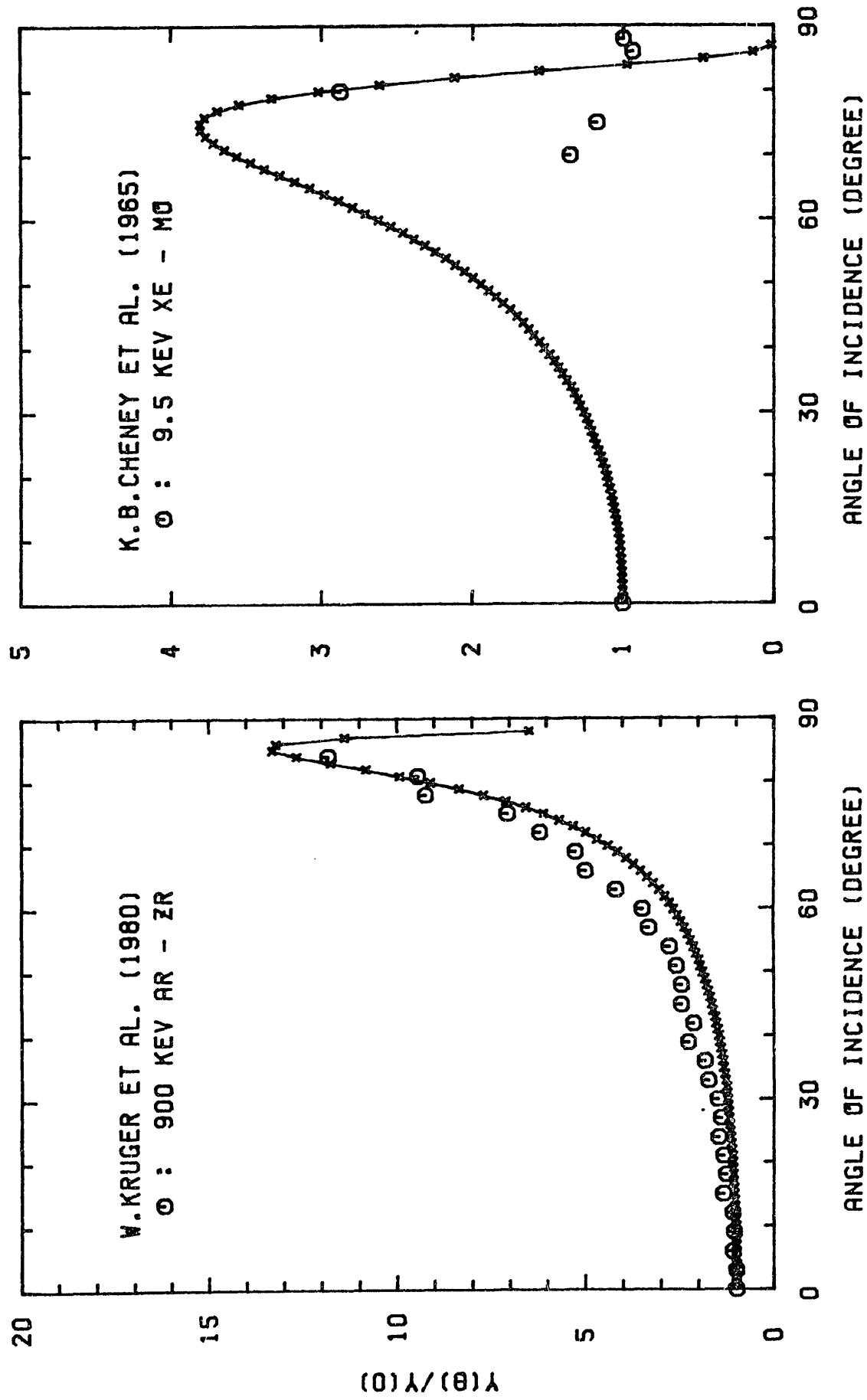


Fig. 40

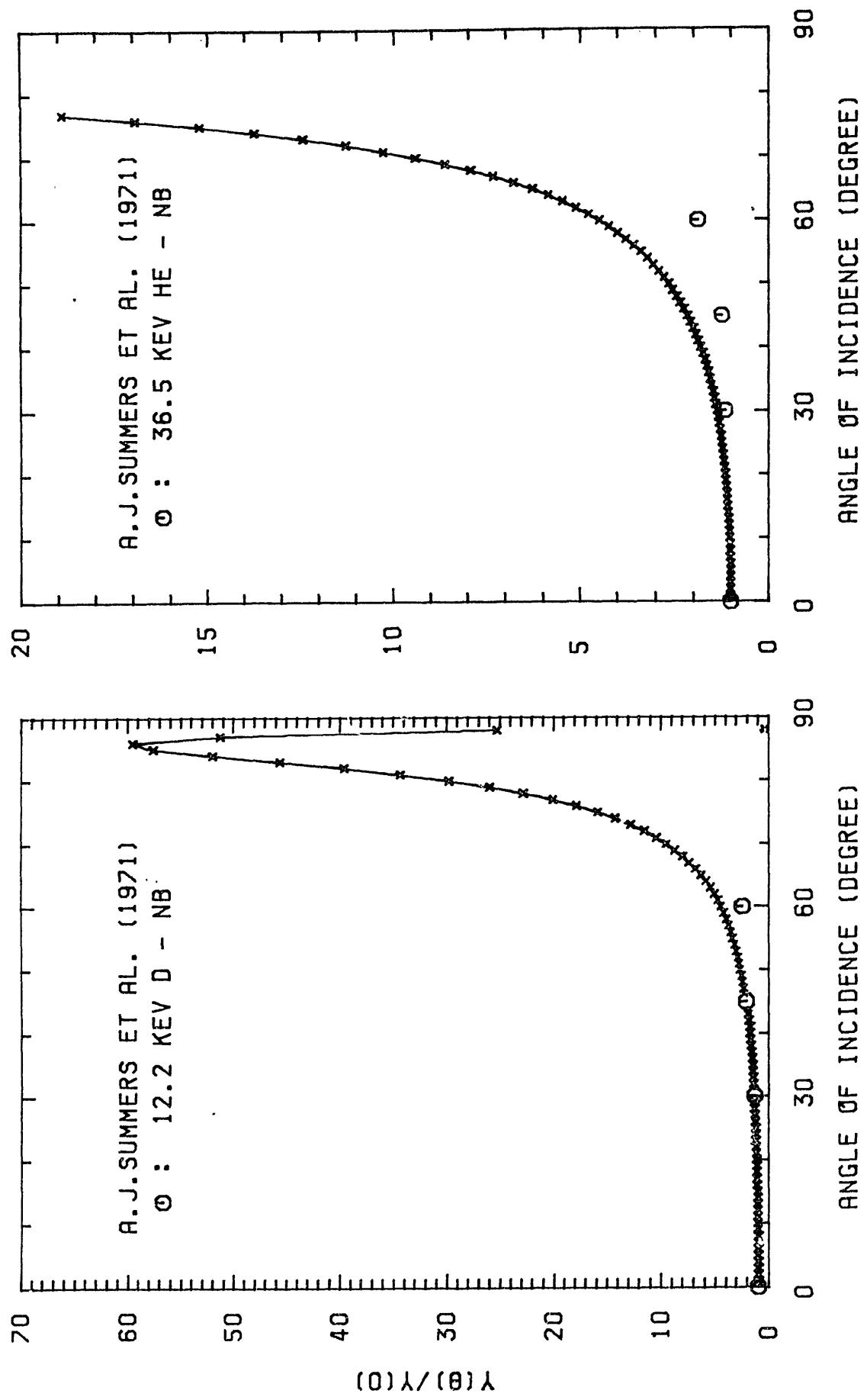


Fig. 41

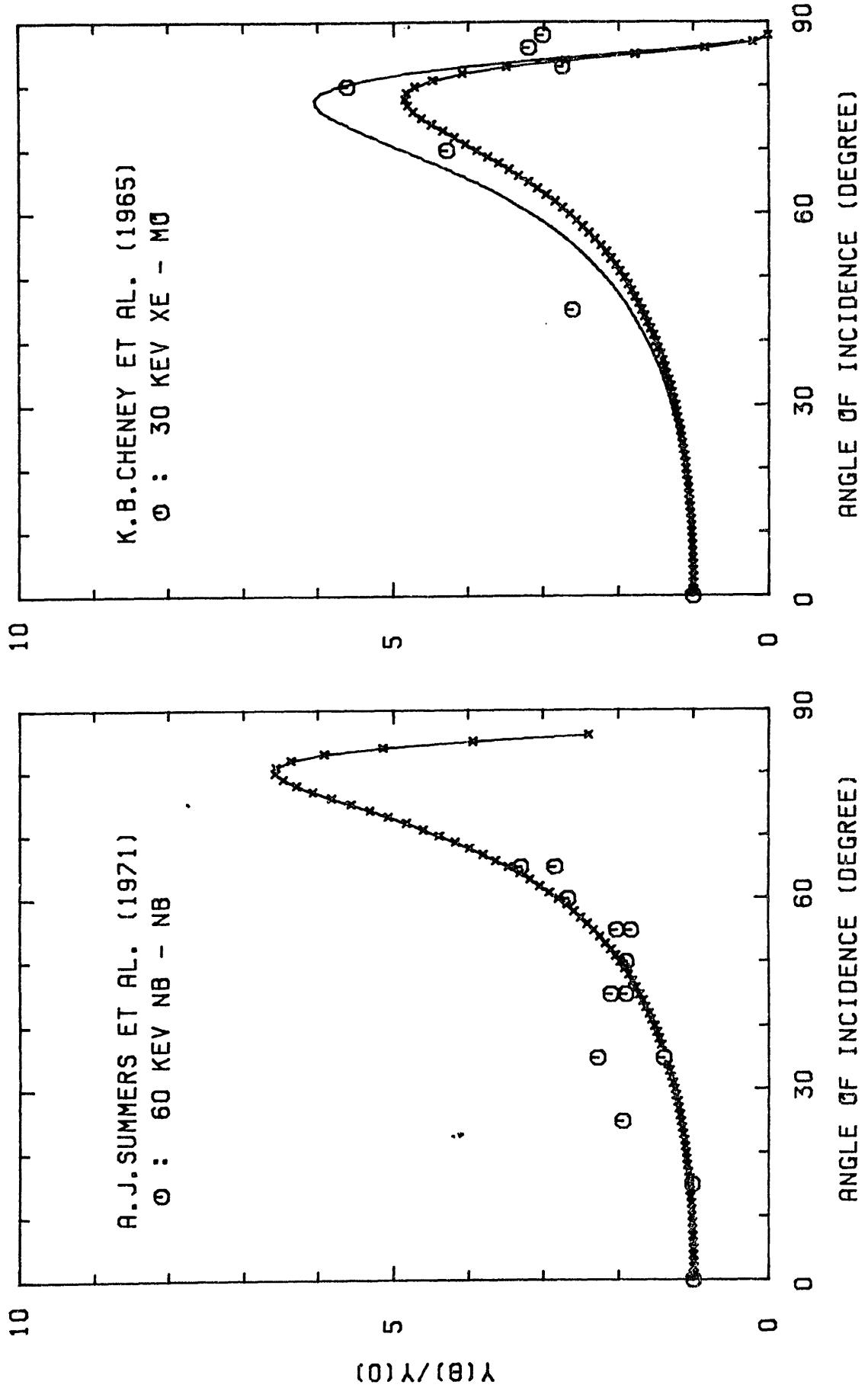


Fig. 42

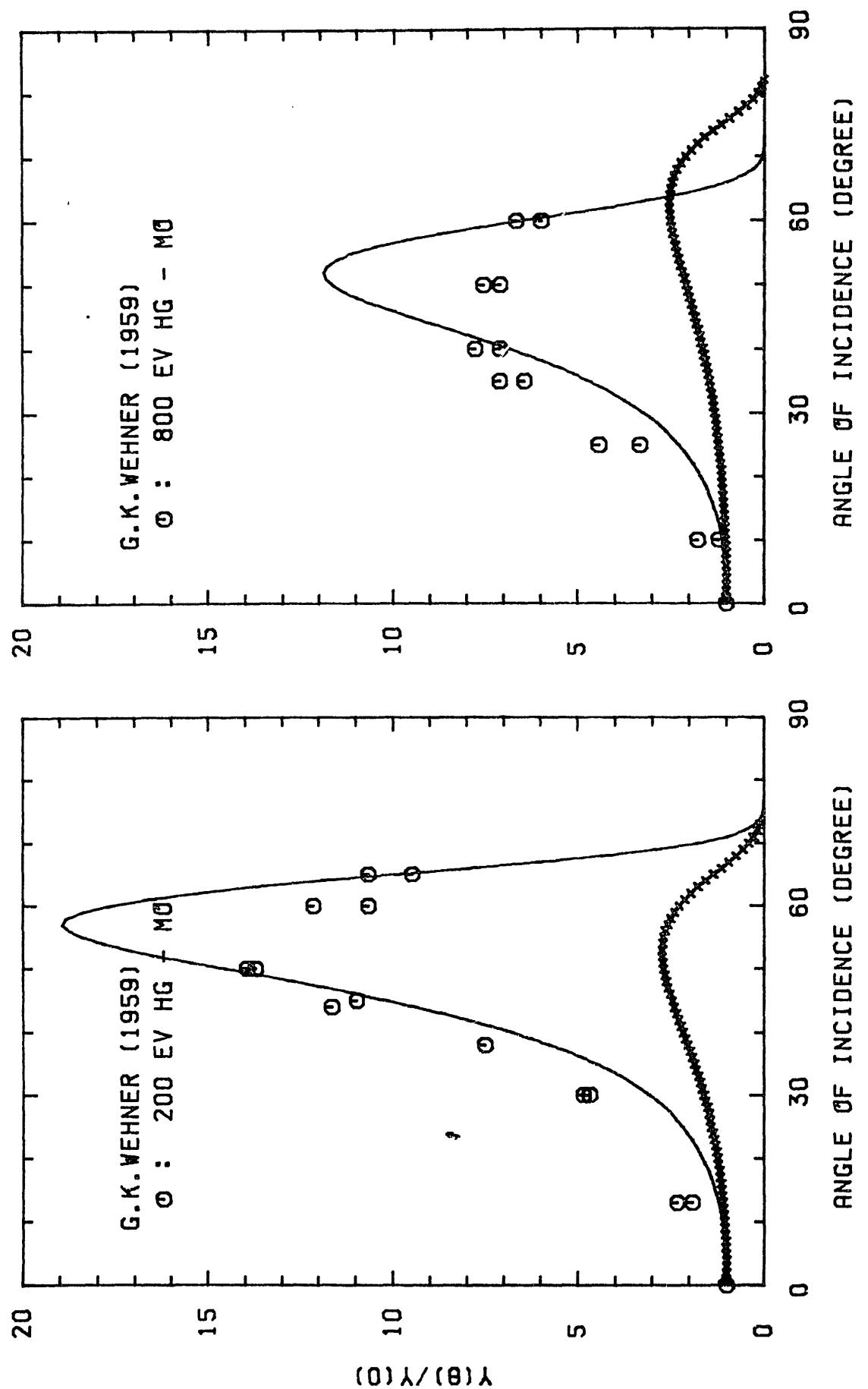


Fig. 43

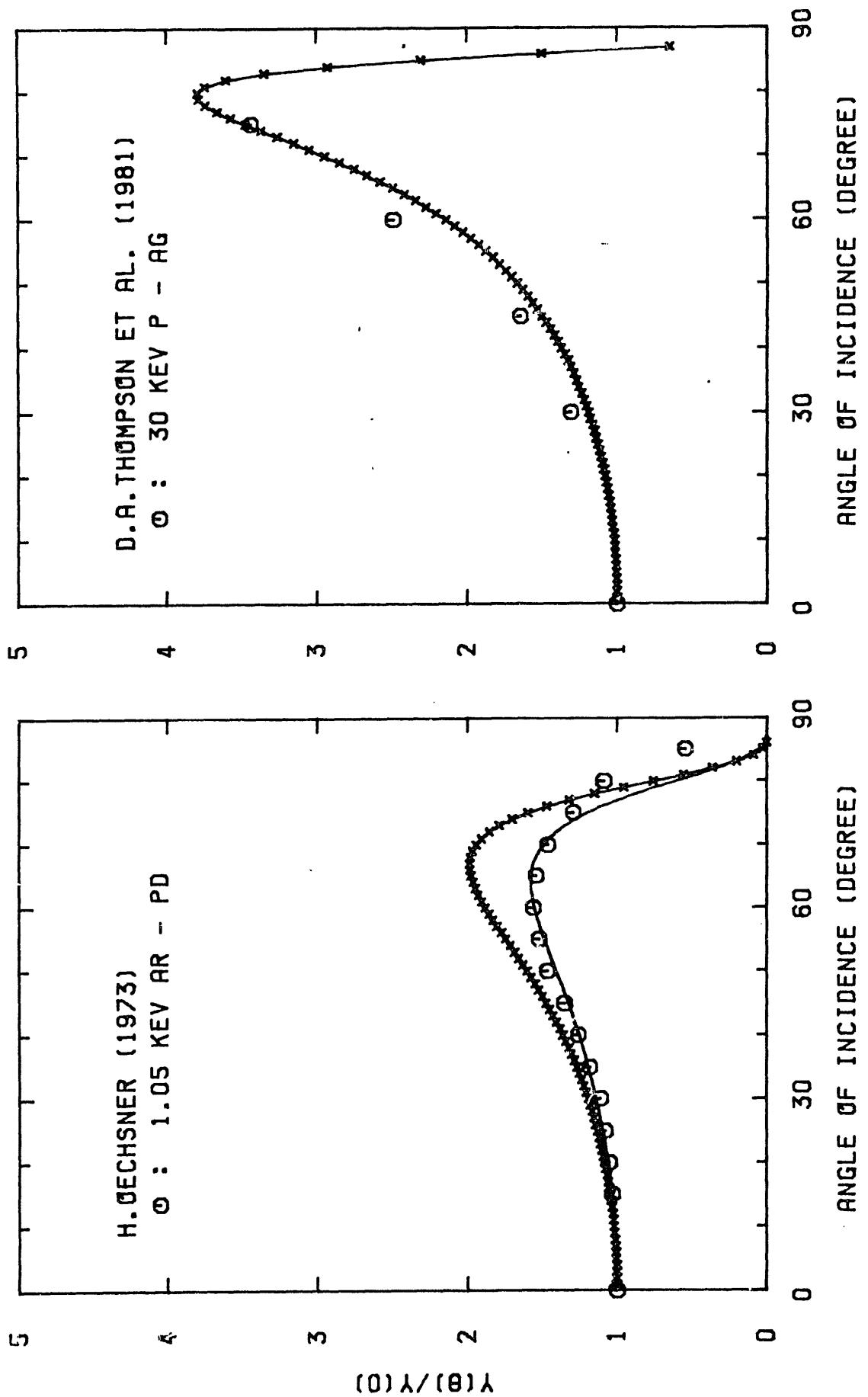


Fig. 44

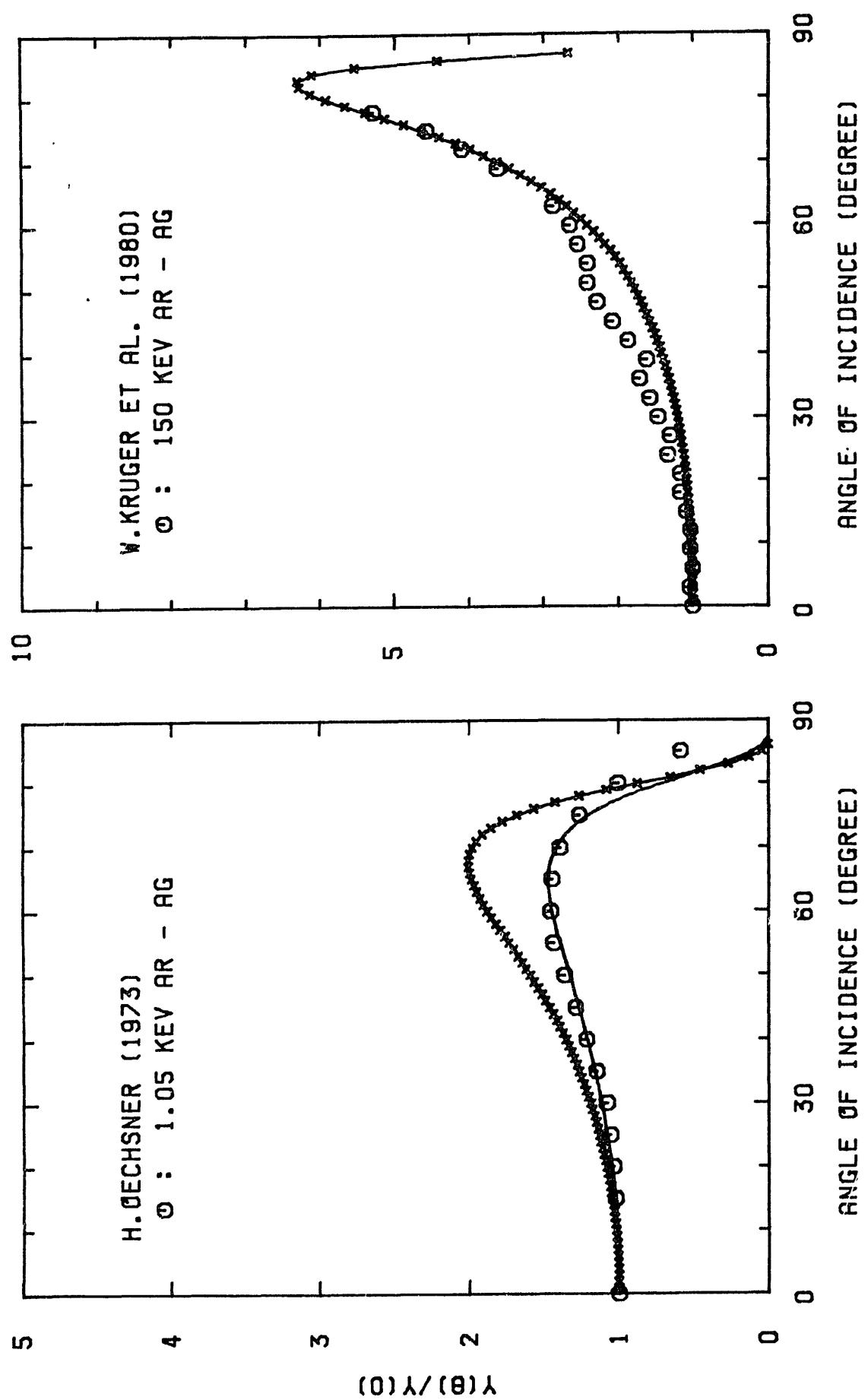


Fig. 45

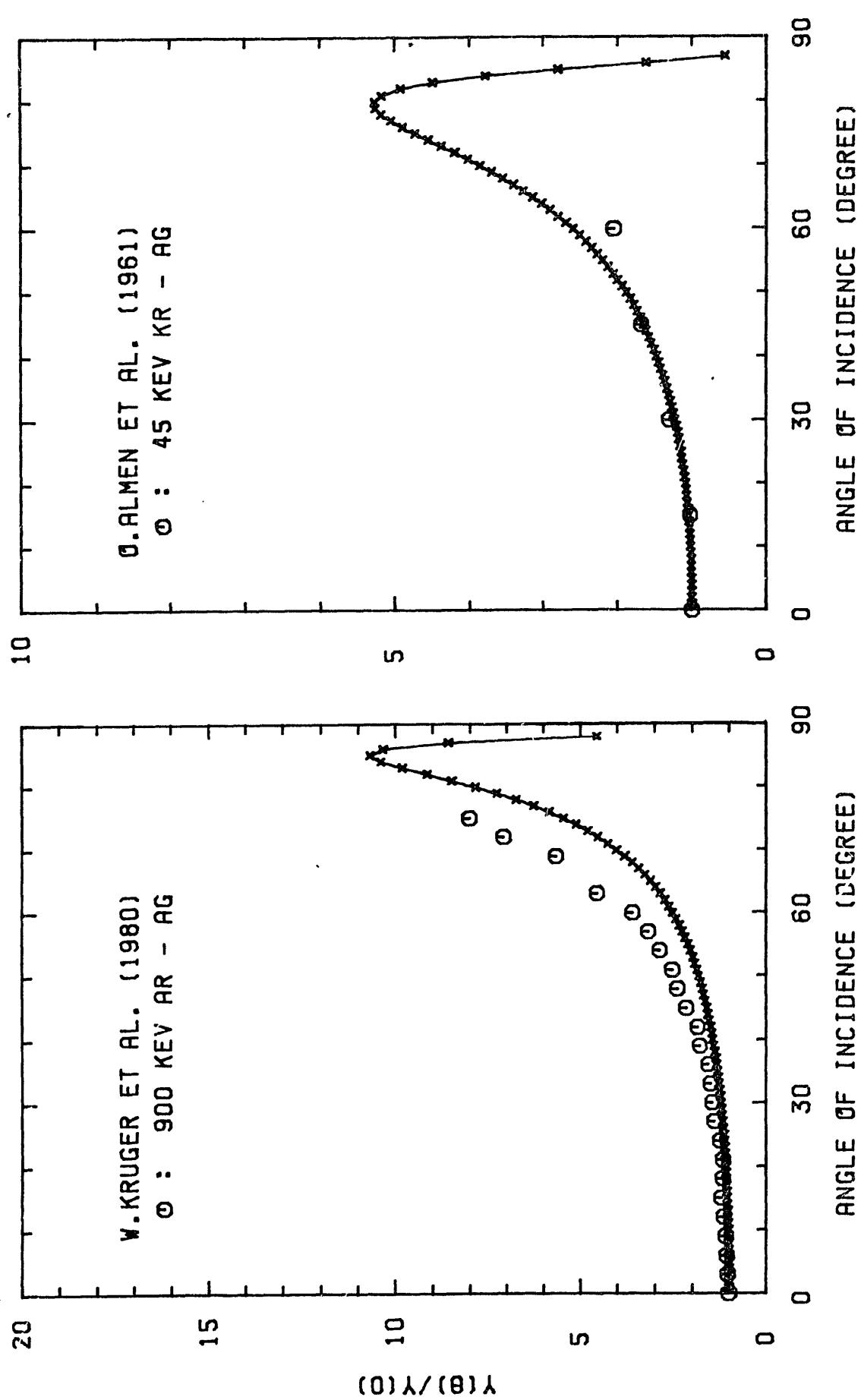


Fig. 46

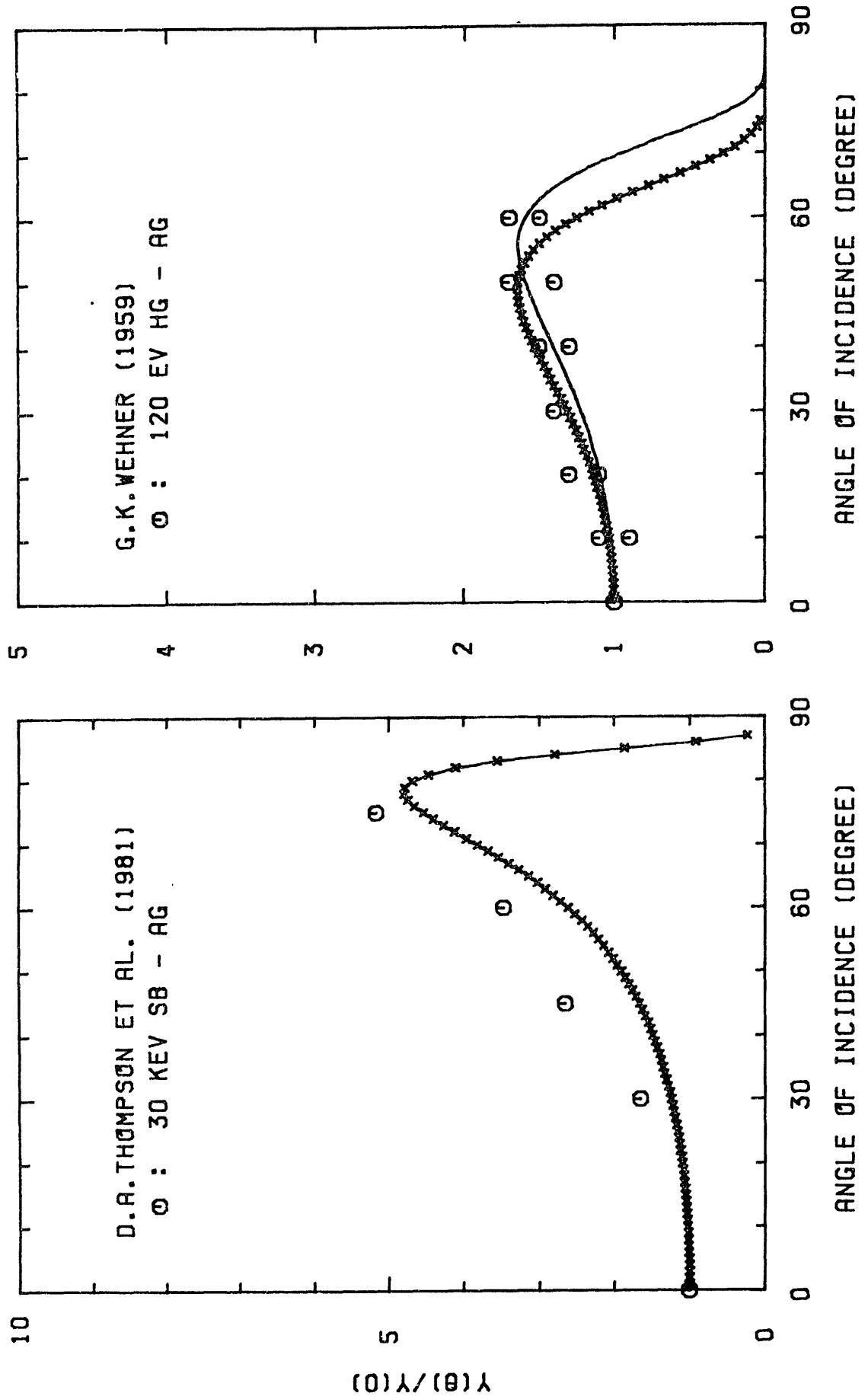


Fig. 47

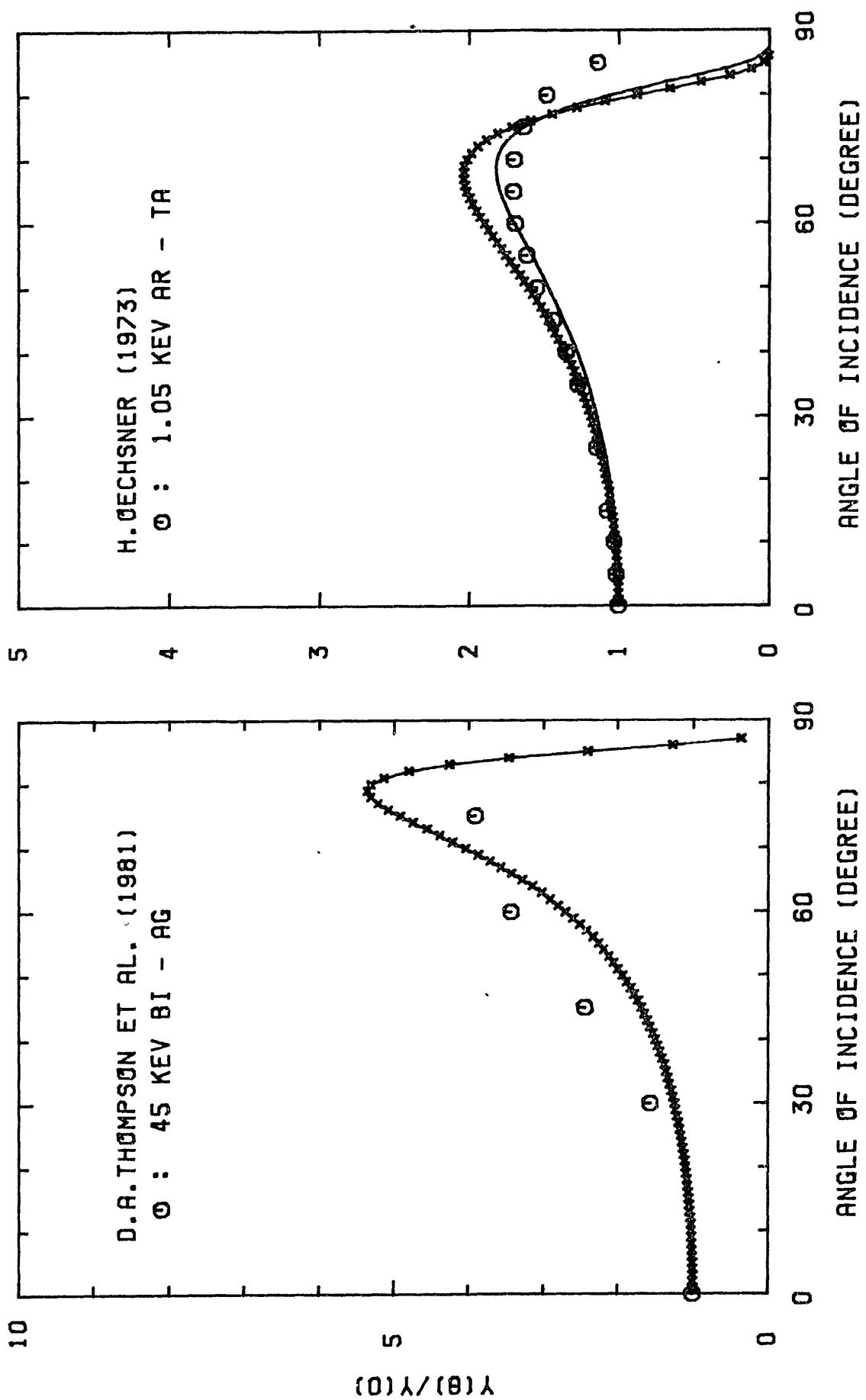


Fig. 48

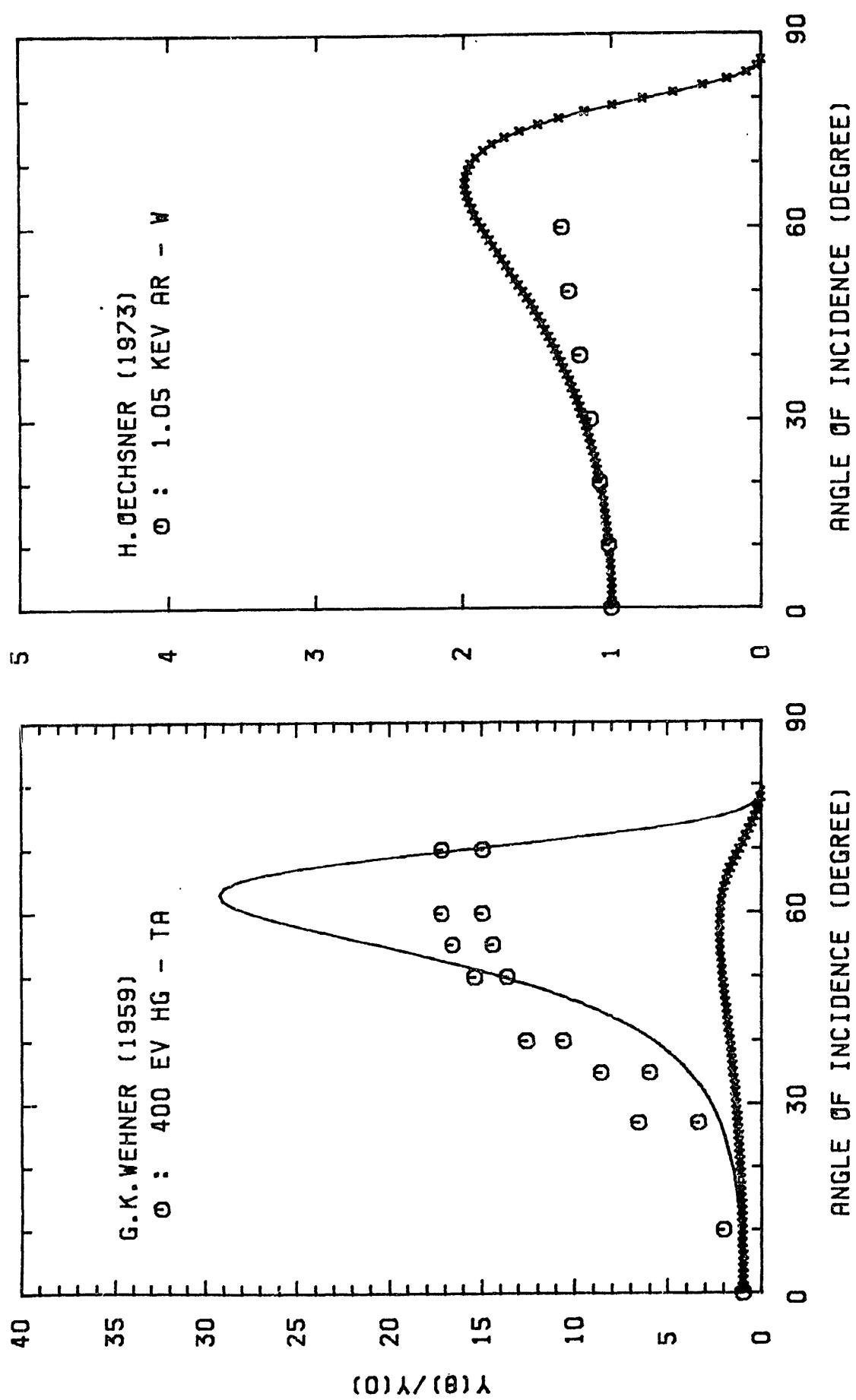


Fig. 49

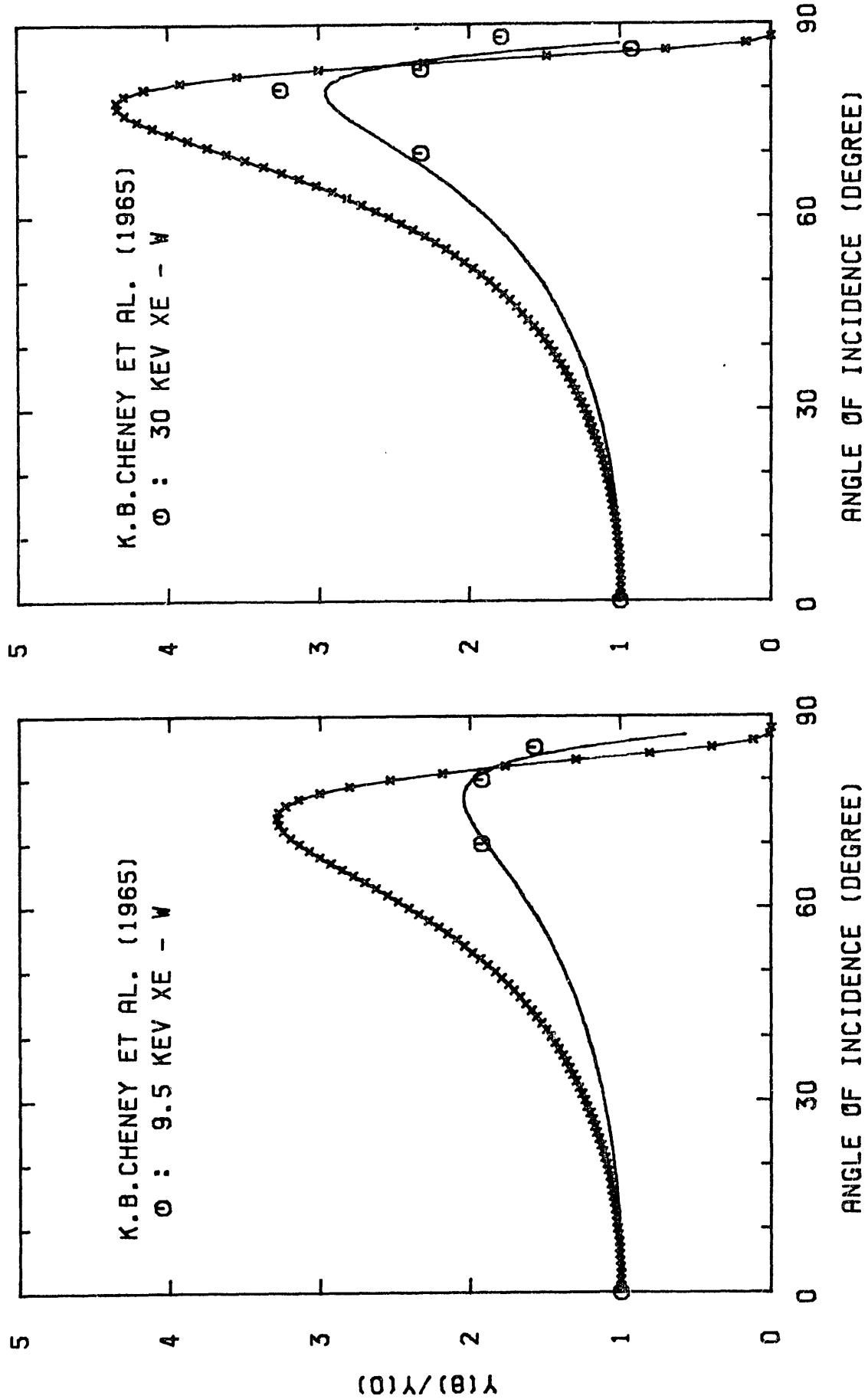


Fig. 50

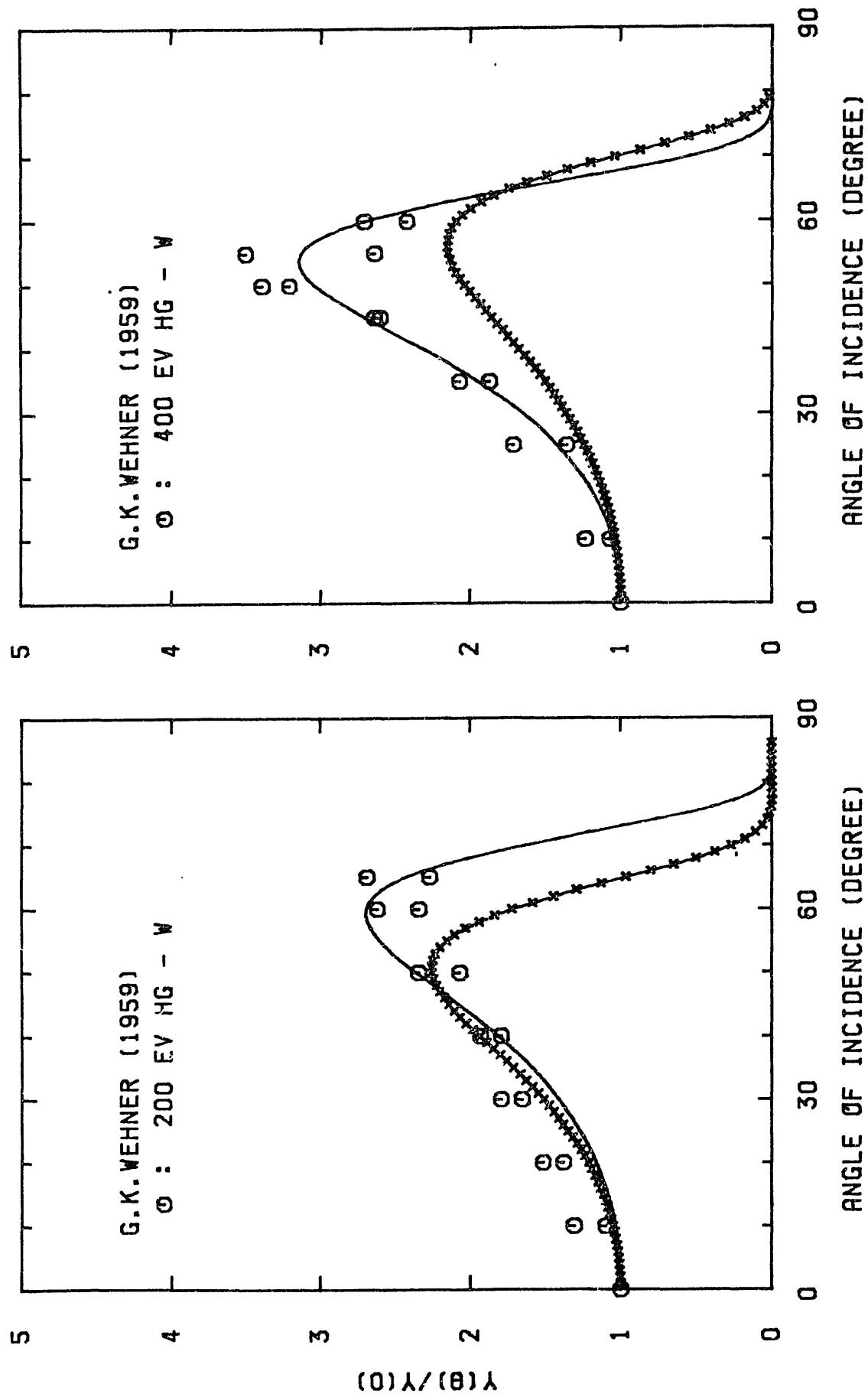


Fig. 51

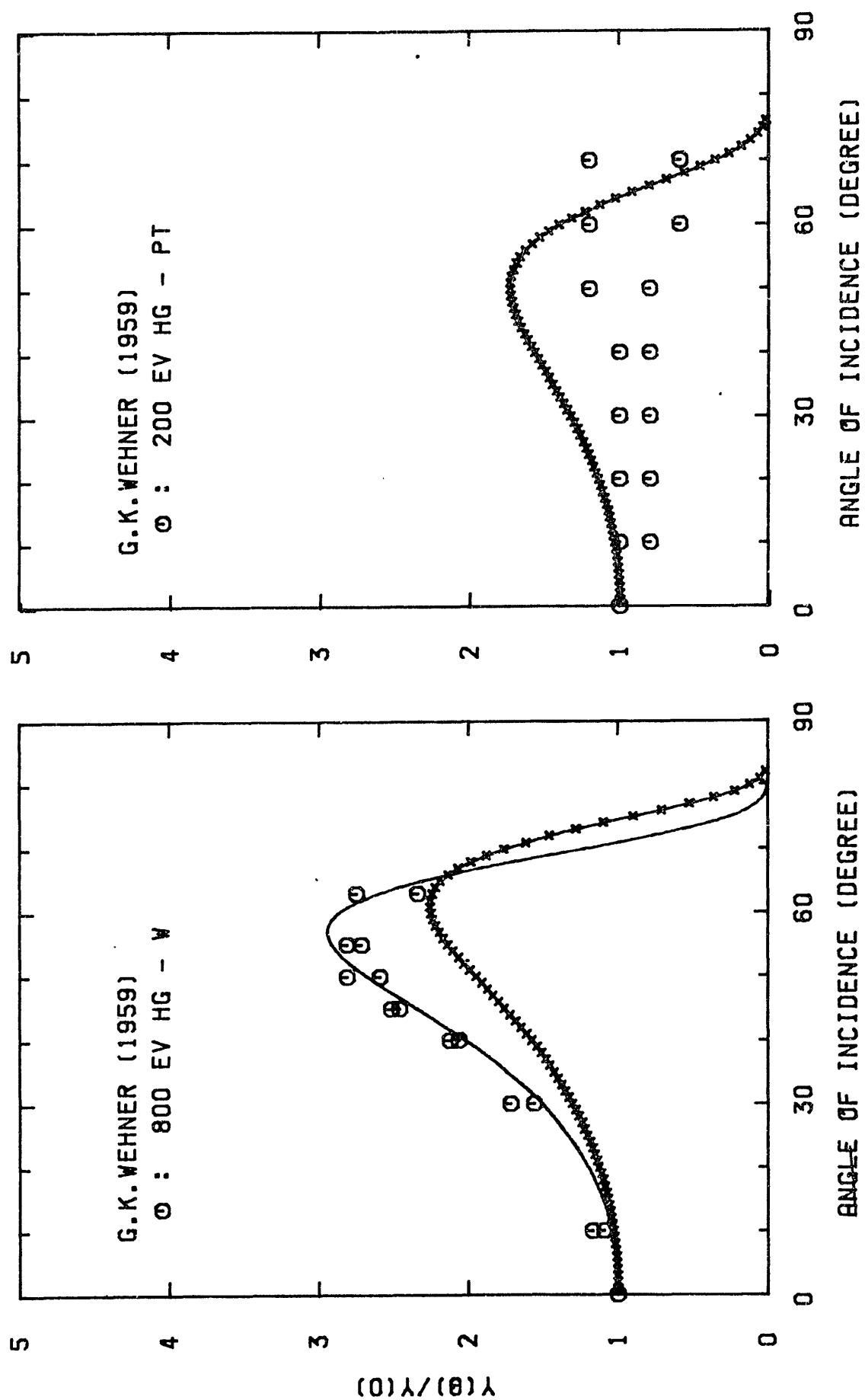


Fig. 52

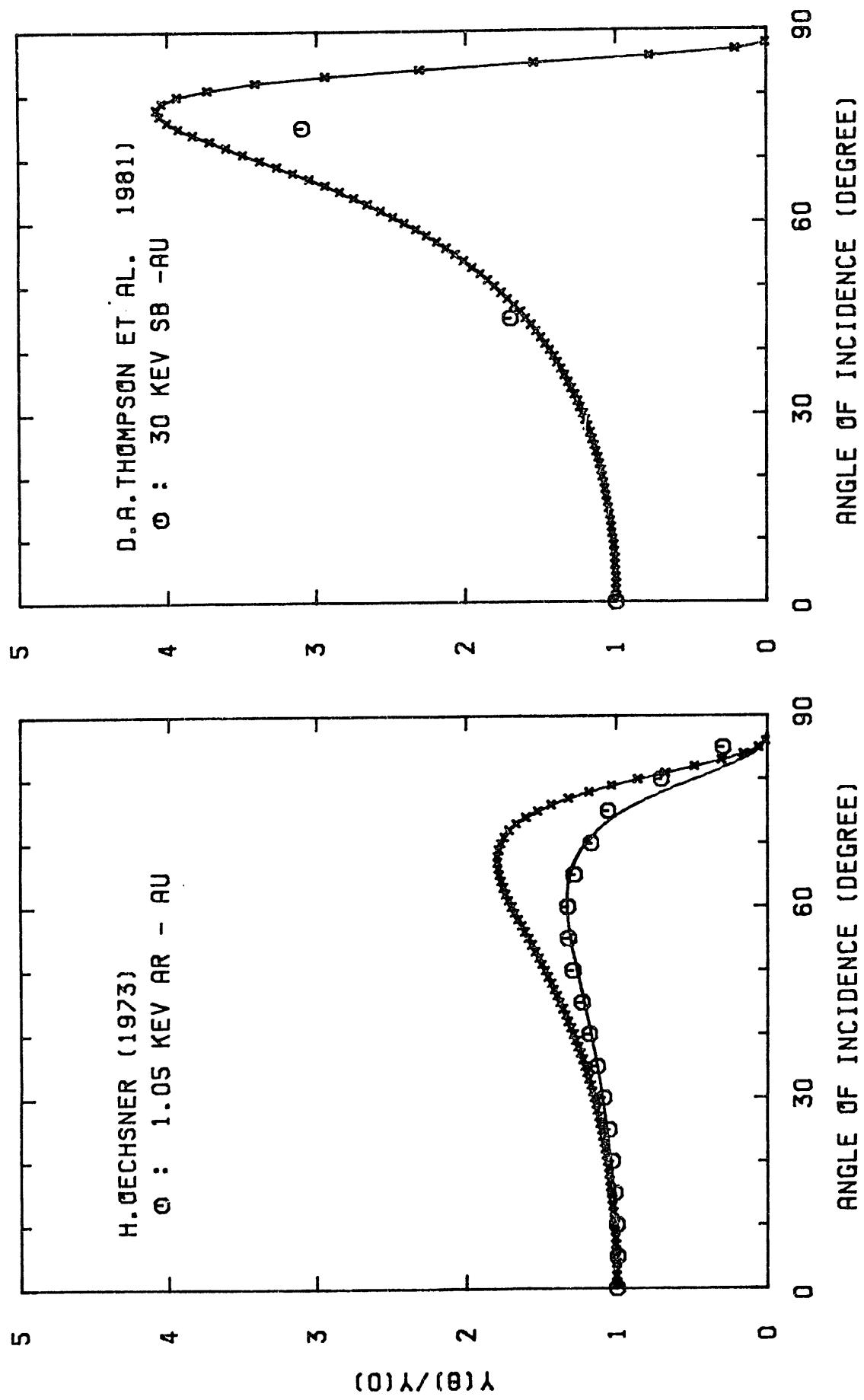


Fig. 53

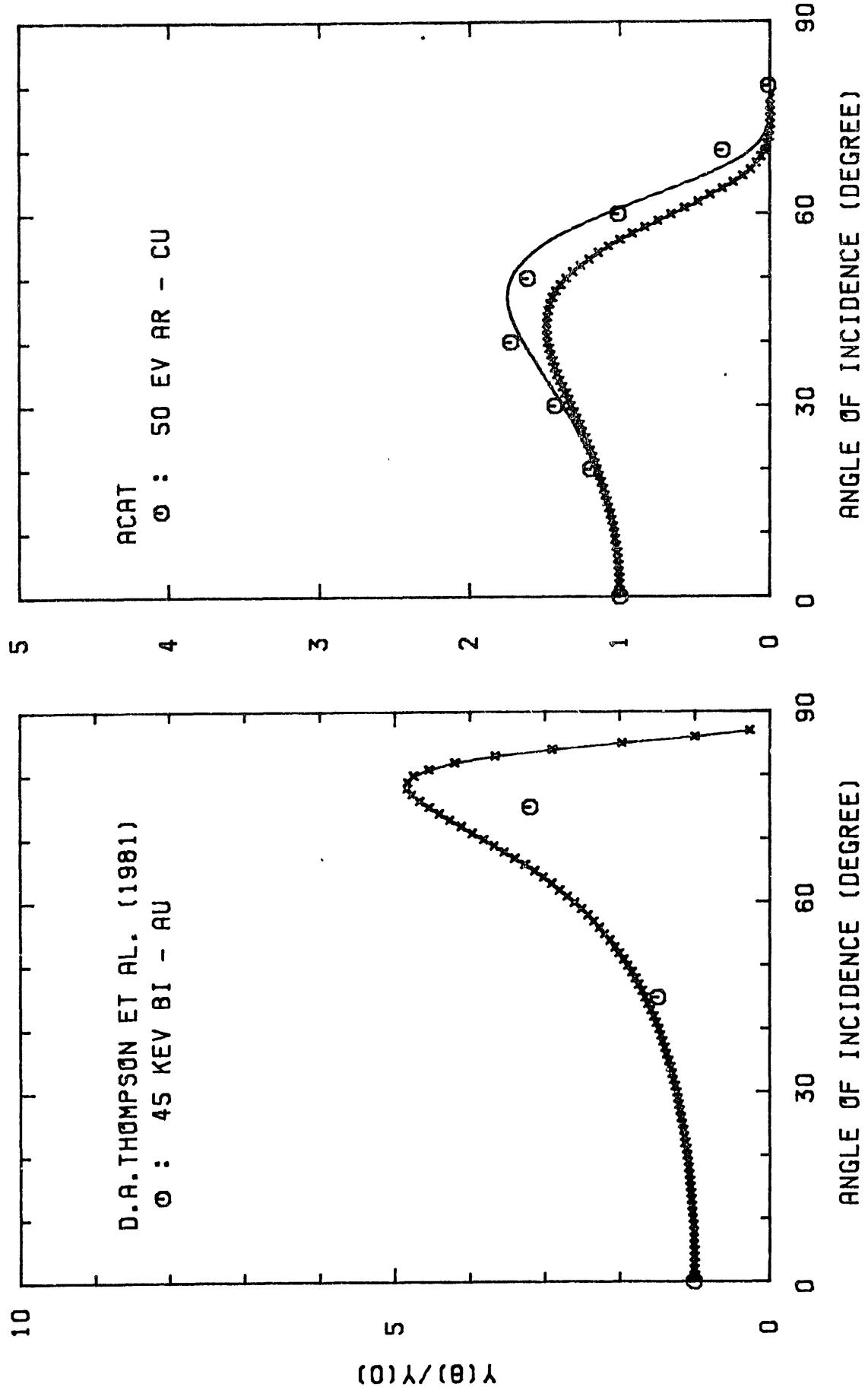


Fig. 54

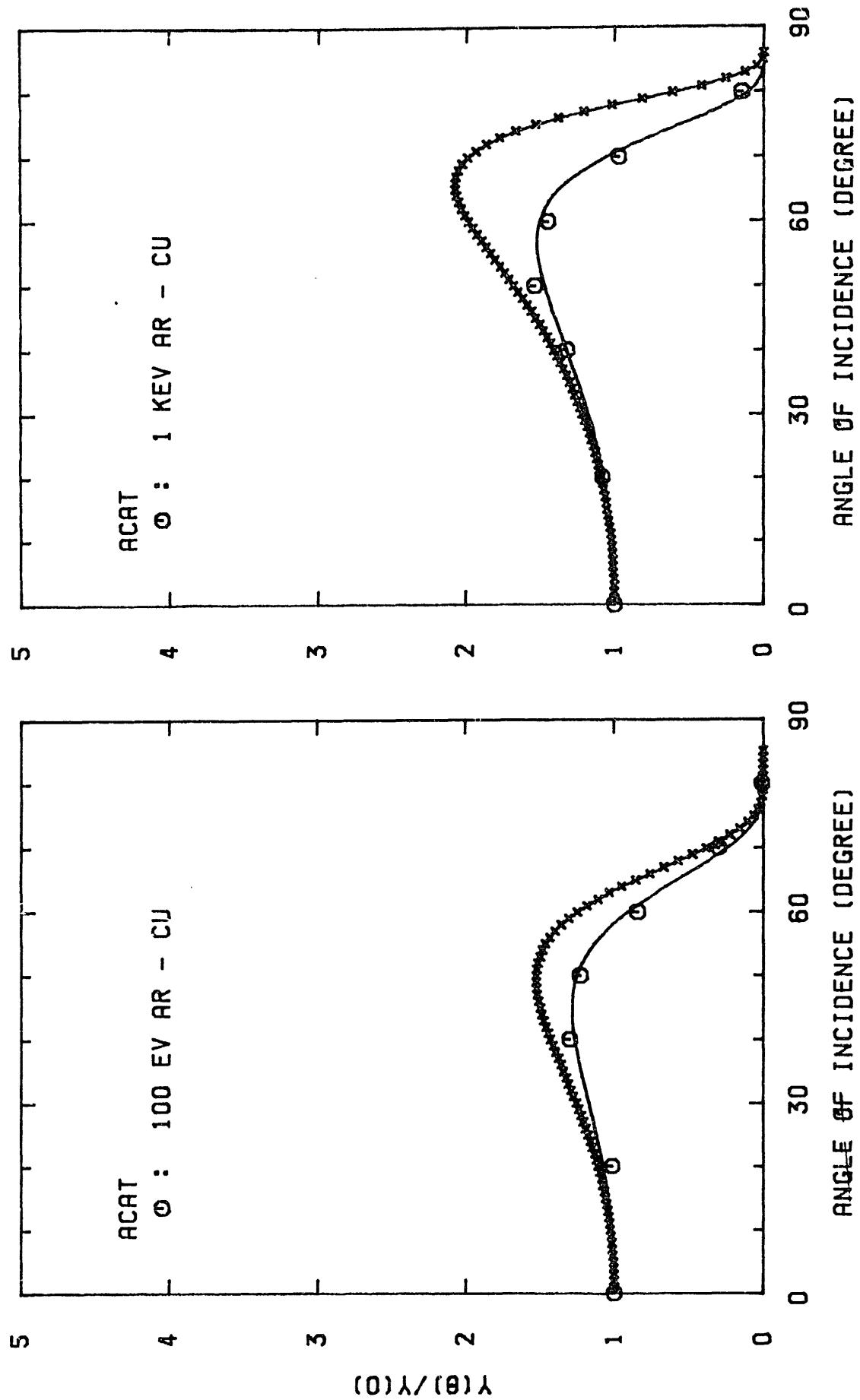


Fig. 55

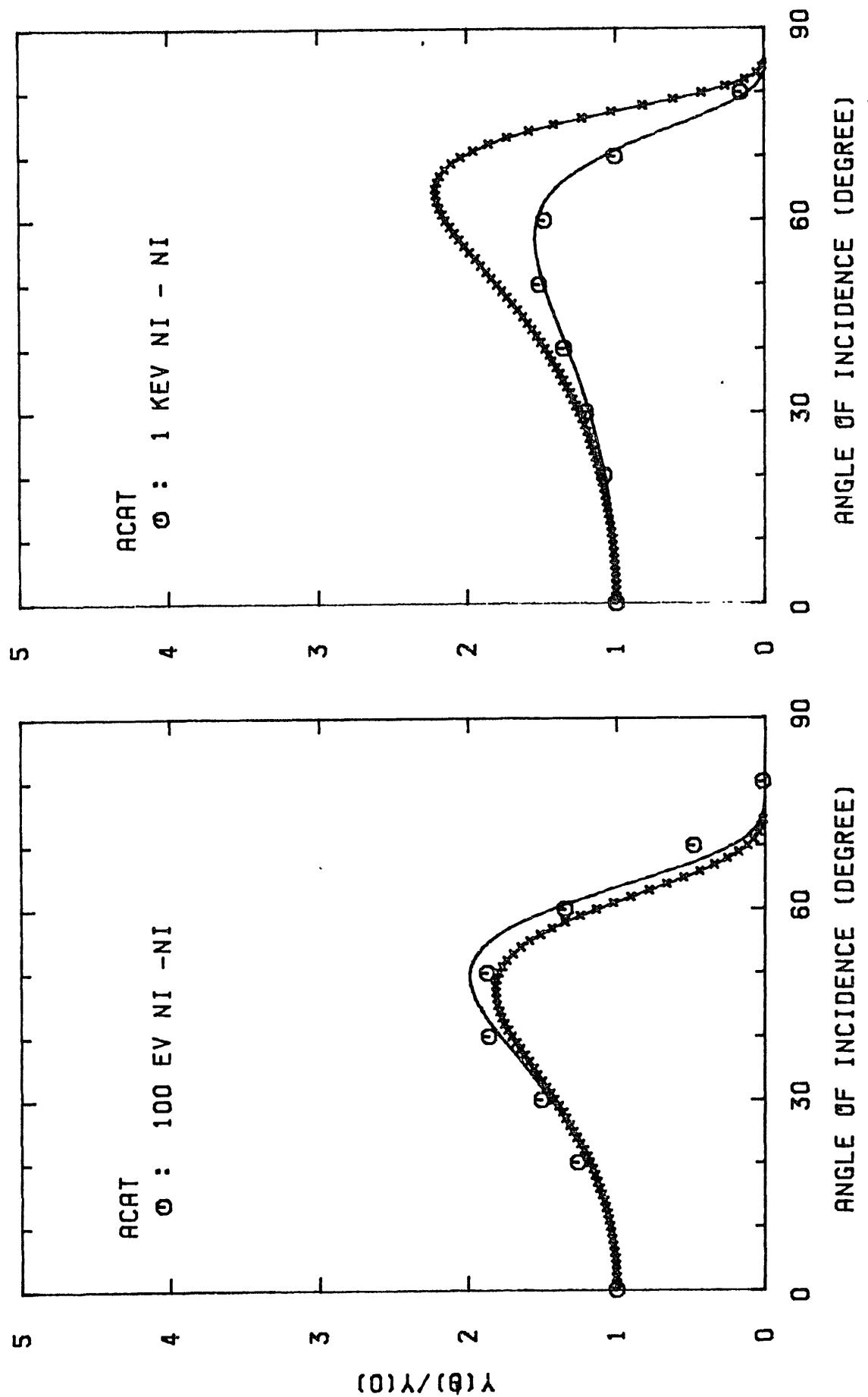


Fig. 56

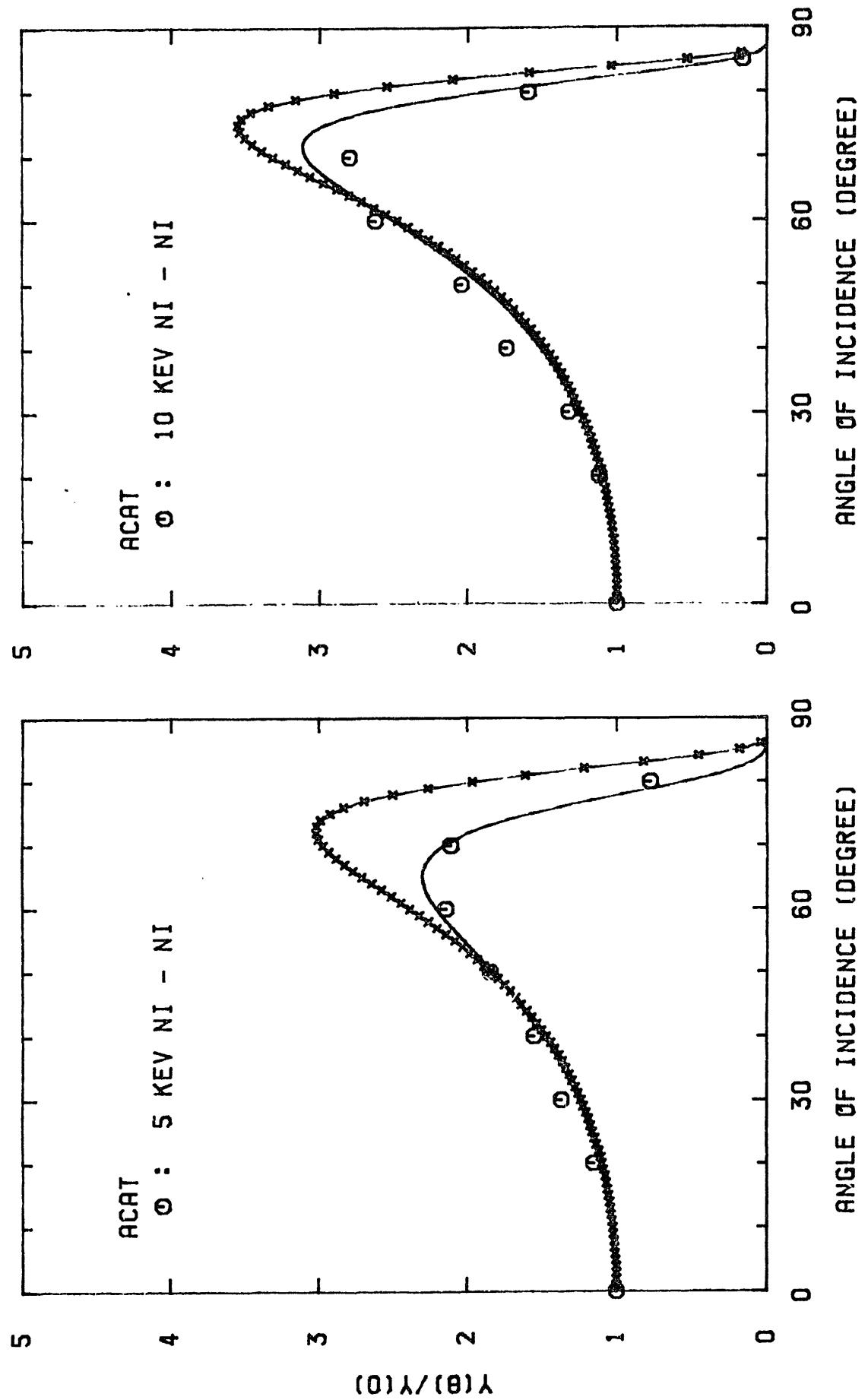


Fig. 57

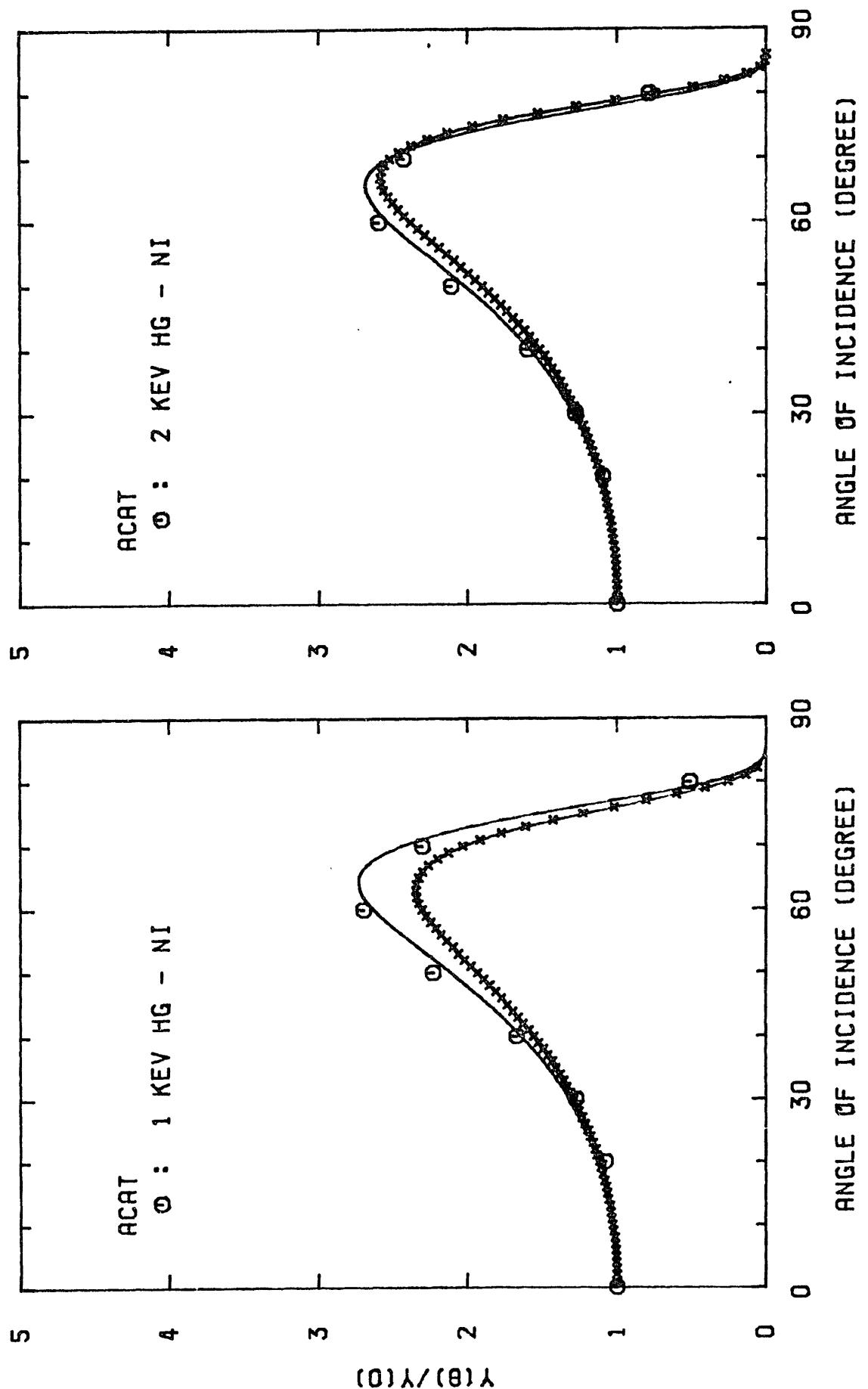


Fig. 58

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Y. Yamamura, Y. Itikawa and N. Itoh (1983)

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Available upon request to Research Information Center, Institute of Plasma Physics, Nagoya University, Nagoya 464, Japan, except for the reports noted with\*.