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Abstract

The angular dependence of sputtering yields of light-ion sputtering and heavy-ion sputtering has been investigated in detail , and the following empirical formula is proposed:

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$$\frac{Y(\theta)}{Y(0)} = t^{f} \exp \left[-\Sigma \left(t-1\right)\right]$$

where θ is the angle of incidence measured from the surface normal, and t = $1/\cos \theta$. The parameters f and Σ are adjustable parameters which are determined by the least-square method so as to fit the present empirical formula to available experimental data.

The best-fit parameters and their average values are listed in tables, where the value of θ_{opt} is listed in place of Σ . Here, θ_{opt} is the angle of incidence at the maximum yield and the relation between θ_{opt} and Σ is simple, i.e.,

 $\Sigma = f \cos \theta_{opt}$.

The present empirical formula has been compared with available experimental data of various ion-target combinations, and it is found that the agreement is satisfactory in a wide range of the angle of incidence.

1. Introduction

Current needs for sputtering yield at normal incidence and at oblique incidence have accelerated the experimental measurements of sputtering yields, particularly by light ions. The extensive uses of sputtering data for the design of the fusion reactors required the comparison of experimental data with empirical formula and the reliable empirical formulae at normal and oblique incidences.

The empirical formulae for the sputtering yields at normal incidence have been proposed by Bohdansky et al.¹, Matsunami et al.², and Yamamura et al.³ The compilations of the experimental data for available combinations of ions and target atoms have been published^{4,5}.

The angular dependence of sputtering yields has been investigated by many authors⁶⁻²⁵ and it was found that its dependence on the angle of incidence was roughly given by $\cos^{-1}\theta$ for not-too-oblique incidence,⁸ where θ is measured from the surface normal. On the other hand, the theoretical investigation on the angular dependence of sputtering yields was done by Sigmund²⁶, who showed that the normalized yield $Y(\theta)/Y(0)$ had the $\cos^{-f}\theta$ -dependence at not-too-oblique incidence, where 1 < f < 2.

At energies around 1 keV, the angular dependence of sputtering yields has been investigated systematically by Oechsner¹⁹. For not-too-large angles of incidence, he found that the normalized yield obeyed a simple relation $\Delta Y(\theta) / \Delta Y(\theta_{opt}) = 1.2 \hat{\theta}^2$, where $\hat{\theta} = \theta / \theta_{opt}$, $\Delta Y(\theta) = Y(\theta) - Y(0)$, and θ_{opt} is the angle of incidence at the maximum yield.

The rapid variation of sputtering yields with the angle of incidence has been reported by Bay et al.²⁰ for light-ion sputtering in low keV region. They found that the lighter the projectile, the maximum of the normalized yield was higher and also it increased with increasing

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the energy and increasing the surface binding energy. For the grazing angle of incidence, the surface channeling plays an important role and makes the drop-off of the sputtering yield at the glancing angles.

It is desired to have some analytical formula describing the angular dependence of the sputtering yields in a wide range of the angle of incidence. In this paper, a simple formula for the angular dependence of the normalized sputtering yield $Y(\theta)/Y(0)$ is proposed, taking into account the effect of the surface channeling at large angles, and the comparison of the present empirical formula with the existing experimental data will be made in detail.

2. An empirical formula for angular dependence of sputtering yields Light-ion sputtering is mainly due to collision cascades created by ions backscattered from the interior of the solid, while the heavy-ion sputtering is due to collision cascades generated by incoming ions directly²⁷. This difference is very important for low-energy sputtering, especially for the angular dependence of low-energy sputtering.

In the case of light-ion sputtering, the angular dependence of the threshold energy does not have a clear minimum. On the contrary, in the case of heavy-ion sputtering, the angular dependence of the threshold energy has a minimum near 60°. The threshold energy of heavy-ion sputtering is a decreasing function of the angle of incidence because of the anisotropic velocity distribution of recoil atoms near the surface, and for grazing angles of incidence it increases rapidly with increasing angle of incidence because of surface channeling. (see APPENDIX A). In other words, even if the ion energy is less than the threshold energy at normal incidence, the finite number of target atoms will be sputtered in oblique incidence in the case of heavy-ion sputtering. It must be noted that the normalized sputtering yield $Y(\theta)/Y(\vartheta)$ can not be well defined in such a low energy region.

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2.1 Angular dependence of light-ion sputtering

Light-ion sputtering is directly connected with the particle reflection coefficient because it is due to collision cascades generated by backscattered ions. Recently, Yamamura et al. have derived the following formula²⁸

$$Y(E) = 0.042 \frac{F_D(E^*)R_N(E)}{U_s} [1 - (\frac{E_{th}}{E})^{\frac{1}{2}}]^{2.8}$$
(1)

for light-ion sputtering at normal incidence, where $F_D(E^*)$ is the deposited energy near the solid surface by a backscattered ion, E^* is the average energy of the reflected ion, and $R_N(E)$ is the particle reflection coefficient of the ion with the incident energy E. The surface binding energy U_s is taken to be equal to the sublimation energy. E_{th} is the threshold energy of the sputtering at normal incidence.

For not-too-oblique incidence, the normalized yield is given by

$$\frac{Y(\theta)}{Y(0)} = \frac{F_{D}(E^{*}(\theta))}{F_{D}(E^{*})} \frac{R_{N}(E,\theta)}{R_{N}(E)}$$
(2)

where the threshold effect of the light ion sputtering is neglected because of its weak angular dependence and Y(0) is the sputtering yield at normal incidence which is described by Y(E) in eq.(1). Similarly $R_N(E)$ means $R_N(E, \theta=0)$.

The angular dependence of the reflection coefficient is roughly estimated in terms of the range distribution. For very small angles of incidence, the ratio $R_N(E,\theta)/R_N(E)$ is given by

$$\frac{R_{N}(E,\theta)}{R_{N}(E)} = \frac{\int_{\infty}^{\theta} dx \ F(E,\theta,x)}{\int_{\infty}^{\theta} dx \ F(E,0,x)} = (\cos\theta)^{-f}R, \qquad (3)$$

where

$$f_{R} = 1 + \frac{\langle Y^{2} \rangle_{R}}{\langle \Delta X^{2} \rangle_{R}}$$
, (4)

and $F(E,\theta,x)$ is the range distribution and the subscript R of the moments means those of the range distribution. The exponent f_R is nearly equal to 2 for large mass ratio²⁹.

Since $E^*(\theta)$ does not depend so largely on the angle of incidence,

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the angular dependence of $Y(\theta)/Y(0)$ is mainly determined by those of the particle reflection coefficient, and we can write

$$\frac{Y(\theta)}{Y(0)} = (\cos \theta)^{-f_{R}} .$$
 (5)

As the angle of incidence increases, the effect of surface channeling becomes important. In order to sputter target atoms at the outermost layer, the projectile must penetrate the first layer of the solid surface, and this penetration probability is roughly estimated by

$$exp(- N\sigma R_0 / \cos \theta)$$
,

where σ is the hard-sphere collision cross section between a projectile and a target atom, $R_0 = N^{-\frac{1}{3}}$ is the average lattice constant of the random target, and N is the number density of the target atom.

From above discussions we know that the angular dependence of the normalized yield will have the form

$$\frac{Y(\theta)}{Y(0)} = t^{f} \exp[-\Sigma(t-1)], \qquad (6)$$

where $t = 1/\cos \theta$ and the parameters f and Σ are adjustable parameters. The angle of incidence at the maximum yield is simply given by

$$\theta_{\text{opt}} = \cos^{-1}\left(\frac{\Sigma}{f}\right) . \tag{7}$$

Using the least-square method, the best-fit parameters to the present empirical formula are obtained from experimental data^{19,20,21,24} and computer results (ACAT)³⁰. The best-fit values of f and θ_{opt} are listed in Table 2. It is very interesting that the best fit f's are nearly equal to 2 which is a theoretical value of Eq. (4).

The best-fit values of f depend slightly on the sublimation energy and so the ratio of the best-fit f to $\sqrt{U_s}$ is plotted as a function of mass ratio M_2/M_1 in Fig. 1, where M_1 and M_2 are the atomic masses of a projectile and a target atom, respectively. The solid line in Fig. 1 corresponds to the average value of f which satisfies the following relation:

$$\frac{f}{\sqrt{U_s}} = 0.94 - 1.33 \times 10^{-3} (M_2/M_1) .$$
 (8)

In Fig. 2 the best-fit values of θ_{opt} are plotted as a function of

$$\eta = \frac{a}{R_0} \left(\frac{1}{2 \epsilon q} \right)^{\frac{1}{2}} , \qquad (9)$$

where $q = (U_s / \gamma E)^{\frac{1}{2}}$ corresponds to the cosine of the scattering angle of a recoil atom which gains the energy U_s in a single collision. The LSS reduced energy ε is defined by $\varepsilon = E/E_{L}$, where

$$E_{L} = \frac{M_{1} + M_{2}}{M_{2}} \frac{Z_{1}Z_{2}e^{2}}{a} , \qquad (10)$$

a = 0.4685
$$\left(\frac{1}{Z_{1}^{2/3} + Z_{2}^{2/3}}\right)^{\frac{1}{2}}$$
 (11)

 Z_1 and Z_2 are the atomic numbers of a projectile and a target atom, respectively and $\gamma = 4M_1M_2/(M_1 + M_2)^2$, M_1 and M_2 being their masses. The solid line in Fig. 2 is a theoretical curve of θ_{opt}^{31}

$$\theta_{\rm opt} = 90^{\circ} - 57.3 \, \eta$$
 (12)

which is derived from the direct knock-out model. The Agreement between the best-fit values and the theoretical results is very good, and so we can calculate θ_{opt} from the theoretical formula.

2.2 Angular dependence of heavy-ion sputtering

In the case of heavy-ion sputtering, one cannot neglect the threshold effect which is a decreasing function of the angle of incidence for the not-too-oblique incidence. This means that the normalized yield has the following angular dependence:

$$\frac{Y(\theta)}{Y(0)} = (\cos \theta)^{-f_{s}} \left[\frac{1 - (E_{th}/E)^{\frac{1}{2}} \cos \theta}{1 - (E_{th}/E)^{\frac{1}{2}}} \right]$$
(13)

where the exponent f_s is given in the form by Sigmund²⁶ as follows:

$$f_{S} = 1 + \frac{\langle Y^{2} \rangle_{D}}{\langle \Delta X^{2} \rangle_{D}} \left[\frac{\langle X \rangle_{D}^{2}}{\langle \Delta X^{2} \rangle_{D}} - 1 \right]$$
(14)

for not-too-large angles of incidence, where the subscript D of the moment means those of the damage distribution.

The neccessary condition for the genuine collision cascade near the solid surface is that the projectile must penetrate a few layer of the surface. This means that an empirical formula for heavy-ion sputtering can be expressed by the product of the similar expression to that for light-ion sputtering and the threshold term of Eq. (13). At present, the threshold energy is not well established. For simplicity, let us employ an empirical formula with the same functional form as that of light-ion sputtering, eq.(6), i.e.,

$$\frac{Y(\theta)}{Y(0)} = t^{f} \exp[-\Sigma(t-1)], \qquad (15)$$

where the exponent f will include the threshold effect of Eq. (13), and so it will depend on the ion energy in the low-energy region. This tendency is much different from light-ion sputtering.

The best-fit parameters to the present formula, Eq. (15), are obtained for about 25 ion-target combinations (Table 1), using the least-square method and are listed in Table 3. In the energy region where the threshold effect can be neglected, the best-fit values of f are consistent with Sigmund f_S , as shown in Fig. 3.

In Fig. 4 the ratios of the best-fit f's to Sigmund f_S are plotted as a function of $\zeta = 1 - (E_{th}/E)^{\frac{1}{2}}$, where E_{th} is calculated from the following relation: ³

$$E_{th} = 1.5 \frac{0_s}{\gamma} [1 + 1.38 (M_1/M_2)^h]^2$$
(16)

with h = 0.834 for $M_2 > M_1$ and h = 0.18 for $M_2 < M_1$. This empirical relation for the threshold energy corresponds to the second Matsunami formula for sputtering yields at normal incidence³. The solid line in Fig. 4 is

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$$\frac{f}{f_{s}} = 1 + 2.5 \frac{1 - \zeta}{\zeta} .$$
 (17)

Equation (17) shows that f is infinite at $E = E_{th}$, which corresponds to the fact that the normalized sputtering yield Y(θ)/Y(0) is not well defined in the energy region of E < E_{th} .

In Fig.5 the best-fit values of 90° - θ_{opt} are plotted against

$$\psi = \left(\frac{a}{R_0}\right)^{3/2} \left| \frac{z_1 z_2}{\left(z_1^{2/3} + z_2^{2/3}\right)^{\frac{1}{2}}} \frac{1}{E} \right|^{\frac{1}{2}} .$$
 (18)

The parameter ψ is directly connected with the critical angle

$$\psi_{\rm C} = \left(U_{\rm R}(0) / E \right)^{\frac{1}{2}}$$
(19)

of surface channeling, where $U_R(0)$ is the average potential at the amorphous solid surface which is defined in APPENDIX A. The solid line in Fig. 5 means the average value of the best-fit θ_{opt} 's which has the form

$$\theta_{\text{opt}} = 90^\circ - 286.0 \ \psi^{0.45}$$
 (20)

3. Compilation of Experimental Data on Angular Dependence of Sputtering Yields

The angular dependence of sputtering yields of various combinations has been compiled and stored in a computer. The compiled data are summarized in Table 1. When determining the best-fit values of the adjustable parameters f and Σ , we excluded the experimental data which do not have explicit maximum values or which do not have the data at normal incidence.

Table 4 shows the physical constants necessary for calculating the angular dependece of the sputtering yield by means of the present empirical formula. For extensive use of the present empirical formula, the parameters f and η are calculated from Eq. (8) and Eq. (9) for typical projectiles H, D, T and He, which are listed in Tables 5, 6

7 and 8, where the calculated parameters η correspond to 1 keV ion.

For calculations of the angular dependence of heavy-ion sputtering, 26 Sigmund f of m = 1/3 and ψ for 1 eV ion are also calculated and

listed in Tables 9 through 18, where as the

typical projectiles C, Al, Ar, Fe, Ni, Cu, Kr, Xe and Hg ions are selected.

The plots of the angular dependence of sputtering yields for various combinations of the incident ions and the target atoms are shown in Figs. 6 through 58, where Figs. 6 through 24 correspond to light-ion sputtering and Figs. 25 through 58 to heavy-ion sputtering. The solid lines in these figures are best fit curves to the present empirical formula, and the solid lines with cross marks show the results calculated by putting the average values of the best-fit parameters into each empirical formula.

In order to know the absolute yield $Y(\theta)$, one must calculate the sputtering yield at normal incidence. The authors recommend to use the third Matsunami formula for the sputtering yield at normal incidence, which has the form³²

$$Y(E) = P - \frac{s_n(\varepsilon)}{1 + 0.35U_s s_e(\varepsilon)} [1 - (E_{th}/E)^{\frac{1}{2}}]^{2.8}, \qquad (21)$$

where

$$P = 0.042 - \frac{E_{L}}{R_{L}} - \frac{N}{U_{s}} \alpha (M_{2}/M_{1})Q(Z_{2}), \qquad (22)$$

$$R_{\rm L} = \frac{1}{\pi a^2 N \gamma} , \qquad (22)$$

$$s_e(\varepsilon) = k \varepsilon^{\frac{1}{2}}$$
 , (23)

and $s_n(\varepsilon)$ is the LSS elastic stopping cross section in the reduced unit and the following analytical expression is useful for the present purpose:²

$$s_{n}(\varepsilon) = \frac{3.441\sqrt{\varepsilon}\log(\varepsilon + 2.718)}{1 + 6.355\sqrt{\varepsilon} + \varepsilon(-1.708 + 6.882\sqrt{\varepsilon})} \qquad (24)$$

The inelastic coefficient k of $s_e(\epsilon)$ is given as³³

$$k = 0.0793 Z_{1}^{1/6} \frac{(Z_{1}Z_{2})^{\frac{1}{2}} (M_{1} + M_{2})^{3/2}}{(Z_{1}^{2/3} + Z_{2}^{2/3})^{3/4} M_{1} (M_{1}M_{2})^{\frac{1}{2}}}, \quad (25)$$

and the threshold energy E_{th} for the third Matsunami formula has the following empirical relation:

$$E_{\text{th}} = U_{\text{s}} [1.9 + 3.8(M_{1}/M_{2}) + 0.314(M_{2}/M_{1})^{1.24}].$$
(26)

The parameter $\alpha(M_2/M_1)$ is represented as

$$\alpha (M_2/M_1) = 0.08 + 0.164 (M_2/M_1)^{0.45} + 0.0145 (M_2/M_1)^{1.29}$$
(27)

and $Q(Z_2)$ is listed in Table 4 for each element. For extensive uses of the third Matsunami formula, the parameters E_L , P, E_{th} , α and k are listed in Tables 19 through 32 for various ion-target combinations, where as the projectile H, D, T, He, C, Ne, Al, Ar, Fe, Ni, Cu, Kr, Xe and Hg are selected.

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References

- 1) J. Bohdansky, J. Roth, and H.L. Bay, J. Appl. Phys. <u>51</u>, 2861 (1980)
- 2) N. Matsunami, Y. Yamamura, Y. Itikawa, N. Itoh, Y. Kazumata,
 - S. Miyagawa, K. Morita, and R. Shimizu, Radiat. Eff. Lett. 50, 39 (1980).
- 3) Y. Yamamura, N. Matsunami, and N. Itoh, Radiat. Eff. Lett. <u>68</u>, 83 (1982).
- 4) N. Matsunami, Y. Yamamura, Y. Itikawa, N. Itoh, Y. Kazumata,
 - S. Miyagawa, K. Morita, and R. Shimizu, Report IPPJ-AM-14,Institute of Plasma Physics, Nagaya University (1980).
- 5) J. Roth, J. Bohdansky, and W. Ottenberger, IPP 9/26, Max-Plank-Institut fur Plasmaphysik (1979).
- 6) G.K. Wehner, J. Appl. Phys. 30, 1762 (1959).
- 7) P.K. Rol, J.M. Fluit, and J. Kistemaker, Physica 26, 1000 (1960).
- V.A. Malchanov and V.G. Tel'kovskii,
 Soviet Phys. Doklady <u>6</u>, 137 (1961).
- 9) D. Almen and G. Bruce, Nucl. Instr. Methods 11, 257 (1961).
- 10) I.I. Dushkov, V.A. Malchanov, V.G. Tel'chanov, V.M. Chicherov, Soviet Phys. - Technical Phys. 6, 735 (1962).
- 11) C.E. Ramer, M.A. Narasimham, H.K. Reynolds, and J.C. Allred, J. Appl. Phys. <u>35</u>, 1673 (1964).
- 12) E.S. Mashkova and V.A. Malchanov,

Soviet Phys. - Technical Phys. 9, 1601 (1965).

- 13) K.B. Cheney and E.T. Pitkin, J. Appl. Phys. <u>36</u>, 3542 (1965).
- 14) G. Dupp and A. Scharmann, Zeit. Phys. <u>194</u>, 448 (1966).
- 15) L.N. Evdokimov and V.A. Malchanov, Can. J. Phys. 46, 779 (1968).
- 16) H. Ismail and A. Septier,

Proc. 3rd Int. Symp. on Discharges and Electrical Insulation in Vacuum, (1968) p 95.

- 10 -

- 17) G. Holmen and Q. Almen, Ark. Fys. 40, 429 (1970).
- 18) A.J. Summers, N.J. Freeman, and N.R. Daly, J. Appl. Phys. 42, 4774 (1971).
- 19) H. Oechsner, Z. Phys. 261, 37 (1973).
- 20) H.L. Bay and J. Bohdansky, Appl. Phys. 19, 421 (1979).
- 21) H.L. Bay, J. Bohdansky, W.O. Hofer, and J. Roth, Appl. Phys. 21, 327 (1980)
- 22) W. Kruger, A. Scharmann, H. Afrid, and G. Brauer, Proc. of Symposium on Sputtering, Perchtoldsdorf/Wien, Austria (1980), p. 28.
- 23) D.A. Thompson and S.S. Johar, Radiat. Eff. 55, 91 (1981).
- 24) J. Bohdansky, G.L. Chen, W. Eckstein, J. Roth, and B.M.U. Scherzer, J. Nucl. Mater. 111&112, 717 (1982).
- 25) J. Bohdansky, Nucl. Fusion (to be published).
- 26) P. Sigmund, Phys. Rev. 184, 383 (1969).
- 27) M.W. Weissmann and P. Sigmund, Radiat. Eff. 19, 7 (1973).
- 28) Y. Yamamura, N. Matsunami, and N. Itoh, Radiat. Eff. 71, 65 (1983).
- 29) K.B. Winterbon, P. Sigmund, and J.B. Sanders, Mat.-Fys. Medd. Dan. Vid. Selsk. 37, 14 (1970)
- 30) W. Takeuchi and Y. Yamamura, Radiat. Eff. 71, 53 (1983).
- 31) Y. Yamamura, Radiat. Eff. (to be published).
- 32) N. Matsunami, Y. Yamamura, Y. Itikawa, N. Itoh, Y. Kazumata,
 - S. Miyagawa, K. Morita, and R. Shimizu,

ATOMIC DATA AND NUCLEAR DATA TABLES (to be published).

33) J. Lindhard, M. Scharff, and H.E. Schiott,

Mat.-Fys. Medd. Dan. Vid. Selsk. 33, No.14 (1963).

- 34) R. Behrisch, G. Maderlechner, B.M.U. Scherzer, and M.T. Robinson, Appl. Phys. 18, 391 (1981).
- 35) Y. Yamamura, Radiat. Eff. 55, 49 (1980).

APPENDIX A: ANGULAR DEPENDENCE OF THRESHOLD ENERGY OF LIGHT-ION SPUTTERING AND HEAVY-ION SPUTTERING

The sputtering mechanism for oblique incidence is separated into three parts: 1) The mechanism due to the direct knock-out collisions with incident ions at the outermost layer of the solid surface (mechanism Ia of Fig. Al). 2) The mechanism due to collision cascades created by incoming ions near the solid surface (mechansim Ib of Fig. Al) 3) The mechanism due to collision cascades generated by ions backscatted from the interior of the solids (mechanism II of Fig. Al).



Fig. Al Schematic representation of sputtering mechanism at oblique incidence

For light-ion sputtering the mechanisms Ia and II play an important role.

The threshold energy of mechanism II is given as 3^{34}

$$E_{th} = \frac{U_s}{\gamma} \frac{1}{(1 - \gamma)}$$
(A1)

for normal incidence. For not-too-large angles of incidence, the factor $(1 - \gamma)$ of Eq. (Al) must be modified. If only a single collision process is taken into consideration, the threshold energy will be a slightly decreasing function of the angle of incidence. For oblique incidence, however, the multiple scattering becomes important and this effect weaken the angular dependence of the factor $(1 - \gamma)$. Roughly speaking, the threshold energy of mechanism II is

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$$E_{\rm th} = \frac{U_{\rm s}}{\gamma} \frac{1}{1 - \gamma \cos^2(\theta/2)}$$
(A2)

for not-too-oblique incidence, where the difference of the scattering angles between in the L system and in the CM system is neglected because of large mass ratio.

For oblique incidence, an incoming ion must penetrate the first layer for mechanism Π . The average potential at the surface of the amorphous solids is roughly estimated by

$$U_{R}(y) = \frac{1}{R_{0}^{3}} \int_{-R_{0}/2}^{+R_{0}/2} \int_{0}^{\infty} 2\pi r dr \ V(\sqrt{(y-z)^{2}+r^{2}}), \quad (A3)$$

where \dot{y} is the distance from the surface and V(r) is the interatomic potential. If one employ the Moliere potential as the interatomic potential we have

$$U_{R}(y) = 4 \pi \frac{A}{A+1} E_{L}(\frac{a}{R_{0}})^{3} \sum_{i=1}^{3} \frac{\alpha_{i}}{\beta_{i}^{2}} \sinh(\frac{\beta_{i}R_{0}}{2a}) \exp(-\frac{\beta_{i}}{a}y) ,$$

$$A = M_{0}/M_{1}, \qquad (A4)$$

where

$$A = M_2/M_1,$$

$$\alpha_i = (0.35, 0.55, 0.10)$$

$$\beta_i = (0.3, 1.2, 6.0).$$

The critical angle for penetration through the first layer is given as

$$\psi_{\rm c} = \cos^{-1} \left[\frac{U_{\rm R}^{(0)}}{E} \right]^{\frac{1}{2}} , \qquad (A5)$$

where ψ_{c} is measured from the surface normal. The critical angle ψ_{c} for the incident energy of the order of the threshold energy is about 50° for H - Ni. For $\theta < \psi_{c}$, E_{th} of the mechanism II is given by eq.(2).

For grazing angles of incidence ($\theta > 70^{\circ}$), the direct knock-out process become important and the criterion of the sputtering due to this process is given by ³¹

$$\cos\theta + 2q < 1 \tag{A7}$$

$$p_2 > p_1 > R_0 \cos \theta \tag{A8}$$

where $q = (U_s/\gamma E)^{\frac{1}{2}}$ and the impact parameters p_1 and p_2 are the lower and the upper limits of the impact parameters available for the sputtering due to the direct knock-out process.

From the inequality of Eq. (A7) we obtain

$$E_{th}(\theta) = \frac{U_s}{\gamma} \frac{1}{\sin^4(\theta/2)}$$
 (A9)

The criterion of Eq. (A8) is not important as compared with surface channeling for oblique incidence. Namely, in order to knock off an atom at the outermost layer, an ion must arrive at the surface. This leads to the following expression for the threshold energy:

$$E_{th}(\theta) = \frac{U_R(R_0/2)}{\cos^2 \theta}$$
(A10)

where $U_R(R_0/2)$ is the average potential at the distance $R_0/2$, at which there exists an atom with a finite probability in the case of the random target. From Eq. (A4), $U_R(R_0/2) \simeq U_R(0)/2$.



Fig. A2
The angular dependence of the threshold energies for H + Ni.
mechanism II direct knock-out process surface channeling

In Fig. A2 the threshold energies corresponding to each mechanism are plotted against the angle of incidence. Figure A2 tells us that the threshold energies corresponding to the direct knock-out process can be neglected. Finally we get

$$E_{th}^{L}(\theta) = \begin{cases} \frac{U_{s}}{\gamma} & \frac{1}{1 - \gamma \cos^{2}(\theta/2)} & \text{for not-too-oblique incidence} \\ \frac{26.85}{1 + A} & E_{L} \left(\frac{a}{R_{0}}\right)^{2} \\ \frac{\cos^{2}\theta} & \text{for grazing angles of incidence} \end{cases}$$

When the incident energy is very low, sputtered atoms will be ejected before they lose the memory of the direction of the incident ion beam. This means that the velocity distribution of recoil atoms generated by incoming heavy-ions is anisotropic. Taking into account the anisotropic effect of the recoil flux, Yamamura showed that the angular dependence of the heavy-ion sputtering was proportional to $\cos^2 \theta^{35}$.

For grazing angles of incidence, the surface channeling will play an important role. In the case of heavy-ion sputtering, the threshold energy due to surface channeling is given by

$$E_{th}(\theta) = \frac{U_R(y_{min})}{\cos^2 \theta}, \qquad (A12)$$

where y_{\min} is the minimum distance above which the projectile will be reflected without producing any recoil atom available for sputtering. For the amorphous solid surface the minimum distance y_{\min} may be of the order of

$$y_{\min} = -\frac{R_0}{2} + p_{\min}$$
, (A13)

where p_{min} is the collision diameter for the Moliere potential and depends on the incident energy. Since the incident energy of present interest is very low, p_{min} is roughly given by

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where s is the solution of the following transcendental equation: $\epsilon = \exp(-0.3s)/s$.

Let us consider a typical example, i.e., $Ar^+ - Cu$. In this case, s is nearly equal to 15. In Fig. A3 the angular dependence of threshold energy for $Ar^+ - Cu$ is plotted as a function of the angle of incidence. Finally, we have

$$E_{th}^{H}(\theta) = \begin{cases} E_{th}^{(0)} \cos^{2}\theta & \text{for not-too-oblique incidence} \\ \frac{0.3 \frac{A}{A+1} E_{L}^{(\frac{a}{R_{0}})^{3}}}{\cos^{2}\theta} & \text{for grazing angles of incidence} \end{cases}$$
(A14)

where $E_{th}(0)$ is the threshold energy at normal incidence, and y_{min} is set to equal to $R_0/2 + 15a$.



ANGLE OF INCIDENCE (DEGREE)

				•]	Car	get							
References	Ion	C	A1	. Ti	Fe	Ni	Cu	Zr	Nb	Мо	Pđ	Ag	Та	W	Pt	Au
Wehner (1959)	Hg				0	0				0		0	0	0	0	
Rol et al. (1960)	Ar						ο		1							
Marchanov et al. (1961)	Ar						ο									
Almen et al. (1961)	Kr						ο									
Dushikov et al. (1962)	He N Ne						0 0 0									
	Ar						0						_			
	Ar						0						0			
Marchanov et al. (1965)	Ar						ο			0				0		
Cheney et al. (1965)	Ar Xe						0 0			0				о		
Dupp et al. (1966)	Ar						ο									
Evdokimov et al. (1968)	Ne Ar Kr						0 0			0 0						
Ismail et al. (1968)	Hg						ο									
Holmen et al. (1970)	Hg	o			0											
Summers et al. (1971)	D He Nb						0 0 0									
Oechsner (1973)	He Ne Ar Kr Xe		o	ο		ο	0 0 0 0	o			0	ο	ο	ο		0
Bay et al. (1979)	H D He					0 0				0 0 0						
Bay et al. (1980)	н					ο										
Kruger et al. (1980)	Ar			ο					ο			ο				
Thompson et al. (1980)	P Sb Bi											0 0 0			C)
Bohdansky et al. (1982)	H D He			0 0		0	0			0 0 0			0 0			
Bohdansky (1983)	Н					ο										

Table] Ion-target combinations in the present data compilation

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				ومراجع والمتحد المتحد المتحال المحاولة ويعتقد ويريدا فالتعاد ويستعادين والم	
			Best-fit	values	_
Energy	Ion	Target	f	^θ opt	Ref.
450 eV	Н	Nİ	1.62	74.4°	25
l keV	н	Ni	2.34	78.3°	20
4 keV	.H	Ni	2.27	82.3°	20
450 eV	н	Ni	2.19	78.7°	20
l keV	н	Ni	2.32	82.9°	30
4 keV	н	Ni	2.62	84.2°	30
l ĸeV	D	Ni	1.88	80.4°	25
100 eV	He	Ni	3.20	56.3°	30
500 eV	He	Ni	3.30	66.l°	30
l keV	He	Ni	2.50	72,1°	30
4 keV	He	Ni	2.09	79.0°	30
4 keV	He	Ni	1.52	80.5°	20
50 keV	н	Cu	1.88	82.1°	24
1.05 keV	He	Cu	1.55	66.5°	19
2 keV	Н	Мо	2.40	81.8°	20
8 keV	H	Мо	2.80	82.0°	20
2 keV	D	Мо	1.98	82.0°	20
4 keV	He	Мо	2.23	77.3°	20
l keV	н	Au	1.14	78.0°	20
4 keV	Н	Au	1.53	79.5°	20
l keV	D	Au	1.22	79.2°	20

Table 2 Best-fit parameters of the present empirical formula for light-ion sputtering

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_		Best-fit	values	
Ion	Target	f	⁰ opt	Rei.
Ar	Cu	35.4	44.2°	30
Ar	Cu	9.33	46.1°	30
Ar	Cu	5.25	43.6°	30
Ar	Cu	3.35	49.6°	30
Ar	Cu	3.07	55 .7°	30
Ar	Cu	2.66	65.7°	30
Ar	Cu	2.19	75.0°	30
Hg	Ni	37.1	47.5°	30
Hg	Ni	15.0	52.5°	30
Hg	Ni	5.01	61.2°	30
Hg	Ni	4.02	63.3°	30
Hg	Ni	3.56	64.7°	30
Ni	Ni	22.8	44.2	30
Ni	Ni	11.8	45.5°	30
Ni	Ni	3.75	50.5°	30
Ni	Ni	3.05	56.2°	30
Ni	Ni	3.13	64.2°	30
Ni	Ni	3.37	66.4°	30
Hg	Ni	12.8	48.2	6
Hg	Ni	8.57	51.0°	6
Hg	Fe	15.5	57.6°	6
Hg	Fe	9.53	60.7°	6
Hg	Мо	26.0	53.0°	6
Hg	Мо	26.9	50.9°	6
Hg	Та	15.0	62.0°	6
Hg	W	5.87	58.3°	6
Hg	W	10.6	52.8°	6
Hg	W	7.64	56.1°	6
	Ion Ar Ar Ar Ar Ar Ar Ar Hg Hg Hg Hg Hg Hg Hg Hg Hg Hg Hg Hg Hg	IonTargetArCuArCuArCuArCuArCuArCuArCuHgNiHgNiHgNiHgNiNiNiNiNiNiNiNiNiHgNiHgNiHgNiHgNiNiNiNiNiNiNiNiNiHgNiHgFeHgFeHgMoHgMoHgWHgWHgWHgWHgW	Best-fitIonTargetBest-fit f f Ar Cu 35.4 Ar Cu 9.33 Ar Cu 3.25 Ar Cu 3.35 Ar Cu 3.07 Ar Cu 2.66 Ar Cu 2.19 Hg Ni 37.1 Hg Ni 5.01 Hg Ni 5.01 Hg Ni 5.01 Hg Ni 5.01 Hg Ni 3.56 NiNi 3.56 NiNi 3.13 NiNi 3.13 NiNi 3.37 Hg Ni 12.8 Hg Ni 8.57 Hg Fe 15.5 Hg Fe 9.53 Hg Mo 26.0 Hg Mo 26.0 Hg Mo 26.9 Hg Ta 15.0 Hg W 5.87 Hg W 10.6 Hg W 10.6 Hg W 10.6	Best-fit valuesIonTarget f θ_{opt} ArCu35.444.2°ArCu9.3346.1°ArCu5.2543.6°ArCu3.3549.6°ArCu3.0755.7°ArCu2.6665.7°ArCu2.1975.0°HgNi15.052.5°HgNi5.0161.2°HgNi5.0161.2°HgNi3.5664.7°NiNi3.7550.5°NiNi3.1364.2°NiNi3.1364.2°NiNi3.3766.4°HgNi12.848.2HgNi15.557.6°NiNi3.3766.4°HgNi12.848.2HgNi8.5751.0°HgFe15.557.6°HgFe9.5360.7°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°HgMo26.053.0°Hg

Table 3 Best-fit parameters of the present empirical

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formula for heavy-ion sputtering

-		T	m	Best-fit va	lues	Dof
Ene	ərgy	ION	Target	£.	^θ opt	Rel.
1.05	keV	Ar	Al	2.10	70.2°	19
1.05	keV	Ar	Ti	2.04	68.8°	19
1.05	.keV	Ar	Ni	1.72	69.5°	19
1.05	keV	Ne	Cu	1.03	70.6°	19
1.05	keV	Ar	Cu	1.29	69.8°	19
1.05	keV	Kr	Cu	2.19	66.9°	19
550) eV	Xe	Cu	9.40	53.8°	19
1.05	keV	Xe	Cu	4.56	61.5°	19
1.55	keV	Xe	Cu	3.89	64.0°	19
2.05	keV	Xe	Cu	2.44	69.0°	19
1.05	keV	Ar	Zr	1.73	67.7°	19
1.05	keV	Ar	Pd	1.85	63.1°	19
1.05	keV	Ar	Ag	1.50	63.7°	19
1.05	keV	Ar	Та	1.75	67.5°	19
1.05	keV	Ar	Au	1.50	59.8°	19
						10
37	keV	Ar	Cu	1.16	71.90	T3
30	keV	Xe	Cu	1.94	75.0°	13
9.5	keV	Xe	Cu	2.53	69.5°	13
30	keV	Xe	Mo	2.58	76.7°	13
30	keV	Xe	W	1.33	78.5°	13
9.5	keV	Xe	W	1.07	76.0°	13

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Table 4 Some physical constants for calculations of sputtering yields.
Table 5 through 8
The parameters for the angular dependence of light-ion sputtering.
The correspondence between Tables and projectiles are as follows:
H : Table 5
D : Table 6
T : Table 7
He : Table 7
He : Table 8
Let us show briefly how to use these tables and suppose the angular dependence of 4 keV H⁺ → Ni is desired.
The appropriate table is Table 5. From Table 5 we have

 $f = (4.44)^{\frac{1}{2}} \times (0.94 - 0.00133 \times 58.24) = 1.82$,

where figures in italics corresponds to values in Table 5. The quantity η is inversely proportional to $E^{1/4}$ and so we get

 $\eta = (\frac{1}{4})^{1/4} \times 0.1535 = 0.1085$.

From Eq. (12) θ_{opt} can be calculated as follows:

 $\theta_{\text{opt}} = 90^{\circ} - 57.3 \times 0.1085 = 83.8^{\circ}.$

Since $\Sigma = f \cos \theta_{opt}$, we have

 $\Sigma = 1.82 \cos 83.8^\circ = 0.197.$

Finally, we have the following angular dependence for 4 keV $H^+ \rightarrow Ni$:

$$\frac{Y(\theta)}{Y(0)} = x^{1.82} \exp[-0.197(x-1)],$$

where $x = 1/\cos \theta$

Tables 9 through 18

The parameters for the angular dependence of heavy-ion sputtering.

The correspondence between Tables and projectiles are as follows:

С	:	Table	9	Ne	:	Table	10
Al	:	Table	11	Ar	:	Table	12
Fė	:	Table	13	Ni	:	Table	14
Cu	:	Table	15	Kr	:	Table	16
Xe	:	Table	17	Hg	:	Table	18

Let us show briefly how to use these table for calculations of the angular dependence of heavy-ion sputtering. Then, suppose the angular dependence of 1 keV $\operatorname{Ar}^+ \longrightarrow \operatorname{Cu}$ is desired. The appropriate table is Table 15. Fist of all, we must calculate the quantity ζ

 $\zeta = 1 - (E_{th}/E)^{\frac{1}{2}} = 1 - (20.72/1000)^{\frac{1}{2}} = 0.8561.$

Since $f_s = 1.71$, the parameter f is calculated from Eq. (17),

 $f = 1.71 \times (1 + 2.5 \times 0.1439/0.8561) = 2.43$

The quantity ψ is inversely proportional to \sqrt{E} , which is known from Eq. (18). Then, we have

 $\psi = 0.1305/\sqrt{1000} = 0.004127$.

From Eq. (20) we get

 $\theta_{\text{opt}} = 90^{\circ} -286 \times 0.004127^{0.45} = 65.8^{\circ}$

The relation $\Sigma = f \cos \theta_{opt}$ yields

 $\Sigma = 2.43 \cos 65.8^\circ = 0.9961.$

In the above calculations, figures in italics are the values in Table 15. Finally, we get the following angular dependence for 1 keV $Ar^+ \rightarrow Cu$;

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 $\frac{Y(\theta)}{Y(0)} = x^{2.43} \exp[-0.9961(x - 1)].$

where $x = 1/\cos \theta$.

Table 19 through 32

The parameters for the third Matsunami formula, where the correspondences between Tables and projectiles are as follows:

H	:	Table	19	D	:	Table	20	т	:	Table	21
He	:	Table	22	С	:	Table	23	Ne	:	Table	24
Al	:	Table	25	Ar	:	Table	26	Fe	:	Table	27
Ni	:	Table	28	Cu	:	Table	29	Kr	:	Table	30
Xe	:	Table	31	Hg	:	Table	32.				

Let us show how to use these tables for calculations of sputtering yields at normal incidence by the third Matsunami formula. Suppose the sputtering yield of 1 keV H^+ — Ni is desired. The appropriate table is Table 19. The reduced energy ε for 1 keV $Ar^+ \rightarrow Ni$ is calculated like this

 $\varepsilon = 1000/(2.799 \times 1000) = 0.3572.$

Direct insertion of this value into Eqs. (23) and (24) yields

 $s_{e}(\varepsilon) = 4.35 \times \sqrt{0.3572} = 2.60$

 $s_{n}(\epsilon) = 0.408$.

Since P = 0.4814 and $E_{th} = 100.6$, we have

 $Y = 0.4814 \times 0.408/(1 + 0.35 \times 4.44 \times 2.60)$ $\times [1 - (100.6)^{\frac{1}{2}}]^{2.8} = 1.33 \times 10^{-2} (\text{atoms/ion}),$

where $U_s = 4.44$ eV is in Table 4, and in the above calculations figures in italics corresponds to those in the present tables.

4.003 He 2. 1.77 0 1.77 0 1.56 .02 1.56 .02 1.56 .02 1.78 .08 Ar 19 Ar 19 1.78 .08	83.8 1 1 30 1 3.57	131.3 xe 54 xe 54 1.77 4.4 4.4 1.87 1.87 1.87 1.87 1.87 1.87 1.87 1.87 1.87 1.87 1.87 1.87 1.73 1.87 1.73 1.07 1.07 1.73 1.74 1.73 1.73 1.73 1.73 1.73 1.74 1.73 1.73 1.73 1.73 1.74 1.73 1.74 1.73 1.74 1.73 1.74 1.73 1.74 1.73 1.74 1.73 1.74 1.74 1.73 1.74 1.74 1.73 1.74 1.74 1.74 1.74 1.74 1.74 1.74 1.74 1.74 1.74 1.74 1.74 1.74 1.74 1.73 1.74 1.74 1.73 1.74 1.74 1.73 1.74
19 F 9 1.97 .84 1.97 .84 35.45 2.09 1.4 1 7.05	79.91 Br 35 4.1 1.22 1 3.19	126.9 1326.9 1,941;11 1,941;11 1,955 1,971,0 1,971,0 1,971,0 1,971,0 1,971,0
16 1.45 2.65 1.45 2.65 32.06 5 2.65 1 2.95	78.96 Se 34 4.79 2.25 1 3.02	127.6 Te 52 6.24 2.33 1.24 3.23 210 210 1.4 1.5 1.4 3.34 1.68.9 1.68.9 1.68.9 1.5 3.12 1.5 3.12
14.01 N 7 1.03 4.92 1.03 4.92 1.03 4.93 1.82 3.43 1.83 3.05	74.92 As 33 5.72 2.96 1 2.8	121.7 5b 51 5b 51 1.6.2 2.75 1.6.2 2.75 1.6.2 2.18 1. 3.13 1.5.29 1.5.29 1.5.29 1.5.29
12.01 C 6 2.29 7.37 2.96 2.07 2.95 2.07 51 14 51 14 51 2.35 2.62 2.35 2.63	72.59 6e 32 5.32 3.85 .84 2.83	118.6 5n 50 7.3 5.14 7.3 5.14 11.4 2.03 11.4 2.03 11.4 2.03 11.4 2.03 1.64.9 1.0 5.12 1.0 5.12
10.81 8 5 2.34 5.77 1 1.98 61 15 26.98 61 15 2.1 2.56	69.72 6a 31 5.91 2.81 1 2.7	114-18 10 49 1. 22-52 1. 22-52 1. 22-97 1. 32-97 1. 32-97 1. 32-18 1. 12.52 1. 52-94 1. 32-14 1. 32-14 1
,	65.38 2n 30 7.14 1.35 1 2.48	112.4 Cd 48 8.65 1.16 1 2.77 1 2.77 1 2.77 1 2.77 1 2.77 1 2.79 1 2.79 1 2.97 1 2.97 1 2.97 1 2.97 1 2.97 1 2.97 1 2.91 1 2.91 1 3.94 1 3.94
	43.55 Cu 29 8.96 3.49 1.33 2.28	107.8 Ag 47 10.5 2.95 11.13 2.88 196.9 196.7 115 2.81 197.2 1157.2 1157.2 1157.2
.2	58.71 N1 28 8.9 4.44 1.11 2.22	106-4 Pa 45 125 2:49 195 1:05 2:48 Pt 78 1:03 2:48 1:03 2:48 1:03 2:48 1:03 2:48 1:03 2:48 1:03 2:48
gy (eV) Constant R ₀ (58.93 Co 27 B.9 4.39 1.13 2.23	102.9 Rh 45 112.4 5.75 11.22 2.42 11.22 2.42 120.5 6.94 11.25 2.42 11.25 2.42 11.52 2.42 1.55 5.49
is Number mic Number jimation Ener rage Lattice Random Target	55.85 Fe 26 7.86 4.28 1.12 2.28	101 Ru 44 112.2 6.74 113.2 5.4 1145 1145 1145 1145
	54.93 Mn 25 7.43 2.92 1.21 2.31	98.91 Tc 45 11.5 2.45 11.5 2.45 Re 75 21.6 2.45 144.2 144.2 1.16 2.46 7 3.44 144.2 1.6 2.45 1.6 2.45 1.6 2.45 1.16 2.75 1.16 2.75 1.17 2.75 1.16 2
20cmula	52 Cr 24 7.19 4.1 1.27 2.29	93.94 Ho 42 10.2 6.82 .91 2.55 .91 2.55 .91 2.55 .91 2.55 .97 3.76 .6.77 3.77 .15.4 0 .15.4 0 .15.4 0 .15.4 0 .5.78
Symbi Benaity (g/cr Le of the Jrd- Leni Empirical	50.94 v 23 6.1 5.31 .88 2.41	2.91 Nb 41 B.4 7.57 .93 2.64 190.9 140.1 140.1 140.1 140.1 140.1 13.26 232 232 232 232 232 13.7 5.26 117 5.26 238 140.1 140.1 17 5.26 238 140.14
Q valt Matsur	47.9 T1 22 4.51 4.85 .59 2.61	91.22 2r 40 6.49 6.23 6.7 2.80 178.4 178.4 13.1 6.44 13.1 6.44
	44.95 Sc 21 2.99 3.9	88.91 48.91 Y 39 1 4.57 1 5.22 6.17 4.47 6.17 4.45 1 1.138.9 1 1.133.9 1 1.133.9 1 1.133.9 1 1.133.9 1 1.133.9 1 1.133.3 1 1.335.5 1 1.335.5
9.012 Be 4 1.85 5.32 2.15 2.01 24.5 60 12 1.74 1.51 1.72 2.66	40.08 Ca 20 1.54 1.84 1 3.52	97.42 5r 38 5r 38 1.72 1.5.83 1.5.53 1.5.544 1.5.5444 1.5.5444 1.5.54444 1.5.54444444444
1.008 H 1 1.008 0 1.089 0 6.941 L1 3 1.53 1.63 1.63 1.63 1.63 1.63 1.63 1.63 1.63	39.07 k 19 .86 .92 1 4.23	85.47 Rb 37 1.53 .85 1.53 .85 1.9 .89 1.9 .89 1.0 0

TABLE f 4 PHYSICAL CONSTANTS FOR THE THIRD MATSUNANT FORMULA AND THE PRESENT EMPIRICAL FORMULA

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	.1238	۲۹ ۲۹	3.971 0 0 0	.7665	Ne 10	20.02.02 .4286.13	1142.1	Ar 18	39.62 .08 .2618 .25	3.8636	х х	83.13 .12 .2352 .29	6.5396	Xe 54	130.3 .16	12.019	Rn Bb	220.2.2	9.3504	Lu 71	173.5 4.43					
				.6723	F P	18.85 .84 .1807 .84	1.4826	CI 17	35.17 1.4 .1419 1.06	3.7263	Br • 35	79.28 1.22	6. 3829	8	125.9 1.11	11.838	At 85	208.3 0 0 0	9.1782	V5 70	171.6 1.6					
				.5845	8 0	15.87 2.6 .1301 1.48	1.3752	S 16	31.81 2.85	3.5886	Se 34	78.33 2.25	6.2252	Te 52	126.6 2.23	11.655	Po 84	208.3 1.5 .1422 .81	5.0075	Tm 69	167.6 2.42 .1334 1.12					
				4978	z	13.9 4.92 .1022 2.04	1.2669	۹ ت	30.72 3.45	3.4539	As 33	74.33 2.96	6.0711	Sb 51	120.7 2.75	11.473	B1 83	207.2 2.18 .1311 .98	8,8368	Er 69	165.9 3.29 .124 1.3					
				.4146	c 6	11.91 7.37	1.1632	Si 14	27.86 4.63	3.3195	Ge 32	72.01 3.85	5.9168	Sn 50	117.7 3.14	11.292	Pb 82	205.5 2.03	8.6671	Ho 67	163.6 3.14 .1245 1.28					
				.3328	Ω Ω	10.72 5.77	1.0592	AI 13	26.77 3.39 .1319 1.67	3.1868	Ga 31	69.17 2.81 .1405 1.42	5. 7638	In 49	113.9 2.52	111.111	11 61	202.7 1.88 .1455 .92	B.4983	Dy 66	161.2 3.04					
										3.0564	Zn 30	64.86 1.35 .1846 .99	5.6113	Cd 48	111.5 1.16	10.932	Hg B0	198.9 .67 .1987 .55	8.3306	Tb 65	157.6 4.05					
										2.9258	Cu 29	63.05 3.49 .1576 1.6	5.4607	Ag 47	106.9 2.95	10.754	Au 79	195.3 3.81	8.1632	Gd 64	156 4.14 .1139 1.49					
										2.7988	N1 28	58.24 4.44 .1535 1.82	5.3097	Pd 46	105.6 3.89 .1467 1.58	10.575	Pt 78	193.5 5.84 .1354 1.65	7.9979	Eu 63	150.7 1.86					
						gy (eV) Souttering				2.6693	Co 27	58.46 4.39 .1512 1.81	5.1608	Rh 45	102.1 5.75	10.398	Ir 77	190.7 6.94 .1328 1.81	7.8321	Sm 62	149.1 2.14 .1323 1.08					
A			000		mic Number	limation Ener or Light-Ion				2.5439	Fee 26	55.41 4.28 .1489 1.79	5.0121	Ru 44	100.2 6.74	10.221	0s 76	188.7 8.17 .1278 1.97	7.6685	Pm 61	143.8 0 0 0				1	
UTTERING VIEL			~ ^E L ^{/1}	13	4 - Ato	3.32 1.69				2.4183	Чл 25	54.49 2.92 .1601 1.48	4.8646	Tc 43	98.13 6.85 .1282 2.12	10.046	Re 75	184.7 8.03 .1259 1.97	7.5041	OS PN	143.1 3.4 .1166 1.38	13.131	U 92	236.1 5.55 .1245 1.47		
LIGHT-ION SPI 1 1.008				.25	1	B.94 .1438				2.2958	Cr 24	51.59 4.1 .1483 1.76	4.7186	Mo 42	95.18 6.82 .1247 2.12	9.8707	ы 74	182.3 8.9 .1201 2.08	7.3416	Pr 59	139.8 3.7 .1138 1.45	12.945	Pa 91	229.2 0 0 0		
DEPENDENCE OF ILEH MBER					Symbo	Ratio (M2/M1 for 1 keV Ion				2.1734	23	50.54 5.31 .1308 2.01	4.5738	ND 41	92.17 7.57	9.6965	Ta 73	179.5 8.1	7.1789	Ce 58	139 4.32	12.758	Th 90	230.2 6.2 .1036 1.58		
i for Angular Project Z - Nu Mass-N						α S S S S S S S S S S S S S S S S S S S				2.0542	11 22	47.52 4.85 .1235 1.93	4.4294	2r 40	90.5 6.25 .111 2.05	9.5229	HF 72	177 6.44		/	/		/			
PARAMETERS					<u>.</u>					1.9367	Sc 21	44.55 3.9 .1161 1.74	4.2865	۲ 39	ab.2 4.37 .1075 1.72	7.0174	La 57	1.7.8 4.47	12.573	Ac 89	225.2 4.25					
TABLE 5				.2565	Be 4	8.94 3.32 .1438 1.69	.9597	Mg 12	24.11 1.51 .1441 1.12	1.8231	Ca 20	39.76 1.84 .118 1.2	4.1441	s. 38	86.92 1.72 .1135 1.09	6.8569	Ba 56	136.2 1.9	12.387	Ra 88	224.2 1.66 .1092 .83					
	69B0.	ч н	•• -•	. 1853	с Г	4.886 1.63 .1178 1.19	-B60b	II AN	22.82 1.11 .1282 .96	1.7071	k 19	38.78 .93 .1151 .86	4.0034	8 0 31	84.79.85 1141.76	6.6983	Cs 55	131.8 .8 .1102 .68	12.203	Fr 87	221.2 0 v c				, ,	

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		_			_	_		-									_	_							
	.1486	He 2 .	1.958 0 0 0		.8029	Ne 10	10.02 .02	1.6302	År 18	19.83 .08 .3112 .26	3.9095	Kr [.] 36	41.61 .12 .2796 .31	6-5893	Xe 54	65.19 .16 .2468 .34	12.073	Rn B	110.2.2	9.4039	Lu 71	86.84 4.43 .1373 1.74			
					1901.	o L	9.434 .84 .2149 .85	1.5235	C1 12	17.6 1.4 .1687 1.08	3.7726	Br 35	39.68 1.22 .1756 .98	6.4331	1 53	63.01 1.11 .1685 .9	11.894	At 85	104.3 0 0 0	9.2313	Yb 70	85.9 1.6 .1584 1.04			
					1619.	8	7.944 2.6	1.417	S 16	15.92 2.85 1461 1.55	3.6337	Se 34	39.21 2.25 .158 1.33	6.2739	Te 52 (63.36 2.23 .1517 1.28	11.71	Po 84	104.3 1.5 .1691 .98	9.0608	Ta 69	83.86 2.42 .1586 1.29			
					.5312	N 1	6.956 4.92 .1215 2.06	1.3068	٩ 15	15.38 3.43 .1334 1.7	3.4996	As 33	37.2 2.96 .1596 1.53	6.120B	Sb 51	60.43 2.75 .1498 1.43	11.528	B1 83	103.7 2.18 .1559 1.18	8, 8897	Er 68	83.02 3.29 .1474 1.5			
					.4467	c 6	5.963 7.37	1.2034	S1 14	13.94 4.63 .1388 1.98	3.3649	Ge 32	36.04 3.85 .1474 1.75	5.9666	Sn 50	58.89 3.14 .1511 1.53	11.346	Pb 82	102.8 2.03 .167 14	8.7197	Ho 67	81.88 3.14 .148 1.47			
					.3612	ю 44	5.367 5.77	1.0972	A1 13	13.4 3.39 .1568 1.7	3.2321	Ga 31	34.62 2.81 .167 1.5	5.8139	In 49	57 2.52 .1614 1.37	11.166	18 11	101.4 1.88 .1735 1.1	8.5506	Dy 66	80.69 3.04 .148 1.45			
				_							3.1028	Zn 30	32.46 1.35 .2194 1.04	5.661	Cd 48	55.81 1.16 .2083 .93	10.987	Hg B0	99.55 .67 .2362 .66	8.3831	Tb 45	78.9 4.05 .1378 1.68			
											2.9714	Cr 29	31.55 3.49 .1873 1.68	5.5112	Ag 47	53.53 2.95 .1789 1.49	10,808	Au 79	97.77 3.81 .1732 1.58	6.2151	Gd 64	78.05 4.14 .1354 1.7			
											2.8459	N1 28	29.15 4.44 .1825 1.9	5.3595	Pd 46	52.83 3.89 .1744 1.72	10.63	Pt 76	96.82 5.84 .161 1.96	B. 0505	Eu 63	75.42 1.86 .1654 1.15			
							gy tev) Souttering				2.7141	Ca 27	29.26 4.39 .1798 1.89	5.2107	Rh 45	51.09 5.75 .1622 2.09	10.452	Ir 77	95.43 6.94 .1579 2.14	7.8842	5a 62	74.63 2.14			
2			1000		radanin ria	limit of Family	umation cheri or Light-Ion (2.5889	Fe 26	27.73 4.28 .177 1.87	5.0615	Ru 44	50.15 6.74	10.275	0s 76	94.44 8.17 .152 2.33	7.7213	Pm 61	0 0 0			
UTERING TICL			~_EL/.		22	4	5 A				2.4618	Mn 25	27.27 2.92 .1904 1.54	4.9136	Tc 43	49.11 6.85 .1525 2.29	10.1	Re 75	92.45 8.03 .1496 2.32	7.5561	Nd 60	71.6 3.4 .1386 1.56	13.187	n 92	118.2 5.35 .148 1.84
Liuni-lux ar 1 2.014					. 28		4.475				2.3394	Cr 24	25.82 4.1	4.7676	Ma 42	47.64 6.82 .1483 2.29	9.9245	ы 74	91.26 8.9 .1427 2.44	7.3936	5 2	69.96 3.7 .1233 1.63	13.001	Pa 91	114.7 0
JLED MBERD					nd much	IM/CM/ UITED	for 1 keV Ion				2,2155	۲ ۲	25.29 5.31	4.6228	Nb 41	46.13 7.57 .1368 2.42	9.7501	Te 73	89.82 8.1 .1394 2.34	7.2301	8 2 2	69.56 4.32 .1296 1.76	12.813	14 90	115.2 0.2
PROJECT Z - NU MASS-N						N STATE					2.0965	13	23.78 4.85 .1468 2	4.4777	2r 40	45.29 6.25 .1319 2.2	9.5763	HF 72	88.58 6.44 .137 2.09		/	/		/	
				F							1.9791	Sc 21	22.32 3.9 .1781 1.8	4.3344	۲ ۲	44.15 4.37 .1278 1.84	7.0678	La 57	68.97 4.47 .1246 1.79	12.628	Ac 89	112.7 4.25			
0					.2822	Be 4	4.475 3.32	6266.	Mg 12	12.07 1.51	1.8677	Ca 20	19.9 1.84 .1403 1.24	4.1912	5 2	43.51 1.72 .135 1.16	6.9067	Ba 56	48.17 1.9 .1278 1.17	12.442	Ra 88	112.2 1.46			
	. 1303	н 1	۰0 ٥٥		, 2088	מ ב	3.446 1.63 .1401 1.19	.8967	Na 11	11.42 1.11	1.75	K 19	19.41 .93 .1368 .88	4.05	Rb 37	42.44 .85 .1357 .81	6.74 Bb	5e 53	65.99 .8 .131 .76	12.257	Fr 87	110.7 0 0 0			
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6 PARAMETERS FOR ANGULAR DEPENDENCE OF L PROJECTILED

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	.1734	He 2	1.327 0 0 0		. 8392	Ne 10	4 6.691 .02 5 .5636 .13		43 1.6692	7 Ar 18	4 13.24 .08 09 .3443 .26	38 3.9551	5 . 1 1 36	22 27.79 .12	31 6.6389	3 Xe 54	11 43.53 .16 3 .273 .35	51 12.127	5 Rn 86	73.61 .2 .2347 .38	.	11 n1 0	5 57.99 4.43 39 .1519 1.82				
					. 139	۰ د	6.3 .8 .2377 .8		1.56	8	.11.75 1.	3,81	ы В	26.5 1.	¢.48	6 -	42.08 1.	11.9	At 8	69.63 0 0 0		4X	57.36 1.6				
					. 4535	8 0	5.305 2.6		1.4587	s 16	10.63 2.85	3.6787	Se 34	26.18 2.25 .1748 1.36	6.3224	Te 52	42.31 2.23	11.766	Po 84	69.63 1.5 .1871 1.04		7011.7 7011.7	56 2.42 .1754 1.35				
					. 5044	r z	4.645 4.92 .1344 2.07		1.3465	۹ 15	10.27 3.43 .1476 1.72	3.5452	As 33	24.84 2.96 .1765 1.56	4.1704	10 95	40.35 2.75	11.502	B1 83	69.26 2.18 .1725 1.25		Er 68	55.44 3.29 .1631 1.57				
					.4786	9 U	3.982 7.37 .1631 2.54		1.2435	Sı 14	9.31 4.63 .1535 2	3.4101	Ge 32	24.07 3.85 .1631 1.78	6.0161	οğ B	39.32 3.14 .1672 1.57	11.401	Pb 87	68.67 2.03 .1648 1.21	CLF C	Ho 67	54.68 3.14 .1637 1.54				
					. 3894	נ ו מ	3.584 5.77 .1738 2.25		1.1351	A1 13	8.946 3.39 .1734 1.71	3.2773	Ga 31	23.12 2.81 .1848 1.52	5.8638	In 49	38.06 2.52 .1786 1.41	11.22	18 11	67.74 1.88 .1919 1.17		DY 66	53.88 3.04 .1637 1.51				
				-								3.1489	20 52	21.68 1.35 .2428 1.06	5.7106	Cd 48	37.27 1.16 ,2304 .96	11.041	Hg 80	66.48 .67 .2613 .7		Tb 65	52.69 4.05 .1524 1.75				
												3.0168	۶ ت.	21.0, 7 49	5.5615	Ag 47	35.74 2.95 .1979 1.53	10.863	Au 79	65.29 3.81 .1916 1.67	0776 0	6d 64	52.12 4.14 .1498 1.77				
												2,8929	N1 28	19.47 4.44 .2019 1.93	5.409	Pd 46	35.28 3.89	10.684	Pt 78	64.66 5.84 .1781 2.06	arot a	Eu 63	50.36 1.86 .1829 1.19				
							y (Ev) Suttering					2.7588	Co 27	19.54 4.39 .1989 1.92	5.2605	Rh 45	34.12 5.75	10.506	Ir 7	63.73 6.94 .1747 2.25		59 52 57 52	49.83 2.14 .174 1.28				
			00		and and a		imation Energ					2.6338	Fe 2b	18.52 4.28 .1958 1.89	5.1108	Ru 44	33.49 6.74 .1719 2.32	10.329	0s 76	63.06 8.17 .1681 2.45		19 m4	48.08 0 0 0				
TTERING VIELD			L/10	,	*			5	•			2,5051	E S	18.21 2.92 .2106 1.56	4.9624	Tc 43	32.8 6.85 .1687 2.35	10.154	Re 75	61.74 8.03 .1655 2.43		Nd 60	47.81 3.4 .1534 1.62		13.242	U 92	78.91 5.55
LIGHT-ION SPU .016					.307		2.998 3					2.3028	۲ ۲	17.24 4.1 .195 1.86	4.8164	Mo 42	31.81 6.82 .164 .2.34	9.978	M 74	60.94 8.9 .1579 2.56		Pr 59	46.72 3.7 .1497 1.69		12.027	Pa 91	76.59 0
EPENDENCE OF LE						TOOWAG	Ratio (M2/M1). or 1 bev Too.					2,2574	د د	16.89 5.31 .172 2.11	4.6716	ND 41	30.81 7.57 .1513 2.47	9.8035	Ta 73	59.98 8.1 .1542 2.45		Ce 58	46.45 4.32 .1434 1.83		12.868	Th 90	76.92 6.2
FICR ANGULAR DI PROJECTI Z - NUM PROJECTI						:	Nass A r					2.1386	11 22	15.88 4.85 .1624 2.02	4.5258	Zr 40	30.25 6.25	9.6295	HF 72	59.15 6.44 .1515 2.19	$\left[\right]$	/	/	\int	/	/	7
PARAMETERS F												2.0213	Sc 21	14.9 3.5 .1527 1.85	4.3822	۲ 39	29.48 4.37 .1414 1.88	7.1181	2	46.05 4.47 .1378 1.86		Ac 89	75.27 4.25				
TABLE 7					.3079	Be 4	2.988 3.32 .1891 1.71		1.0359	Mg 12	8.057 1.51	1.9122	Ca 20	13.29 1.84	4.238	ы Вх З	29.05 1.72 .1493 1.1B	6.9564	Ba 56	45.52 1.9 .1414 1.21		Ra 88	74.43 1.66 .1436 1.08				
	3221.	 H	.334 0		.2321	n I	2.301 1.63		. 9326	Na 11	7.62611	1.7926	K 19	12.96 .93	4.0964	49 12	28.34 .85 .1501 .83	6.7987	5	44.06 .8 .145 .79		Fr 87	73.94 0 0 0				

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	.438	H 2	~ 0		1.83	Ne 1	5.042 .0	.8346 .1	40 °P	Ar 1	9.98 .0 .5.32 .2	B. 19	n Z	20.94 .1	13.6	n X	32.8 .1	- 24.7	R B	55.46 .2	19.2	רי רי	43.7 4. -2288 1.			
					1.629	с Ц	4.747 .84	.3515 .86	3, 3303	CI 17	8.857 1.4 .2781 1.1	7.9201	Р 35	19.76 1.22 .2912 1.01	13.316	1	31.7 1.11 .2802 .95	24.356	At 85	52.47 0 . 0 0 0	18-775	Yb 70	43.22 1.6 .2638 1.12			
					1.4533	æ 0	3.997 2.6	.2526 1.51	3.117	5 16	8.01 2.85 .2406 1.57	7.6338	Se 34	19.73 2.25 .2621 1.37	12.988	Te 52	31.68 2.25	23.982	Po 84	52.47 1.5 .2819 1.07	18-432	Ta 69	42.2 2.42 .2641 1.37			
					1.2673	r z	3.5 4.92	.1981 2.07	2.8939	P 15	7.737 3.43	7.3647	As 33	18.72 2.96 .2646 1.57	12.684	Sb 51	30.41 2.75 .249 1.49	23.612	B1 B3	52.19 2.18 .2599 1.29	19.785	Er 68	41.77 3.29 .2455 1.6			
					1.0874	ہ د	3.001 7.37	.2397 2.54	2.6743	51 14	7.015 4.63	7.0899	Ge 32	18.14 3.85 .2444 1.8	12.372	Sr S	29.63 3.14	23.244	Pb 82	51,74 2.03 .2784 1.24	17.941	Ho 67	41.2 3.14 .2464 1.57			
					.8946	ю 8	2.701 5.77	.2548 2.25	2.4482	A1 13	6.741 3.39 .2576 1.71	6.820b	Ga 31	17.42 2.81 .2768 1.54	12.065	In 49	28.68 2.52 .2684 1.43	22.88	11 81	51.04 1.88 .2891 1.2	17 500	Dy 66	40.6 3.04 .2464 1.54			
				•					<u> </u>			4.5425	Zn 30	16.33 1.35	11.755	Cd 48	28.08 1.16 .3462 .97	22.52	68 FH	50.09 .67	17 241	Tb 45	39.7 4.05 .2294 1.79			
												6.2929	Cri 29	15.88 3.49 .3103 1.72	11.455	Ag 47	26.93 2.95 .2974 1.55	22.161	Au 79	49.19 3.81 .2887 1.71	14 07	Gd 64	39.27 4.14 .2254 1.81			
												6.044B	N1 28	14.67 4.44 .3023 1.94	11,145	Pd 46	26.58 3.89 .2898 1.78	21.799	Pt 78	48.72 5.84 .2684 2.12	102 11	Eu 63	37.95 1.86 .2753 1.21			
							37 (eV)	Sputtering				5.7677	Co 27	14.72 4.39	10.845	Rh 45	25.71 5.75 .2695 2.17	21.441	Ir 77	49,02 6.94 .2632 2.31	14 255	Sm 62	37.55 2.14 .2618 1.3			
<u>,</u>			1000			nic Number	limation Energ	ar Light-Ion S				5.5144	Fe 26	13.95 4.28	10.541	Ru 44	25.23 6.74	21.082	0s 74	47.52 8.17 .2532 2.51	15 020	Pm 61	34.23 0 0 .0			
JTTERING VIELI			(/ ^T a/		×	A Atom	5.32 5ubl					5.2499	۲ ۲	13.72 2.92 .3149 1.58	10.24	Tc 43	24.71 6.85	20.73	Re 75	46.52 8.03 .2493 2.49	18 501	Nd 60	36.03 3.4 .2308 1.64	26.054	U 92	59.46 5.55 .2459 2.03
LIGHT-ION SPL 2 1.0026					512.		2.252 3	. 2761				5.0016	Cr 24	12.99 4.1	9.9448	Mo 42	23.97 6.82 .2463 2.37	20.375	ы 74	45.92 8.9 .2378 2.62	140 21	Pr 39	35.2 3.7 .2252 1.72	26.585	Fa 91	57.71 0
JEPENDENCE OF ILE					i	Symbol	Ratio (M2/M1)	tor 1 keV Ion				4.7436	v 23	12.73 5.31	9.652	ND 41	23.21 7.57 .2271 2.5	20.023	Ta 73	45.2 8.1 .2322 2.5	10 11	5 28 28	35 4.32 .2157 1.86	26.201	7h 90	57.96 6.2
FOR ANGULAR I PROJECTI Z - NUR MASS-NU							Mass	e E				4.5023	11 22	11.97 4.85 .2426 2.04	9.3556	2r 40	22.79 6.25 .219 2.27	19.672	Hf 72	44.57 6.44 .2282 2.24					/	7
PARAME'.cRS				_								4.2642	Sc 21	11.23 3 9 .228 1.83	9.0642	۲ 39	22.21 4.37	14.599	La 57	34.7 4.47 .2073 1.89	X at	Ac 89	56.71 4.25 .2167 1.78			
TABLE 8					.7197	Be 4	2.252 3.32	.2761 1.71	2.2455	Mg 12	6.071 1.51 .2813 1.15	4.0468	Ca 20	10.01 1.84	B.7704	Sr 38	21.89 1.72	14.271	Ba S6	34.3 1.9	75. 453	Ra 88	56.46 1.66 .2165 1.11			
	.4915	 +	.252 0		.5568	L1 3	1.734 1.63	. 2252 1.2	2.0293	Na 11	5.746 1.11 .25 .9B	3.7997	k 19	9.766 .93 .2257 .89	8.4827	Rb 37	21.35 .85 .2251 .84	13.954	Cs 33	33.2 .8 .218 .8	100.20	Fr 87	55.71 0 0 0			



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	•	ê 13	.333 0		.115	Ne 10	1.68 .02 .0675 1.69		. 383	Ar 18	3.326 .08 '.0534 1.43	. 665	kr 36	-6.978 .12 .0492 1.05		1.102	Xe 54	10.93 .16		1.936	Rn 86	18.48 .2 .0349 .21		20.4	Lu 71	14.56 4.43 .0593 .5				
					5.003	٥ ٤	1.582 .84 .0768 1.71		é. 755	C1 17	2.952 1.4 .0613 1.48	6.641	Rr 33	6.654 1.22 .0582 1.07		7.503	1 53	10.57 1.11		•	At 85	17.49 0 0 .28		13.00	Yb 70	14.4 1.6 .0503 .51				
					17.33	8 0	1.332 2.6		13.95	S 16	2.669 2.85 .0639 1.53	12.19	Se 34	6.575 2.25 .0632 1.08		15.12	Te 52	10.62 2.23 .0564 .78		13.96	Po 84	17.49 1.5 .0525 .28		19.44	Tm 69	14.06 2.42 .0588 .53				
	•				36.38	2 2	1.167 4.92 .0627 1.79		16.9	Р 5	2.579 3.43	15.75	As 33	6.238 2.96 .0709 1.11		18.17	Sb 51	10.13 2.75 .0594 .82		20.21	B1 83	17.39 2.18 .0537 .29		20.25	۳ 8	13.92 3.29				
					62.62	د د	1 7.37 .0978 1.81		23.34	S1 14	2.338 4.63	20.27	Ge 32	6.044 3.85 .0697 1.12		20.46	Sn 50	9.875 3.14 .0633 .84		18.71	Pb 82	17.24 2.03 .0582 .3		×8.42	Ho 67	13.73 3.14 .0589 .56				
					50.26	ก ค	.9 5.77 .1013 1.83		17.29	A1 13	2.246 3.39 .0783 1.59	14.61	Ga 31	5.805 2.81 .0748 1.14		16.14	In 49	9.559 2.52 .06+3 .86		17.16	T1 81	17.01 1.88 .06 .32		79-67	Dy 66	13.53 3.04 .0584 .57				
								_				4.891	0£ 12	5.444 1.35 .085 1.19		7.347	Cd 48	9.359 1.16 .0707 .88		6.037	Hg 80	16.69.67 .0647.34		72.10	TE 65	13.23 4.05 .0585 .59				
												17.68	Cu 29	5.291 3.49 .0964 1.21		18.3	Ag 47	8.976 2.95 .0796 .9	*	¢.12	Au 79	16.39 3.81 .078 .36		1.10	Gd 64	13.09 4.14 .0577 .6				
												22.08	N1 28	4.888 4.44 .1003 1.25		23.97	Pd 46	8.859 3.89 .0855 .91		51.62	Pt 78	16.24 5.84 .0824 .38		11-01	Eu 63	12.65 1.86 .0575 .64				
				(eV)			14 (max)					21.85	Co 27	4.907 4.39		34.86	Rh 45	8.568 5.75 .0888 .93		40.74	Ir 77	16 6.94 .0855 .39		14.61	Sm 62	12.51 2.14				
				ishold Energy	in Number		Jmation Energ	+ pun				21.08	Fe 26	4.65 4.28 .0963 1.28		40.5	Ru 44	8.41 6.74 .0889 .95		12	0s 76	15.84 8.17 .0861 .4		5	Pm 61	12.07 0 0 .48				
JTTERING VIELD				Thre	59 × 61 20		1.85 1.85					14.34	Mn 25	4.574 2.92 .0944 1.29		40.76	Tc 43	8.236 6.85 .0873 .96		68.79	. Re 75	15.5 8.03 .0836 .43		24. /4	09 PN	12.01 3.4 .0557 .68		10.40	U 92	19.82 5.55 .0698 .11
HEAVY-IDN SPL					30.5		22:					19.95	54 C	4.33 4.1 .0955 1.31		40.02	Mo 42	7.988 6.82 .0837 .98		75.58	м 74	15.3 8.9 .0812 .44		90.97	Pr 59	.0555 .7		•	16 e d	19.23 0
SEPENDENCE OF TREE					o terio	nomye	HALIO (HZ/HI	for 1 e				25.77	23	4.241 5.31 .0884 1.31		43.79	ND 41	7.736 7.57		68.06	Ta 73	15.06 B.1 .0758 .46		20.41	28 0	11.67 4.32		61.97	Th 90	19.32 6.2
FOR ANGULAR I PROJECTI Z - NUP MA23-N						3	59 19 19					23.38	11 22	3.988 4.85 .0783 1.34	, .	35.87	Zr 40	7.595 6.25		53.61	HF 72	14.85 6.44 .0679 .48	ľ	/	/	/	V	/	/	
PARAMETERS								_				18.71	Sc 21	3.743 3.9 .0658 1.36		24.81	4 39	7.403 4.37		31.82	La 57	11.57 4.47 .0534 .72		18.14	Ac 89	18.9 4.25 .052 .18			•	
TABLE 9					30.59	Be 4	.75 3.32		7.984	Mg 12	2.023 1.51	8.811	Ca 20	3.337 1.84 .0498 1.43		9.706	Sr 38	7.296 1.72		13.43	Ba 56	11.43 1.9		10.28	Ra 88	18.82 1.66 .0367 .19				
	•	 1	.084 0 .0421 1.7		16.76	L1 3	.578 1.63 .054 1.85		6.002	Na 11	1.915 1.11 .0502 1.64	4.457	K 19	3.255 .93 .0378 1.44		4.749	89 37	7.117 .85 .0344 1.04		5.35	22 23	11.07 .8 .0303 .75		5	Fr 87	18.57 0 0 .21				

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	¢	н Н Щ	.198 0 .0377 1.8	-17	Ne 10	1 .02 .0745 1.81	.427	Ar 18	1.97° .08 .061 1.63		185.	kr . 36	4.153 .12 .058 1.32	.864	Xe 54	6.506 .16 .0517 1.09		1.383	Rn 86	11 .2 .0425 .76	27.01	Lu 71	8.667 4.43 .0718 .93					
			-	7.234	о ц	.942 .84 .0943 1.82	7.879	CI 17	1.757 1.4 .0697 1.68		5. <i>8</i> /7	Br 35	3.96 1.22 .0686 1.34	5.922	1 23	6.288 1.11 .0601 1.1		0	At 85	10.41 0 0B	9.703	Yb 70	8.573 1.6 .0609 .93					
				23.51	8 0	.793 2.6 .0769 1.84	16.93	S 16	1.589 2.85 .0725 1.71	•	10.83	Se 34	3.913 2.25 .0744 1.35	11.92	Te 52	6.323 2.23 .0675 1.1		10.05	Po 84	10.41 1.5 .0639 .8	14.51	Tm 69	8.37 2.42 .0712 .35					
				46.48	r z	.694 4.92 .0679 1.85	20.8	P 15	1.535 3.43 .0688 1.72		14.2	As 33	3.713 2.96 .0833 1.37	14.47	Sb 51	6.031 2.75 .0711 1.12		14.57	B1 83	10.35 2.18 .0654 .8	19.63	Er 68	8.285 3.29 .0719 .96					
				74.75	ہ ت	.105 1.85	29.92	S1 14	1.391 4.63 .0809 1.75		18.44	Ge 32	3.597 3.85	16.39	20 20	5.877 3.14		13.5	Pb 82	10.26 2.03 .0708 .81	18.62	Ho 67	8.171 3.14 .0712 .96					
				61.66	រ ភ្	.536 5.77	22.54	A1 13	1.337 3.39 .0878 1.76		13.45	6a 31	3.455 2.81	13.02	In 49	5.689 2.52		12.41	11 81	10.12 1.88	17.9	Dy 66	8.053 3.04 .0706 .97					
											6.47	Zn 30	3.24 1.35	5.958	Cd 48	5.57 1.16 .0845 1.18		4.579	68 Bi	9.94 .67 .0787 .83	23.61	Tb 65	7.874 4.05					
											16.75	5 Cr	3.149 3.49	14.98	Ag 47	5.342 2.95		24.65	Au 79	9.757 3.81	24.02	Gd 64	7.79 4.14					
											21.46	N1 28	2.909 4.44	19.69	Pd 46	5.273 3.89		19.75	Pt 78	9.463 5.84 .1001 .85	10.63	Eu 63	7.527 1.86					
				(eV)	uter .	17 (EV)					21.21	Co 27	2.92 4.39	28.87	Rh 45	5.099 5.75		44.30	Ir 77	9.524 6.94 .1039 .86	12.18	Sm 62	7.448 2.14					
				shold Energy	ite Number	und f					20.82	Fe 26	2.768 4.28	33.69	Ru 44	5.005 6.74 .1058 1.24		44.10	05 76	9.425 B.17 .1046 .87	0	Pm 61	7.185 0 0 1.04			•		
ITTERING YIELD						1.84					14.24	Mn 25	2.722 2.92	34.09	Tc 43	4.901 6.85 .1038 1.25		n. 0	Re 75	9.227 8.03 .1015 .89	19.03	09 PN	7.146 3.4	10 01			11.79 5.33	
HEAVY~ION SPL				29.1	4 4	1447					20.2	Cr 24	2.577 4.1	33.72	Mo 42	4.754 6.82 .0994 1.27		9.00 0	M 74	9.108 8.9 .0985 .9	20.51	Pr 53	6.982 3.7 .0668 1.05	c	, eq		11.45 0	
DEPENDENCE OF ILE1					Symbol	Ratio (MZ/MI) for 1 m					26.27	v 23	2.524 5.31	37.21	Nb 41	4.604 7.57		20.2	Ta 73	8.944 8.1 .0919 .91	23.9	28 5	6.943 4.32 .0668 1.05	41 08	2 2 2 2		11.5 6.2	
FOR ANGULAR I PROJECT) Z - KUP MASS-NI					:	Rass					24.35	11 22	2.374 4.85 .0903 1.57	30.62	Zr 40	4.52 6.25 .0812 1.29		39.64	Hf 72	8.84 6.44 .0823 .91		/			/	/	/	
PARAMETERS							_				19.94	Sc 21	2.227 3.9	21.32	4 7	4.406 4.37		24.65	La 57	6.883 4.47 .3642 1.06	29.77	Ac 89	11.25 4.25					
тавсе 10	-			39.3	Be 4	.447 3.32	10.88	Mg 12	1.204 1.51		9.8	50 Ca	1.986 1.84	8.375	rs B	4.342 1.72		10.43	Ba 56	6.804 1.9 .0486 1.06	11.6	R. 88	11.2 1.66 .0448 .74					
	0	- I	.05 0	22.92	2 1	.344 1.63	8.37	Na 11	1.14 1.11 .0557 1.79		5.004	K 19	1.937 .93	4.125	Rb 37	4.235 .85		4.339	22 22	6.586 .8 .0364 1.08	٥	Fr 87	11.05 0 0 .75					

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	•	ie N	10 76 1.76	. 185		5 2	a . U2 76 1.85		.496	۲ 18	15 1.73	.576	r 36	36 .12 36 1.46	. 795	Xe 54	67 .16 53 1.26		41-1	88 98	18 . 28 18 . 96	23.89	12 m	33 4.43 37 1.09				
			₹ <u>10</u>	2			B4 74		<u>ي</u>	17	76 .06	8		-22 3.1. -48 .06	78	8	.27 .05	-		8	99 B.2	74	1 20	.6 6.4 .09 .071				
				2.9		u.	. 704 .6 .0875 1.			5	1.314 1.	5.8	ä	2.962 1.074 1	4	H	4.703 1.		•	đ	7.784 0	8.5	ę	6.412 1 .0668 1				
				26.41		8	.593 2.6 .0796 1.85		20.75	S 16	1.188 2.85 .0764 1.78	10.87	Se 34	2.927 2.25 .0802 1.48	11.02	Te 52	4.729 2.23		R. 701	Po 84	7.784 1.5	12.89	Tm 69	6.26 2.42 .078 1.1				
				53.44		r z	.519 4.92 .0699 1.85		25.71	4 15	1.148 3.43	14.39	As 33	2.777 2.96	13.47	Sb 31	4.511 2.75 .0773 1.29		12.62	B1 83	7.743 2.18 .0719 .99	17.47	Er 68	6.197 3.29 .0787 1.11				
				R7.41		ຈ ບ	.445 7.37		37.87	S1 14	1.041 4.63 .0851 1.8	18.82	Ge 32	2.691 3.85 .088 1.52	15.32	Sn 50	4.396 3.14 .0824 1.3	4		ЪР В3	7.676 2.03 .0778 1	16.59	Ho 67	6.112 3.14 .078 1.11				
				73.11		ю а	.401 5.77		28.8	A1 13	1 3.39 .092 1.81	13.84	Ga 31	2.584 2.81 .0942 1.54	12.24	In 49	4.255 2.52		10.78	18 11	7.572 1.88 .0802 1.01	15.99	Dy 66	6.023 3.04 .0772 1.12				
												6.743	Zn 30	2.423 1.35	5.617	Cd 48	4.166 1.16		3.61	68 БН	7.431 .67 .0864 1.02	21.15	Tb 65	5.89 4.05 .0772 1.13				
												17.36	Cu 29	2.355 3.49	14.22	Ag 47	3.996 2.95		C.12	Au 79	7.298 3.81	21.55	Gd 64	5.827 4.14 .0761 1.14				
												22.87	N1 28	2.176 4.44 .1254 1.6	18.73	Pd 46	3.944 3.89		32.83	Pt 78	7.228 5.84	9.583	Eu 63	5.63 1.86				
				(eV)		(08)						22.59	Co 27	2.104 4.39 .1242 1.6	27.62	Rh 45	3.814 5.75 .1147 1.36		к. яс	Ir 7	7.124 6.94	10.99	Sm 62	5.571 2.14 .0743 1.18				
				shold Energy	ac Number	testion Foero						22.44	Fe 26	2.07 4.28 .1197 1.62	32.34	Ru 44	3.744 6.74 .1146 1.36		4.04	0\$ 76	7.05 8.17	•	Pm 61	5.374 0 0 1.2				
ITTERING VIELD				Three	Atom		R I		•			15.4	Чл 23 Чл	2.036 2.92	32.83	Tc 43	3.666 6.85 .1124 1.37		44.32	Re 75	6.901 8.03 .1113 1.06	17.27	09 PN	5.345 3.4	1. 15		n 92	8.821 5.55 .0938 .92
HEAVY-ION SPL 13 26.98					7	*	- 124 - 10001					22.11	Cr 24	1.927 4.1 .118 1.64	32.66	Mo 42	3.556 6.82		46,63	ы 74	6.812 8.9 .108 1.06	18.68	Pr 59	5.222 3.7	c	,	Pa 91	8.562 0 .0854 .93
DEPENDENCE OF ILE					Symbol	Ratio (M2/MI		i				28.89	<pre></pre>	1.688 5.31	36.24	Nb 41	3.444 7.57		44.22	Ta 73	6.705 B.1 .1007 1.07	21.78	28 Ce	5.193 4.32	17.45		1h 90	8.599 6.2 .0745 .93
FOR ANGULAR I PROJECT I Z - NUR MASS-NU						And	-					27.15	T1 22	1.775 4.85	29.92	Zr 40	3.381 6.25 .0878 1.42		94°46	HF 72	6.612 6.44 .0902 1.08		/		V	/	/	/
PARAMETERS								_				22.56	Sc 21	1.666 3.9 .0804 1.69	20.93	۲ ۲	3.295 4.37		44.77	2	.07 1.23	25.54	Ac 89	8.414 4.25 .0699 .95				
тав се 11				47 10		Be 4	.334 3.32		13.15	Mg 12	.901 1.51 .0769 1.83	11.39	50 CP	1.486 1.84 .0607 1.73	B. 243	ις Β	3.248 1.72 .0565 1.44		+00.4	Ba 56	022 1.23 .053 1.23	9.956	R.a. 88	8.377 1.66 .0492 .95				
	•	- H	.037 0 .0408 1.7	27 86	20.02	2 1	.257 1.63		9.815	11 4	.0581 1.83	5.849	k 19	1.449 .93 .0458 1.74	4.078	Rb 37	3.168 .85	1 005	C 1	5	4.726 .8 .0397 1.25	•	Fr 87	8.265 0 0 .96				

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o	He 2 .1 0 .0373 1.7	.22 Ne 10 .505 .02	89.	Ar 18	1 .08 .0685 1.8	.626	Łr 36	2.098.12	.766	Xe 54	3.287 .16	1.027	Rn 86	5.558 .2	21.6	Lu 71	4.379 4.4 .0874 1.3				
-		9.58 F 9 .476 .84	12.24	CI 17	.888 1.4 .0781 1.83	6.479	Br 35	2.001 1.22	5.325	1 53	3.177 1.11	0	At BS	5.258 0	7.789	Yb 70	4.331 1.6 .0741 1.31				
		32.95 32.95 0 8 .401 2.6 .0821 1.83	25.67	S 16	.903 2.85 .0808 1.84	12.01	Se 34	1.977 2.25 .087 1.63	10.49	Te 52	3.195 2.23 .0809 1.45	7.587	Po 84	5.258 1.5	11.74	Tm 69	4.229 2.42 .0865 1.32				
		68.23 N 7 .351 4.92 .0718 1.82	31.25	е 51	.775 3.43 .0764 1.84	16.15	As 33	1.876 2.96	13.23	Sb 51	3.047 2.75 .0851 1.47	11.61	B1 83	5.23 2.1B .0802 1.22	15.94	Er 68	4.186 3.29 .0874 1.32				
		114.5 C 6 .301 7.37 .11 1.82	43.71	51 14	.703 4.43	21.31	Ge 32	.0954 1.66	15.14	Sn 50	2.969 3.14 .0906 1.48	10.23	Pb 82	5.185 2.03 .0868 1.22	15.19	Ho 67	4.129 3.14 .0865 1.33				
		97.33 B 5 .271 5.77 .1115 1.81	32.52	A1 13	.076 3.39	15.86	Ga 31	1.746 2.81 .102 1.68	12.2	In 49	2.874 2.52	9.445	T1 B1	5.115 1.88	14.68	Dy 66	4.069 3.04 .0856 1.33				
		L	J			7.885	Zn 30	1.637 1.35	5.63	Cd 48	2.814 1.16	3.352	Нд ВО	5.02 .67 .0964 1.24	19.52	Tb 65	3.978 4.05				
						20.72	Cu 29	1.591 3.49	14.41	Ag 47	2.699 2.95	18,98	Au 79	4.93 3.81 -1161 1.25	19.93	Gd 54	3.936 4.14 .0843 1.34				
						27.66	N1 28	1.47 4.44	19.04	Pd 46	2.664 3.89	29.04	Pt 78	4.882 5.84	8.932	Eu 63	3.803 1.86				
		(eV) Y (eV)				27.29	Co 27	1.475 4.39	28.33	Rh 4 5	2.576 5.75	34.4	Ir 77	4.812 6.94 .127 1.26	10.27	Sm 62	3.763 2.14 .0823 1.36				
		shold Energy ic Number imation Energ	t pun			27.57	Fe 26	1.398 4.28	33.34	Ru 44	2.529 6.74	40.41	03 76	4.762 8.17 .1278 1.27	0	Pm 61	3.63 0 0 1.37				
JTTERING VIELD		Three Three	sign			19.02	Mn 25	1.375 2.92	34.04	Tc 43	2.476 6.85	39.56	Re 75	4.662 B.03	16.29	09 PN	3.61 3.4 .081 1.38	29.09	u _92	5.959 5.55	
HEAVY-ION SPL		86 4				27.79	Cr 24	1.302 4.1	34.14	Mo 42	2.402 6.82	43.74	м 74	4.602 B.9	17.71	Pr 59	3.528 3.7 .0804 1.4	0	Pa 91	5.784 0	
DEFENDENCE OF MER		Symbo Ratio (M2/M1	for 1 e			36.56	v 23	1.275 5.31	38.22	Nb 41	2.326 7.57	39.7	Ta 73	4.529 8.1	20.68	C.e. 58	3.508 4.32	32.24	Th 90	5.809 6.2	
FOR ANGULAR PROJUCAR 2 - NEUT		r se r				35.05	11 22	1.199 4.85 .1028 1.78	31.72	2r 40	2.284 4.25	31.49	Hf 72	4.467 6.44 .1003 1.29						/	
PARAHETERS			_			29.73	Sc 21	1.125 3.9	22.35	42 7	2.226 4.37	21.4	La 57	3.478 4.47	21.96	Ac 89	5.684 4.25				
TABLE 12		65.17 8e 4 .226 3.32 .1017 1.81	15.16	Mg 12	.608 1.51	15.58	Ca 20	1.004 1.84 .047 1.81	8,838	Sr 38	2.194 1.72	9.095	Ba 56	3.438 1.9	8.565	Ra 88	5.658 1.66				
•	H 1 .025 0 .0399 1.7	40.5 L1 3 .174 1.63 .0562 1.78	11.44	Na 11	-576 1.18 20606 1.85	7.938	K 19	.979 .93 .0487 1.81	4.404	89 37	2.14 .85 .0478 1.61	3.831	Cs 55	3.327 .8 .0437 1.43	•	Fr 87	5.583 0 0 1.18				

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	5	He 2	.072 0 .0365 1.7		7/7.	Ne 10	.361 .02 .0831 1.82		. 75	Ar 18	.715 .08 .0723 1.85	014	,	hr 36	1.5 .12 .0739 1.72		.805	Xe 54	2.351 .16		. 964	Rn 85	3.975.2 .0585 1.34	21.27	Lu 73	3.132 4.43			
					14.11	с ц	.34 .84 .093 1.82		13.79	CI 17	.635 1.4 .0822 1.85	111 1	10.01	۳ ۲	1.431 1.22 .0872 1.74		5.642	1 53	2.272 1.11		0	At 85	3.76 0 0 1.36	7.688	Vb 70	3.098 1.6 .0825 1.46			
					41.93	8	.286 2.0 .0839 1.82		29.41	S 16	.574 2.85 .0849 1.85			Se 34	1.414 2.25 .0943 1.74		11.32	Te 52	2.285 2.23 .089 1.58		7.198	Po 84	3.76 1.5 .0878 1.36	11.65	Tm 69	3.024 2.42			
					68.3	rz	.251 4.92 .0731 1.81		36.01	P 15	.555 3.43 .08 1.85		14.03	As 33	1.341 2.96		14.16	Sb 51	2.179 2.75 .0936 1.6		10.46	B1 83	3.74 2.18 .0898 1.36	15.85	Er 68	2.994 3.29			
				1	150.9	ہ ں	.215 7.37 .1113 1.8		51.18	S1 14	.503 4.63 .0935 1.85		20•13	Ge 32	1.3 3.85		16.31	Sn 5v	2.124 3.14		9.735	Pb 82	3.708 2.03	15.15	Ho 67	2.953 3.14 .0961 1.48			
					129.8	n a	.194 5.77 .1121 1.8		38.32	41 13	.483 3.39 .1006 1.85		14.6/	Ga 31	1.248 2.81		13.25	In 49	2.056 2.52		4.01	18 11	3.658 1.88	14.69	Dy 66	2.91 3.04 .0951 1.48			
				L									9.953	Zn 30	1.171 1.35		6.146	Cd 48	2.013 1.16		3.209	Hg 80	3.59 .67 .1077 1.38	19.63	Tb 65	2.845 4.05			
													26.36	Cu 29	1.138 3.49 .1404 1.79		15.9	Ag 47	1.93 2.95 .1241 1.64		18.24	Au 79	3.526 3.81 .1297 1.4	20.09	Gd 64	2.815 4.14 .0935 1.5			
													35.98	N1 28	1.051 4.44 .1453 1.8		21.08	Pd 46	1.905 3.89		27.96	Pt 78	3.491 5.84 .1368 1.41	9.074	Eu 63	2.72 1.86			
				(eV)			14 (EV)						33.46	Co 27	1.055 4.39 .1435 1.8		31.63	Rh 4 1	1.842 5.75		33.22	Ir 77	3.441 6.94 .1418 1.41	10-46	Sm 62	2.691 2.14			
				ishold Energy	tic Number								36.37	Fe 26	1 4.28 .138 1.81		37.4	Ru 44	1.808 6.74 .1373 1.66		39.11	0s 76	3.406 8.17 .1426 1.42	c	Pm 61	2.596 0 0 1.54			
ITTERING YIELD				Thre	Si Aron		25.1	ufite					24.9	Mn 25	.984 2.92 .1344 1.81		38.4	Tc 43	1.771 6.85		38.45	Re 75	3.334 8.03 .1382 1.43	14.74	09 PN	2.582 3.4 .0897 1.54	26.95	U 92	4.261 5.55
HEAVY-ION SPL					88.5	-	19101.						35.41	Cr 24	.931 4.1 .1352 1.82		38.82	Mo 42	1.718 6.82 .1285 1.68		42.63	M 74	3.291 8.9 .134 1.43	18.31	Pr 59	2.523 3.7 .0891 1.55	•	Fa 91	4,136 0
JEPENDENCE OF ILE					5vmbol								46.09	<pre></pre>	.912 5.31 .1243 1.82		43.83	Nb 41	1.664 7.57		38,82	Ta 73	3.239 8.1 .1248 1.44	21.4	5e 58	2.509 4.32	30.01	Th 70	4.154 6.2
FOR ANGULAR I PROJECT 2 Z - NUR MASS-NU						M							42.81	11 22	.858 4.85 .1094 1.83		36.55	Zr 40	1.633 6.25		30.89	Hf 72	3.194 6.44 .1117 1.45	ľ	/		V	/	/
PARAMETERS													1.00	Sc 21	.805 3.9 .0912 1.84		25.93	5 5 7	1.592 4.37		22.19	La 57	2.487 4.47 .0853 1.55	20.52	Ac 89	4.064 4.25			
TABLE 13					88.51	Be 4	.161 3.32		18-16	Mc 12	.435 1.51 .0835 1.84		17.24	50 CP	.718 1.84 .0686 1.85		10.29	87 78	1.569 1 72		9.457	Ba 56	2.458 1.9 .0646 1.56	8.013	fa 88	4.047 1.66			
	•	 	.018 0 .0385 1.7		56.27	1	.124 1.63		13.62	Na 11	.412 1.11 .0628 1.83		C67.8	к 19	.7 .93 .0515 1.85		5.164	8 6	1.53 .85		4.014	ទួ	2.38 .8 .0483 1.57	0	Fr 87	3.993 0 0 1.34			

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	•	He 1	.063 0 .0363 1.7	.298	Ne IO	.318 .02 .0837 1.82	101			.806	kr .36	1.319 .12	. 839	2.066.16		.957	Rn 86	3.493 .2 .0604 1.41	21.57	Lu 71	2.752 4.43				
				13.1	с г	.299 .84 .0935 1.82	97 VI		.558 1.4 .0833 1.85	8.491	в Х	1.257 1.22	5.899	1.997 1.11		0	At 85	3.304 0 0 1.43	7 BUA	Vb 70	2.722 1.6 .0849 1.52				
				46.52	8	.252 2.6	71 45		. 504 2.85	15.81	Se 34	1.242 2.25	11.83	2.008 2.23	2	7.184	Po 84	3.304 1.5 .0906 1.43	1 84	Tm 69	2.658 2.42				
				98.55	r z	.22 4.92 .0733 1.8			487 3.43 0809 1.85	21.69	As 33	1.179 2.96	14.87 Ch 51	1.915 2.75		10.44	B1 83	3.287 2.18 .0926 1.43	14.14	Er 68	2.631 3.29				
				169.4	ہ ن	.189 7.37 .1115 1.8	41 14		.442 4.63	28.98	Ge 32	1.142 3.85	17.17 Gn 30	1.866 3.14		9.727	Pb 82	3.259 2.03	15.45	Ho 67	2.595 3.14				
				146.3	8 8	.17 5.77	41 4		.425 3.39	21.91	Ga 31	1.097 2.81	13.44 In 46	1.806 2.52		9.014	11 81	3.215 1.88 .1031 1.44	15	Dy 66	2.557 3.04 .0978 1.54				
										11.16	Zn 30	1.029 1.35	900.0 84 b)	1.769 1.16	-	3.215	Н9 ВО	3.155 .67	20.08	Tb 65	2.5 4.05				
										29.65	Cu 29	1 3.49	10. Y	1.696 2.95		18.31	Au 79	3.098 3.81	20.58	Gd 64	2.474 4.14 .0962 1.56				
										38.42	N1 28	.924 4.44 .148 1.82	Pd 46	1.674 3.89 .1362 1.69		28.08	Pt 78	3.068 5.84 .141 1.46	9.323	Eu 63	2.39 1.86				
				(1,2)	:					37.95	Co 27	.927 4.39 .:461 1.82	Rh 45	1.619 5.75		33.41	Ir 77	3.024 6.94 .1461 1.47	10.76	Sm 62	2.345 2.14				
				shold Energy	1c Number	imation there				37.52	Fe 2b	.879 4.28 .1404 1.83	 #0.03	1.589 6.74 .1406 1.71		39.37	0s 76	2.993 8.17 .1469 1.47	0	Pm 61	2.282 0				
ITERING YIELD				4 A	Atom	-76 -76				25.72	н 23	.864 2.92 .1367 1.83	 Tc 43	1.556 6.85		38.78	Re 75	2.93 B.03 .1424 1.48	17.29	09 PN	2.269 3.4	26.63	U 92	3.745 5.55	
HEAVY-ION SPU 19 3.55				100.	1	.142 3				36.7	Cr 24	.818 4.1 .1374 1.84	97.14 Ma 42	1.51 6.82 .1315 1.72		43.04	M 74	2.892 8.9 .138 1.49	18.95	Pr 59	2.217 3.7	0	Pa 91	3.635 0	
DEPENDENCE OF ILECu 10668					Symbol Symbol	19/20) 011EM	1			47.85	23	.802 5.31 .1263 1.84	 20-14 41	1.462 7.57	-	39.25	Ta 73	2.847 8.1 .1286 1.49	22.16	58 28	2.205 4.32 .0915 1.6	29.71	Th 90	3.651 6.2 .0965 1.37	
FOR ANGULAR I PROJECTJ Z - NUP MAS9-NL					3					44.62	11 23	.754 4.85	Zr 40	1.435 6.25		31.27	HF 23	2.807 6.44					/	/	F
PARANETERS								_		36.73	Sc 21	.707 3.9 .0925 1.85	 Y 39	1.399 4.37 .0891 1.74		52	La 57	2.186 4.47 .0877 1.6	20.35	Ac 89	3.572 4.25 .0904 1.38				
TABLE 15				100.4	Be 4	.142 3.32	19.73	C.	.382 1.51	18.17	Ca 20	.631 1.84 .0696 1.85	5. rs	1.379 1.72		9.812	Ba 56	2.161 1.9	7.949	Ra 88	3.556 1.66 .0637 1.38				
	•	 #	.016 0 .0381 1.7	64.3	LI J	.109 1.63	15.06	1	.362 1.11	9.289	K 19	.615 .93 .0522 1.85	 Rb 37	1.345 .85		4.178	5	2.091 .B	0	Fr 87	3.509 0 0 1.4				

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	0	He 2	.048 0 .0357 1.7	142.	Ne 10	.241 .02 .0844 1.91	116.	Ar 18	.477 .08 .0749 1.85	1.02	kr - 36	1 .12 .0785 1.81	.958	Xe 54	1.567 .16	86	Rn Bb	2.649.2 .064 1.53	23.15	Lu 71	2.087 4.43 .1059 1.62				
				10.42	ь г	-227 .84 0942 1.81	12.13	CI 17	.423 1.4 .085 1.83	10.48	Br 35	.954 1.22 .0925 1.82	6.787	1 53	1.514 1.11	c	At 85	2.506 0 0 1.55	8.296	Yb 70	2.064 1.6 .0897 1.62				
				59.21	8	.191 2.6 .0846 1.8	57.23	S 16	.383 2.85 .0876 1.83	19.37	Se 34	.942 2.25 .0999 1.82	13.59	Te 52	1.523 2.23 .0958 1.72	7 474	Po 84	2.506 1.5 .096 1.55	12.82	Tm 69	2.015 2.42 .1046 1.63				
				126.8	r Z	.167 4.92 .0734 1.78	45.87	Р 15	.37 3.43 .0824 1.82	25.83	As 33	.894 2.96 .1113 1.83	17.27	Sb 51	1.452 2.75	10 87	B1 83	2.493 2.18 .0981 1.55	17.49	Er 68	1.995 3.29				
				220.5	יז ט	.143 7.37	66.34	S1 14	.335 4.63 .096 1.82	33.89	Ge 32	.866 3.85 .1089 1.83	20.05	Sn 50	1.415 3.14 .107 1.74	10,05	Pb 82	2.471 2.03 .1062 1.56	16.79	Ho 67	1.968 3.14 .1043 1.63				
				191.8	ព	.129 5.77 .1117 1.76	50.02	AI 13	.322 5.39 .1031 1.82	25.03	Ga 31	.832 2.81 .1162 1.83	16.46	In 49	1.37 2.52 .1083 1.75	0 774	18 11	2.438 1.88 .1092 1.56	16.35	Dy 66	1.939 3.04				
										12.27	20 71	.78 1.35 .1312 1.84	7.693	Cd 48	1.341 1.16 .1186 1.75	1 167	68 ВН	2.393 .67 .1176 1.57	21.99	1b 65	1.896 4.05 .103 1.65				
										32.04	Cu 29	.758 3.49 .1479 1.85	20.18	Ag 47	1.286 2.55	<u>a</u>	Au 79	2.35 3.81 .1416 1.57	22.59	Gd 64	1.876 4.14				
										41.98	N1 28	.701 4.44	26.87	Pd 46	1.27 3.89 .1424 1.77	70. AR	Pt 78	2.327 5.84 .1492 1.58	10.31	Eu 63	1.813 1.86 .1007 1.66				
				(eV)		gy (cV)				41.44	Co 27	.703 4.39	40.77	Rh 45	1.228 5.75 .1474 1.78	81.85	lr 77	2.294 6.94 .1546 1.58	11.92	Sm 62	1.794 2.14 .0987 1.66				
a				eshold Energy	atc Number	limation Ener-				41.28	Fe 26	.666 4.28 .1448 1.65	48.51	Ru 44	1.205 6.74 .1469 1.78	41 54	0\$ 76	2.27 8.17 .1554 1.59	•	Pm 61	1.73 0 0 1.68				
UTTERING YIEL				The second secon	4 A A Ato	3.32 1.72				28.36	Hn 25	.1408 1.85	50.16	Tc 43	1.18 4.85	41.09	Re 75	2.222 6.03 .1505 1.59	19.34	09 PN	1.721 3.4 .097 1.68		26.9	U 92	2.84 5.55
HEAVY-ION SP 15 36 83.8				131	1	1008				40.79	Cr 24	.1415 1.85	51.23	Mo 42	1.145 6.82	45.73	н 74 И	2.193 8.9 .1459 1.6	21.3	Pr 59	1.681 3.7		•	Pa 91	2.757 0
DEPENDENCE OF TILE					Symbo	s Ratio (M2/M) for 1 e				53.33	v 23	.608 5.31 .1299 1.85	58.47	ND 41	1.109 7.57	41.84	Ta 73	2.159 8.1 .1358 1.6	24.94	Ce 28	1.672 4.32		30.16	Th 90	2.768 6.2
5 FOR ANGULAR PROJECT 2 - NI MASS-1						Ta				50.15	11 22	.572 4.85	49.07	Zr 40	1113 1.8	33.42	Hf 72	2.129 6.44		/	/	ľ	/	/	
PARAMETERS							r			41-64	Sc 21	.536 3.9	35.12	4 39	1.061 4.37 .0928 1.8	25.93	La 57	1.658 4.47	20.75	Ac 89	2.709 4.25				
TABLE 16				133.1	Be 4	.108 3.32 27.1 4001.	24.12	Mg 12	.27 1.51	20.92	50 C#	.478 1.84 .0713 1.85	14.01	85 73	1.046 1.72 .0713 1.8	11.09	Ba 55	1.638 1.9	8.109	Ra 88	2.697 1.66				
	0	- +	.012 0	86.45	ч С	.083 1.63 .0548 1.7	18.52	Na 21	.274 1.11	10.73	K 19	.446 .93 .0535 1.85	7.087	89 27	1.02 .85 .0552 1.81	4.758	5	1.586 .8 .052 1.71	•	Fr 87	2.661 0 0 1.53				

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	0	He 2	344 1.7		. 559	Ne 10	54 .02 849 1.77		1.232	Ar 18	04 .08 771 1.82	1.179	kr 36	38 .12 832 1.85	1.359	Xe 54	.16 795 1.81	1.148	Rn Bs	691 .2 706 1.69		29.53	;	332 4.43 157 1.76				
L			<u></u>]	24.9	с ц	15 .84 .1		23.66	CI 17	73 1.81 .0	12.25	Br 35	979 1.22 0	9.501	1 53	56 1.11 1 923 1.82 .0	•	At 85	599 0 1.71 1.0		10.75	2	18 1.6 1. 779 1.76 .1				
					91.58	80	22 2.6 .1' 345 1.76 .0'		52.31	S 16	14 2.85 .2 397 1.81 .00	22.71	Se 34	01 2.25 .6	19.06	Te S2	72 2.23 .9	8.877	Po 84	599 1.5 1.71 0	-	16.55		286 2.42 1.1				
					198.9	۲ z	07 4.92 .11 73 1.72 .01		64.82	P 15	36 3.43 .2	30.63	As 33	71 2.96 .6	23.77	Sb 51	27 2.75 .9	12.94	B1 B3	591 2.18 1.1 08 1.71 .1		22.68		273 3.29 1. 15 1.77 .1				
					1351	ہ د	0.1 7.37 .1	-	95.24	S1 14	214 4.63 .2	40.48	Ge 32	553 3,85 55 1149 1.85 .1	27.32	Sn 50	903 3.14 .9	12.11	Pb 82	577 2.03 1. 1167 1.71 .1		21.87) 2	.256 3.14 1. 1137 1.77 .1				
					308	ព	082 5.77 .0	-	72.25	A1 13	205 3.39 .2	30, 16	Ga 31	531 2.81 -:	22.12	In 49	874 2.57 .9	11.31	11 81	.556 1.88 1. 12 1.72 .1		21.42	00 60	.238 3.04 1. 1124 1.77 .1				
] [<u></u>]	ñ	2n 30	498 1.35 138 1.85	10.24	Cd 48	856 1.16 .0	4.076	Hg BO	.527 .67 1.1292 1.72			8	.21 4.05 1. 1121 1.78 .				
												39.41	Cu 29	484 3.49	26.38	Ag 47	.821 2.95	23.44	Au 79	1555 1.73		24.75	5	1.197 4.14 1 1103 1.78 .				
												52.52	N1 28	.447 4.44	34.93	Pd 46	.81 3.89	36.15	Pt 78	1.485 5.84		13.85		1.157 1.86				
												51.81	Co 27	.449 4.39	52.2	Riy 45	.784 5.75 .1578 1.84	43.36	Ir 77	1.464 6.94 .1696 1.73		10.08 5 42 1		1.145 2.14				
_				hold Frency (+ pur				52.2	Fe 2b	.425 4.28 .1513 1.84	61.57	Ru 44	.769 6.74	51.39	0s 76	1.449 B.17 .1703 1.74	-	0 8		1.104 0 0 1.79				
UI IEKING 71ELI							E:-	wbis/				35.99	н 23	.418 2.92	63.03	Tc 43	. 753 6.85	51.23	Re 75	1.418 8.03 .1649 1.74		26.48		1.098 3.4	30.76	U 92	1.813 5.55	
HEAVT-IUN 57 4 31.3					216.	T Be	1 4860.					52.35	с 24	.396 4.1 .1473 1.83	63.45	Mo 42	.731 6.82 .1465 1.85	57.28	ы 74	1.4 8.9 .1597 1.74		29.42 0	5	1.073 3.7 .1044 1.8	•	Pa 91	1.759 0	
DEPENDENCE UF						ronwice		for 1 e				68.73	۲ ۲	.135 1.83	71.29	Nb 41	.708 7.57	52.71	Ta 73	1.378 8.1		24-22 24-22		1.067 4.32 .1042 1.8	34.79	7h 90	1.767 6.2	
s FOR ANGULAR PROJECT: 7 - NUI MASS-NI							580U					65.44	T1 22	.365 4.85 .1184 1.82	59.28	2r 40	.695 6.25	42.32	Hf 72	1.359 6.44	ľ	/	/			/	/	·
PARAMETERS							_					55.03	Sc 21	.342 3.9	41.88	4 39	.677 4.37 .0988 1.85	36.02	La 57	1.058 4.47 .0997 1.8		24.11		1.729 4.25				
TABLE				_	216.8	Be 4	.069 3.32		35.38	Mg 12	.185 1.51 .0864 1.8	28.25	Ca 20	.305 1.84 .0737 1.82	16.58	Sr 38	.0757 1.85	15.47	Ba 56	1.046 1.9 .0754 1.8		9.439		1.721 1.66				
	0	H	.009 0 .0355 1.7		143.2	с 1	.053 1.63		27.38	Na 11	.175 1.11	14.56	K 19	.298 .93 .0551 1.82	8.281	Rb 37	.651 .85 .0585 1.85	6.719	C, 55	1.012 .8 .0562 1.81	,	0	19	1.698 0 0 1.69				

			٢.	١ſ		<u>0</u>	85	12	18	8 B		2	58.	ß	5 7	81 85	47	86	2 .79	١ſ	72	1	8.8			
	•	He	.02 0	10	:	#2 2	.0843 1.	1.7	Ą	.199 .	1-41	2	.418 .0866 1	1.5	a X	. 655	1.5	£	1.107 .		.	3	.124 1			
				10 51		с ц	.095 .84	34.23	CI 17	.177 1.4 .0882 1.78	15.51	Br 35	.399 1.22	10.95	1 23	.633 1.11 .0976 1.85	•	At 85	1.047 0 0 1.B		14.1	Yb 70	.863 1.6 .1049 1.83			
				1 2 2 1		9 0	.08 2.6 .0833 1.7	76.64	S 16	.16 2.85 .0904 1.77	28,83	Se 34	.394 2.25 .1096 1.83	21.94	Te 52	.636 2.23 .1091 1.85	12.2	Po 84	1.047 1.5 .1141 1.8		21.47	Ta 69	.1221 1.83			×
				0 712		r z	.07 4.92	95.37	٩ ت	.154 3.43	39.29	As 33	.374 2.96	27.64	29 29	.607 2.75	17.81	B1 83	1.042 2.18 .1165 1.8		29.28	Er 68	.834 3.29 .123 1.83			
				c 11		9 0	.05 7.37	141.7	S1 14	.14 4.63 .0981 1.76	52.22	Ge 32	.362 3.85 .119 1.82	31.94	50 50	.592 3.14	16.72	Pb 82	1.033 2.03 .1259 1.8		28.07	HD 67	.1215 1.84			
				7 200		n 0	.054 5.77	108	A1 13	.135 3.39 .1048 1.76	39.21	Ga 31	.348 2.81	26.04	In 49	573 2.52 .1227 1.85	15.69	18 11	1.019 1.88		27.3	Dy 66	.81 3.04 12 1.84			
											19.73	Zn 30	.326 1.35	12.11	Cd 4B	.561 1.16 .1342 1.85	3. 693	Hg BV	1 .67 .1392 1.81		36.63	Tb Cô	.793 4.05			
											52.09	Cu 29	.317 3.45	31.46	Ag 47	.538 2.95	32.5	Au 79	.982 3.81 .1673 :.81		37.58	6d 64	.784 4.14 .1176 1.84			
											70.39	N1 28	.293 4.44 .1651 1.82	41.77	Pa 46	.531 J.89	49.92	Pt 78	.973 5.84 .1761 1.81		17.08	Eu 63	.758 1.86 .1167 1.85			
				(A)		v (eV)					68.39	Co 27	.294 4.39 .1623 1.82	62.86	Rh 45	.513 5.75	59.52	Ir 77	.959 6.94 .1823 .82		19.73	Sm 62	.75 2.14			
0				eshold Energy	aic Number	imation Energ	+ pun				70.56	Fe 26	.279 4.28 .1553 1.81	74.43	Ru 44	.504 6.74 .1649 1.85	70.24	0s 76	.949 8.17 .183 1.82		•	Pa 61	.723 0 0 1.85			
UTTERING VIELL					Atom	Idu2	5.32 1.7				48.78	Hn 25	.274 2.92 .1506 1.81	76.53	Tc 43	.493 6.85 .161 1.85	69.39	Re 75	.929 8.03 .1771 1.82		31.82	07 PN	.719 3.4	40.45	U 92	1.187 5.55
HEAVY-ION BPI BB 200.5					1		240.				71.59	Cr 24	.259 4.1 .1508 1.81	77.52	Mo 42	.479 6.82 .1534 1.85	77.16	M 74	.917 8.9 .1714 1.82		34.94	Pr 59	.703 3.7	0	Pa 91	1.152 0
DEPENDENCE OF ILEH					Symbol	Ratio (M2/M1	for 1 e				94.3	v 23	.254 5.31	87.66	4 QN	.463 7.57 .1406 1.85	70.51	Ta 73	.902 8.1 .1594 1.83		40.68	20 20	.699 4.32 .1106 1.85	46.10	Th 90	1.157 6.2
FOR ANGULAR PROJECT Z - NUI MASS-NI						Ass					90.67	11 22	.239 4.85	73.16	Zr 40	.455 6.25 .1239 1.85	56.27	#	.89 6.44 .1425 1.83			/	/	\int	/	/
PARANETERS											76.99	5c 23	.224 3.9	51.95	۲ 39	.443 4.37	42.45	La 57	. 693 4.47		32.23	Ac 89	1.132 4.25			
тавье 1 8				1.52		4 88 81	.045 3.32	53.48	Mg 12	.121 1.51	40.19	Ca 20	.2 1.84 .0749 1.8	20.63	ឆ ភ	.437 1.72	18.13	Ba 56	.685 1.9 .0799 1.85		12.64	Ra 88	1.127 1.66			
	•	- H	.005 0	7 275		n 1	.035 1.63	41.61	Na 11	.115 1.11	20.78	K 19	.195 .93	10.35	8 8	.426 .85 .061 1.84	7.734	8	.663 .8 .0595 1.85		•	Fr 87	1.112 0			

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ТА	.087	л н	0 .26 0 .132	1 IBS	n 1	.2886 .61 .3 6.386 .495 14.		.861	Na 11	.8946 1.47 .6 ⁻ 9.483 1.67 13.	1.707	× 19	1.548 2.41 .8 15.48 2.87 27.	4.003	69 13	2.858 5.5 1. 29.69 6.36 61.	6. 698	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	4.269 9.11 1.1 47.15 9.98 114	12.2	Fr 87	0 16.9 3.1 0 16.9 18/			
VBLE 19 PA				. 256	Be 4	554 . 72 45 . 642		- 96.	Mg 12	-72 1.55	1.823	C 28	117 2.47 .39 .4 2.95 65.	4.144	5r 38	444 5.66 .57 .85 6.53 159	6.857	Ba 56	83 9-46 .7E	12.39	Ra 88	149 17.1 1.2 6 17.1 478			
VRAMETERS OF											1.937	Sc 21	975 2.77 72 3.31 8	4.256	۲ 39	796 5.75 . 7.8 6.63 2	7.017	La 57	892 9.59 7.8 10.4 5	12.57	Ac 89	241 17.2	r		
THE THIRD I PROJECTIL Z - NUME MASS-NUM							Thresho				2.054	11 22	1954 2.96 7.62 3.53	4.429	Zr 40	2773 5.92 35.6 6.81	9.523	Hf 72	465 12.9	$\left \right $	/	/		/	7
MATSUNAMI EMP LEH' 3ER1			-		Symbol		ld Energy(eV)				2.173	۲ 23	2755 3.15	4.574	ND 41	.324 6.04 291.6 6.94	9.697	ta 73	.3851 13.1 692.5 13.7	7.179	29 29	.8276 9.69 271.3 10.5	12.76	Th 90	7721 17.7
IRICAL FORMU				.256	1	P					2.296	3 5	.5311 3.22 81.11 3.84	4.719	Mo 42	.3594 5.27 272.6 7.17	9.871	и 74	.4999 17.4 775.7 13.9	7.342	Pr 59	.9787 9.75 233.9 10.6	12.95	Pa 91	0 17.6
NLA AT NORMAL				1-1-1-	1 - Aton	72 Alpt					2.418	Mn 25	.7336 3.41	4.865	Tc 43	.4014 6.49 284.1 7.39	10.05	Re 75	.6503 13.6	7.504	07 PN	1.082 10 221 10.8	13.13	n 42	.7069 18.2 662.4 18
INCIDENCE				000	dic Number	1	astic Coettic				2.544	Fe 26	.4767 3.47 91.71 4.13	5.012	Ru 44	.5904 6.64 286.5 7.55	10.22	0s 76	.7259 13.9 742.2 14.4	7.568	Pm 61	0 10.1 0 10.9			
											2.669	Co 27	.4834 3.67 99.93 4.36	5.161	Rн 43	.6056 6.7B 249.9 7.7	10.4	r 77	.8308 14.1 638.5 14.5	7.832	Sm 62	1.772 10.5			
						:	11UN 4				2.799	N1 2B	.4814 3.66 100.6 4.35	5.31	Pd 46	.7861 7.05 175.9 7.96	10.58	Pt 78	.8232 14.3 546.8 14.7	949.7	Eu 63	2.065 10.7			
											2.926	Cr 29	.757 3.98 86.55 4.71	5.461	Ag 47	1.134 7.15 135.5 8.07	10.75	Au 79	1.213 14.5 361 14.9	B. 163	Gd 64	.9437 11.1 293.6 11.8			
											3.056	Zn 30	1.51 4.1 34.58 4.85	5.611	Cd 48	2.607 7.51 55.97 8.42	10.93	На ву	7.129 14.8 64.89 15.2	8. 331	Tb 65	.977 11.2 296 12			
				. 333	ย 8	.10B .B1 27.66 .774		40.1	A1 13	.3594 1.7 33.68 1.96	3, 187	Ga 31	.747 4.4 77.49 5.17	5.764	In 49	1.222 7.69 124.7 8.6	11.11	T1 81	2.572 15.2 186.3 15.4	B. 498	Dy 46	1.321 11.5 228.3 12.2			
				.415	ہ د	.2807 .88 37.68 .868		1.163	S1 14	.1888 1.76 47.84 2.05	3.319	Ge 32	.4702 4.6 111.2 5.39	5.917	S S	.2099 7.98 161.5 8.89	11.29	Pb 82	2.409 15.4 204.5 15.7	B. 667	40 67	1.296 11.7 240 12.4			
				. 498	r z	.1547 .98 27.93 1.01		1.20/	۰ ۱3	.3556 1.93 39.07 2.26	3.454	As 33	.7464 4.76 88.69 5.57	6.071	5 5	1.162 8.23 145.9 9.12	11.47	B1 83	2.266 15.6 221.9 15.8	B. 837	Er 68	1.253 11.9 255.7 12.6			
				.384	8	.3161 1.09 16.3 1.16	-	c/?*1	S 16	.4477 1.99 33.62 2.35	3.589	Se 34	1.008 5.04	6.225	Te 52	1.463 8.69 125.2 9.57	11.45	Po 84	3.324 15.7 153.7 15.9	9,007	ĭm 69	1.723 12.1 190.4 12.7			
L				.672	F 9	1.042 1.25 6.058 1.37	1 200 .	1.400	CI 17	.9502 2.19 18.32 2.6	3.726	27 27	1.9 5.11 39.39 5.94	6. 3 83	1 53	2.976 8.63 61.91 9.52	11.84	At 85	0 15.7 0 15.9	0.178	Yb 70	2.645 12.4 129.6 13			
	.124	He 2	0 .45	. 767	Ne 10	46.93 1.32 .152 1.46		140-1	Ar 18	17.33 2.46	3.864	kr 35	19.82 5.39 4.096 e.24	6.54	Xe 54	21.03 8.98 9.295 9.85	12.02	F.n 86	25.63 16.8 21.93 16.8	9.35	Lu 71	.9466 12.6 363.6 13.2			

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3. 017 C. 2. 017 S. 017 S. 017 S. 4. 153 S. 561 A. 4. 153 S. 561 A. 4. 153 C. 4. 15 S. 561 A. 4. 15 C. 4. 15 C. 4. 15 S. 561 A. 4. 15 A. 4. 15	
It NI 28 NI 28 NI 28 NI 28 NI 28 12 2.893 1.29 2.409 1.0.68 2.10 206 2.2 1.0.68	
t k in LSS Un 2.759 2.759 2.759 2.759 2.759 2.759 2.759 2.123 2.1333 2.1333 2.1333 2.1333 2.1333 2.1333 2.1333 2.1333 2.	
Umber Umber 10.534 11.234 11.23 11.23 11.23 10.53 11.23 10.53 11.23 11.23 11.23 11.23 11.23 11.23 11.23 11.23 11.23 12.13 11.2	
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The THIRD MAT PROJECTILE 2 - "UNBER PASS-NUMBER PASS-N	7
ARAMETERS OF 2.021 2.021 2.021 2.021 2.021 2.021 2.021 2.00 1.18 2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.0	
ABLE 21 Part 1, 036 Part 1,	
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	TABLE 22	PARAME TERS	OF THE THIRD PROJECTI Z - NUT MASS-NU	MATSUNAMI ENF ILE	PIRICAL FORMUR	NLA AT NORMAL	INCIDENCE										
.492																L	. 438
- I																	#
0 .18 0 .086							ţ										0 .26 0 .105
282	22	- -					000								-		
				Symbol	1	Atomi	1¢ Number					CAP.	1.087	1.267	104-1	1.027	100.1
2 2	Be 4			a		Aloha						n m	ء ب	r z	8 5	с 1	Ne 10
7.101 .141	.9747 .35		i		. 9747 .	RE	1					.2954 .38 21.73 .196	.765 .39 27.19 .216	.4164 .42 17.81 .244	.8386 .45 9.354 .273	2.696 .49 3.045 .314	120.5 .51
		1,	Thresho	old Energy(eV)		Inel, Inel,	astic Coeffic	tent k in LSS	i Unit								
2.029	2.245											2.448	2.674	2.884	3.117	3.33	3.54
Na 11	Mg 12											A1 13	SI 14	۳ ت	S 16	CI 17	Ar 18
2.244 .55 4.143 .372	1.733 .57 5.708 .392											.8755 .6 13.19 .43	.4567 .62 18.25 .448	.8428 .65 14.01 .489	1.054 .67	2.188 .71 6.065 .555	38.82 .77 .368 .618
3.8	4.047	4.264	4.502	4.744	5.002	5.25	5.514	5.768	6.045	4.293	6.562	6-821	7.09	7.345	7.634	7.92	8.195
×	Ca 20	Sc 21	11 22	v 23	54 54	11 23	Fe 26	Co 27	11 28		2n 30	6. 31	6 12	i a	4 F.	þ	Kr 34
3.491 .76	1.821 .78	. 8682 . 84	4205 AB	5844 97	10 01 1	10 175 1		101									
4.232 .609	8.486.625	19.22 . 694	24.87 .757	28.35.781	867. 2.22	16.42 .841	24.36 .857	25.99 902	26.21 .901	21.88 .971	3.032 1.11 B.655 1	18.97 1.06	26.88 1.1	21.22 1.14	16.87 1.2	9.246 1.21	.948 1.27
8.483	8.77	9.064	9.356	9.652	9.945	10.24	10.54	10.85	11.14	11.45	11.75	12.06	12.37	12.68	12.99	13.32	13.63
Rb 37	ra B	Y 39	2r 40	ND 41	Ma 42	Tc 43	Ru 44	Rh 45	Pd 46	Ag 47	Cd 48	In 49	ទួ	50 S5	Te 52	1 53	Xe 54
5.412 1.39 6.837 1.3	2.719 1.42	1.089 1.44 36.43 1.35	.518 1.47 53.34 1.38	.6032 1.49 65.71 1.41	.6647 1.54 60.99 1.46	.7377 1.58 63.04 1.5	1.081 1.61	1.104 1.64 54.95 1.56	1.424 1.69 38.4 1.61	2.0571 29.49 1.64	4.672 1.77 12.08 1.7	2.18 1.81 26.8 1.74	.3722 1.86 34.49 1.3	2.05 1.91 31 1.84	2.559 2 26.37 1.93	5.212 1.99 13.05 1.92	36.61 2.05 1.948 1.99
13.95	14.27	14.6	19.47	20.02	20.38	20.73	21.08	21.44	21.8	22.16	22.52	22.88	23.24	23.61	23.98	24.36	24.71
5° 53	Ba 56	La 57	HF 72	Ta 73	и 74	Re 75	05 76	Ir 77	Pt 78	Au 79	н д во	11 81	Pb 82	B1 83	Po 84	At 85	Rn 86
7.414 2.08 9.862 2.01	3.16 2.14 24.22 2.08	1.36 2.17 57.67 2.1	.7689 2.77 108.5 2.7	.6354 2.81 138.5 2.74	.8228 2.86 154.9 2.79	1.068 2.9	1.189 2.96 147.6 2.88	1.358 2.99 126.8 2.91	1.343 3.04	1.977 3.07	11.58 3.12 12.83 3.04	4.168 3.19 36.76 3.1	3.896 3.23 40.29 3.14	3.66 3.26 43.69 3.17	5.365 3.28 30.24 3.19	0 3.28 0 3.19	41.05 3.47 4.291 3.37
25.08	25.45	25.83	/	14.93	15.26	15.59	15.93	16.25	16.59	16.92	17.26	17.6	17.94	19.28	18.63	18.97	19.32
Fr 87	Ra 89	Ac 89	/	Ce 58	Pr 59	09 PN	Pm 61	Sm 62	Eu 63	Gd 64	Tb 45	Dy 66	Ho 67	Er 68	Tm 69	Yb 70	Lu 71
u 3.49 U 3.38	5.031 5.54	1.981 3.56 93.49 3.45	7	1.424 2.16 56.24 2.12	1.683 2.2 48.45 2.14	1.853 2.24 45.62 2.19	0 2.2 0 2.2	3.012 2.34 29.99 2.28	3.504 2.36 26.36 2.3	1.592 2.44 60.84 2.38	1.646 2.47 60.21 2.41	2.217 2.52 46.29 2.46	2.169 2.56 48.57 2.5	2.092 2.6 51.65 2.53	2.874 2.62 38.41 2.56	4.394 2.69 26.06 2.62	1.603 2.72 73.02 2.65
			\overline{V}														
			/	26.2	26.58	26.95											
			/	11 %	Pa 91	u 92											
			/	1.261 3.64	0 3.62	1.122 3.74 128.8 3.61						•					
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	3.263	å v	.086		8-241		.6 .31 3 .17			4r 18	1 . 41	28.61	4 2 2			45.59	(e 54	7 .82 , .803	79.81	8	6 1.23	19 1.34	63.28	-12 m	52 1.02 11 1.06			
		<u> </u>	22				6.2 438. 6.2 .08£			-	54 . 291	8	۔ س	131	-	- 9		716 118		. r	18 121.	27 1.4	6	۲ و	01 4.9: 05 26.0			
					7.48	r	9.732 .3 3.812 .1		1	5	8.161 .3 5.18 .2	27.7	ł	12.78 .6		44.6	г П	17.01 .E	78.6	40	·	0	62.1	۲D 7	13.6 1. 9.32 1.			
					6.474	5	2.972 .28 12.85 .148		12.0	S 16	3.938 .37 10.76 .237	26.83	Se 34	6.803.59 8.40 408		43.56	Te 52	8.338 .81 10.63 .78	77-44		16.06 1.18	10.16 1.27	61.15	Tm 69	8.933 .99 13.85 1.03			
					6.326	z	1.447 .27 26.17 .137		11./6	Р 13	3.143 .37 13.06 .229	26.03	As 33	5.131.57		42.68	Sb 51	6.736 .78 12.77 .747	74.49		10.96 1.17	14.7 1.26	60.0a	Er 68	b.514 .98 18.7 1.02			
					5.687	0 U	2.589.26 43 .127		<1.11	S1 14	1.701.35 18.1.214	25.16	Ge 32	3.267 .56 14.54 .443		41.72	Sn 50	1.228 .77 14.37 .73	74, 15	CB 44	11.68 1.16	13.59 1.23	58.99	Ho 67	6.768 .97 17.67 1			
					4.857	n 20	.9758.25 36 .118		10.3	AI 13	3.25 .35 13.41 .207	24.32	Ga 31	5.264 .55 10.51 .447		40.78	In 49	7.234.75 11.34.70B	74.27		12.53 1.15	12.45 1.23	57.92	Dy 66	6.933 .96 16.93 .987			
				_								23.57	Zn 30	10.89.53		39.81	Cd 48	15.56 .74 5.163 .694	71.75		34.94 1.13	4.371 1.71	56.89	Tb 65	5.168 .95 22.2 .5(6			
												22.7	Cu 29	5.506 .52 12.83 .412		38.93	Ag 47	6.875 .72 12.86 .668	10.01	A 1 79	5.982 1.12	24.5 1.19	55.62	Gd 64	5.009 .94 22.53 .956			
								nun				22.01	N1 28	3.6 .5 16.14 .387		37.93	Pd 46	4.783 .71 16.85 .659	20.91	P+ 78	4.07 1.11	57.27 1.18	54.84	Eu 43	11.09 .92 9.889 .926			
								ובטר א זש הפח				21.02	Co 27	3.603.5		37.02	Rh 45	3.73 .7		07. d	4.127 1.1	43.79 1.16	53.78	Sm 62	9.55 .91 11.3 .916			
INCIDENCE				000	ic Number	0						20.25	Fe 26	3.616 .49 15.49 .369		36.05	Ru 44	3.66 .69 28.51 .628		90-60 72 -0	3.618 1.09	51.13 1.15	52.82	Pm 61	0 886 . 0			
LA AT NORMAL					Atom,	Hall I	24 107	Taur				19.34	£ N	5.586 .48		35.1	Tc 43	2.506 .68 28.71 .616	:	10.10	3.264 1.07	49.43 1.13	51.74	09 PN	5.917 .68 17.47 .68	86.74 U 92 704 1	11.79 1.43	-
IRICAL FORMUAI 2.01					<u></u>		23.43					18.57	с 24	4.115 .47		34.19	Mo 42	2.269 .67 28.22 .599		10.00	2.519 1.05	54.25 1.11	50.73	Pr 59	5.397 .87 18.73 .861	85.65 Pa 91	0 1.39	
MATSUNAMI EMP LE6 BER 6 MBER 1					Symbol	æ		ita Energy(ev)				17.69	v 23	2.144 .47		33.28	Nb 41	2.069 .65 30.92 .581		54-00 11	1.951 1.04	48.78 1.1	49.66	Ce 28	4.57 .86 21.79 .855	84.42 Th 90	5.46 1.4	
OF THE THIRD PROJECTI Z - NUM MASS-NU								ousauu				16.95	11 22	1.55 .45		32.33	2r 40	1.781 .65 25.35 .571		04.34	2.367 1.03	38.38 1.08	/		/	\square	7	
PARAMETERS												16.21	Sc 21	3.213 .44		31.41	۲ 39	3.757 .64 17.56 .558		48.61	4.369.86	22.43 .848	83.31	Ac 89	5.849 1.25 30.72 1.37			
TABLE 23					4.152	8e 4	3.095 .24 23.43 .107		4.666	Mg 12	6.405 .33 6.19 .193	15.66	Ca 20	6.789 .41 6.69 .282		30.45	5r 38	9.4 .63 6.873 .549		/0./4	10.17 .85	9.465 .838	82.13	Ra 88	14.86 1.25 11.96 1.36			
	4.94		0 09B		3.504	1	2.351 .22 13.93 .096		8,867	Na 11	8.249 .33 4.644 .184	14.79	K 19	13.01 .41		29.54	Rb 37	18.77 .62 3.367 .537		40.02	24 5	3.907 .813	80.98	Fr 87	0 1.24 0 1.35			

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	тав це 24	PARAMETERS	OF THE THIRD PROJECTI Z - NUMI MASS-NUI	MATSUNAMI EMP LE	IRICAL FORMUA 0 0.18	la at Normal 1	INCIDENCE									ſ	
15.35																	9.269
-1 -1 -1																	He 2 .
0 .13 0																	0 .17 0 .086
9.341	10.65				10.6		00					12.12	13.93	15.13	16.35	17.08	18.73
C 1	Be 4			Symbol.	1	Atomi	c Number					ۍ ه	ہ۔ ن	r z	8	ъ Ц	Ne 10
3.586 .19 21.16 .09	4.858 .2 34.72 .097		Theorem		4.858 .		atte Confile	tent k in ISS	that t			1.565 .21 52.25 .104	4.212.22 61.58.11	2.395 .23 36.7 .117	4.993 .24 17.66 .123	16.63 .25 5.091 .132	755.2.26
19.66	21.23											22.27	23.91	24.94	26.57	27.51	28.25
Na 11	Hg 12											AI 13	Si 14	e L	S 16	CI 17	Ar 18
14.38 .27 5.985 .146	11.23.28 7.889.151											5.749.29 16.73.16	3.022 .29 22.38 .165	5.625 .3 15.79 .174	7.074 .3 12.91 .179	14.75 .32 6.066 .189	261.9 .33 .331 .203
30.37	32.03	32.74	33.97	35.22	36.87	38.16	39.85	41.15	43.06	44.07	45.63	46.8	48.23	49.75	51.05	52.78	54.13
k 19	Ca 20	Sc 21	TI 22	v 23	Cr 24	Ш. 23	Fe 26	Co 27	N1 28	Cu 29	Zn 30	Ga 31	Ge 32	As 33	Se 34	r S	kr 36
23.66 .33 3.874 .203	12.38 .33	5.883 .35 15.47 .222	2.845 .36 18.88 .232	3.944 .37 20.33 .242	7.577 .37 15.61 .247	10.3 .38 10.98 .257	6.676 .38 16.04 .261	6.657 .39 16.28 .271	6.659 .39 16.47 .272	10.19 .4 12.78 .288	20.16 .41 4.926 .295	9.746 .42 10.18 .309	6.05 .43 13.91 .319	9.502 .44 10.67 .328	12.59 .45 8.097 .341	23.66 .45 4.389 .346	242.3 .46 .432 .359
															•		
55.78	57.38	59.1	60.69	62.37	63.9	65.45	67.11	6.83	70.33	72.09	73.53	75.2	76.75	78.38	79.78	81.76	83.31
89 37	ŝ	4 7	2r 40	ND 41	Mo 42	Tc 43	Ru 44	Rh 45	Pd 46	Ag 47	Cd 48	In 49	ŝn 50	50 51	Te 52	1 53	× 4
34.73 .47 3.06 .366	17.39 .47 6.197 .374	6.949 .48 15.75 .379	3.294 .48 22.57 .388	3.825 .49 27.37 .394	4.191.49 24.73.405	4.626 .5 24.91 .416	6.752.51 24.58.423	6.879.51 21.02.431	8.812 .52 14.29 .443	12.66 .53 10.86 .449	28.6 .54 4.303 .465	13.29 .35 9.387 .474	2.253 .56 11.73 .487	12.35 .56 10.38 .498	15.24 .58 8.519 .516	31.11 .58 4.234 .517	216.8 .59 .616 .533
85.11	86.49	88.5	115.4	117.3	119.1	121	122.8	124.7	126.6	128.5	130.4	132.2	134.1	136.1	138.1	140.2	141.6
8 5	Ba 56	La 37	HF 72	Ta 73	N 74	Re 75	0s 76	Ir 77	Pt 78	Au 79	Hg BO	T1 B1	Pb 82	B1 93	Po 84	At 85	Rn 86
43.82 .59 3.091 .539	18.53 .61 7.416 .555	7.958 .61	4.25 .71 27.88 .709	3.5 .72 35.29 .719	4.515 .73 39.08 .729	5.844 .73 35.49 .739	6.468 .74 36.5 .753	7.374.75 31.17.761	7.265 .76 26.43 .771	10.67 .76 17.33 .779	62.24 .77 3.077 .792	22.29.78 8.723.806	20.77 .79 9.49 .817	19.47 .79 10.24 .824	28.52 .8 7.068 .829	0 .8 0 .829	215 .83 .973 .872
143.7	145.6	147.7		90.36	92.25	93.95	95.85	97.41	99.27	100.9	102.7	104.4	106.3	108.1	110	111.7	113.6
Fr 87	а 88 88	Ac 89		8 29	Pr 59	09 PN	Pm 61	5m 62	Eu 63	Gd 64	tb 45	Dy 66	Ho 67	Er 68	Tm 69	Yb 70	Lu 71
0 .83 0 .876	26.24 .84 8.166 .887	10.33 .84 20.96 .892		8.322 .61 16.97 .566	9.826 .61 14.56 .57	10.76 .62 13.49 .582	0 .63 0 .586	17.33 .64 8.616 .605	20.12 .64 7.518 .611	9.064 .66 16.76 .63	9.347 .66 16.66 .636	12.52 .67 12.62 .649	12.21 .68 13.12 .659	11.74 .68 13.83 .667	16.1 .69 10.22 .674	24.46 .7 6.827 .689	8.904 .7 19 .696
				149.5	151.7	153.5											
				Th 90	Pa 91	U 92											
				6.335 .85 30.99 .91	0 	5.776 .87 28.19 .933											

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63.05 H 1 0 112 0 112 35.494 0.112 35.494 0.115 35.494 0.115 79.49 79.49 79.49 5.499 146 5.499 146 5.499 146 5.499 146 5.499 146 5.497 26 5.497 26 5.407 26 5.	TABLE 25 36.85 36.85 36.62 17 26.22 10 10 12 13.15 13.15 130.5 100.5 100	83.5 8.5 8.5 8.5 11.47.27 21.18.155 1.4.34.35	OF THE CHELTO 7 - NUR - NUR	Reference of the second of the	99.94 97.94 97.52 91.5 91.5 91.5 15.01.29 15.01.29 15.01.29 15.01.29 15.01.29 15.01.29 15.01.29 15.01.29 15.01.29 15.01.29 15.01.29 15.01.29 15.01.20 15.00 15.01.20	4.4. AT NCR444.	INCIDENCE INC Number a sstic Coeffic 13.32 29 20.63 1175 149.4 149 44	15.11 LS: 99.84 15.35 .3 20.6 .18 15.27 14.28 .37 14.28 .37) Unit 104.4 Ni 28 135.4 135.4 135.4 18.3 - 337	105.5 20.57 .3 113.8 .1188 1339 Ad 47 26.31 .38	108.7 2n 30 2n 30 2n 30 161.3 161.3 161.3 59.46.33	40,64 8 5 2,533 (18 2,533 (18 2,533 (18 62.81 41 13 10.49 (23 10.49 (23 10.49 (23 10.49 (23 10.49 (23 10.49 (23 10.49 (23) 10.49 (23) 10.41 (23) 10.42 (23) 1	45.79 C 6 6.869.18 6.869.18 107.4.1 113 5.552.23 34.22.127 34.22.127 167.2 167.2 5 5.504 1.67.2 5 5.04	48.39 N 7 3.987.19 5.987.19 68.38 10.47.24 115.9 115.9 115.9 1170.2 110.2 1170.	51.02 0 8 8.465.2 29.72.106 5 16 5 16 118 5 16 13.24.24 13.24.24 19.2.113 5 5.79.23 25.79.23 25.79.23 25.79.23 25.79.23 25.79.23 25.79.23 25.79.23 25.79.23 25.77.23	51.68 F 9 228.64 .21 8.351 .109 73.44 C1 17 73.44 C1 17 121.7 Br 35 8.622 .235 8.622 .235 8.622 .245 6.625 .465 6.625 .465	35-3 He 2 0
3.417 .228	767 · ACA.0	CCZ. #C./1	24.01 .237	27.04 .243	20.40	SEZ. EC.07	ACZ. 41.02	102. 7.12	14.7 .268	1/2. 11.11	4.33I .27B	1 4 57 . 285	11.61 .29	10.12 .296	8.151.306	4.06 .305	-283
182.8 Cs 35	185.5 Ba 56	189.1 La 57	239.7 Hf 72	243.2 Ta 73	246.7 H 74	250.2 Re 75	255.4 De 76	257.1 Ir 77	240.6 Pt 78	264.3 Au 79	267.7 Hg BO	271 T1 81	274.6 Pb 82	276.4 B1 83	282.3 Po 84	286.5 At 85	R 28
91.19 .41 2.91 .317	38.56 .42 6.887 .324	16.56 .42 16.19 .328	8.799 .48 23.24 .404	7.245 .48 29.25 .409	9.339 .40 32.18 .415	44 . 80 . 44 29.06 . 419	13.36 .49 29.62 .427	15.23 .5	14.99 .5 21.23 .436	22.01.5	128.3.51 2.444.447	45.89 .51 6.875 .454	42.73.52 7.438.46	40.05 .52 7.999 .463	58.45 .52 5.508 .466	0 .52 0 .467	440.6 .
292.2	295.8	299.8		192.8	196.6	199.7	203.6	206.1	209.7	212.4	216	219.1	222.6	226.1	229.8	232.8	236.
Fr 87 0 .54 0 .49	Ra 88 53.77 .54 6.177 .496	Ac 89 21.14 .55 15.83 .498	/	Ce 58 17.32 .42 15.63 .331	Pr 59 20.45 .43 13.38 .333	Nd 60 22.39 43 12.28 .339	Pm 61 0 .43 0 .341	5m 62 36.03 .44 7.71 .35	Eu 63 41.84 .44 6.699 .354	6d 64 18.83 .45 14.9 .363	Tb 65 19.42 .45 14.57 .367	Dy 66 25.99.46 10.94.373	Ho 67 25.35 .46 11.7 .378	Er 68 24.37 .46 11.84 .383	Tm 69 33.39.47 8.711.366	Yb 70 50.7 .47 5.764 .394	Lu 7 18.45 .4 15.97 .3
				303 Th 90 13.36 .55 23.2 .508	307.4 Pa 91 0 .55	310.3 U 92 11.79.56 20.89.519											

	1ABLE 26	PARAMETERS	I OF THE THIRD PROJECT Z - NUX MAGS-NI	MATSUNAMI EM TLEA MBER	PIRICAL FORMU ^I 13 26.98	ALA AT NORMAL	INCIDENCE										
28.35																	16.5
н н																	He 2 .
0 .12 0 .113	1																0 .16 0 .087
16.16	18.11	 _			18.1		1000					20.31	23.13	24.81	26.51	27.32	29.78
2	Be 4	_		Symbo	1 Be	Atom	aic Number					รา ส	ہ ن	N 7	8	ъ г	Ne 10
4.367 .18 27.21 .088	5.997 .19		1		5.997 .	19 094			:			1.952 .2	5.292.2 77.28.105	3.038 .21 45.64 .11	6.385 .22 21.78 .115	21.48.23	979.7.24 .141.125
30.91	33.21							cient k in LS:				34.55	36.94	38.22	40.58	41.68	42.43
Na 11	Mg 12											A1 13	St 14	۹ آنا	S 16	C1 17	Ar 18
18.79 .25 7.179 .131	14.74 .25 9.418 .135											7.589 .26 19.78 .141	4.001 .26 26.35 .146	7.485 .27 18.42 .152	9.435 .27 15 .156	19.77 .28 6.972 .164	352.9 .3 .375 .173
45.64	48.02	48.68	50.27	51.88	54.21	55.89	58.28	26-95	62.72	63.87	62.99	67.42	69.29	71.33	72.97	75.36	77.09
K 19	Ca 20	Sc 21	11 22	23	Cr 24	۳ 23	Fe 26	Co 27	N1 28	Cu 29	2n 30	Ga 31	Ge 32	As 33	Se 34	R 33	. rr 36
31.88 .29 4.404 .174	16.7 .3 8.605 .178	7.973.31 17.29.188	3.865 .32 20.92 .196	5.37 .32 22.34 .203	10.33 .33 17.11 .207	14.07 .33 11.94 .214	9.125 .34 17.4 .218	9.114 .34 17.53 .226	9.121 .34	13.98 .35 13.61 .238	27.69 .36 5.224 .244	13.4 .37 10.69 .254	B.326.38 14.51.262	13.09.38 11.08.268	17.35 .39 8.338 .278	32.62 .39 4.512 .282	334.2 .4 .44 .292
79.33	B1.4B	AT BY	PK OA	FC DB	AC OD	10 00			AC 00			0 201	c 201	1 001		0 111	9
£	ъ 8	4 7	2r 40	4 14	Ao 42	Tc 43	Ru 44	5 5	Pd 45	Ag 47	5d 48	In 49	Sn 50	8 21	Te 52	8	xe 54
47.92 .4 3.11 .297	24 .41 6.274 .303	9.596 .41 15.91 .307	4.549 .42 22.69 .314	5.285 .42 27.44 .319	5.792 .43 24.65 .327	6.394 .43 24.71 .335	9.333 .44 24.29 .341	9.51 .44 20.71 .347	12.18 .45 14 .356	17.5 .45	39.54 .46 4.174 .372	18.37 .47 9.072 .379	3.114 .47 11.32 .389	17.06 .48 9.928 .398	21.05 .49 8.081 .413	42.98 .49 4.02 .412	299.4 .5 .581 .424
118.2	120.2	122.7	158.3	140.7	163.2	165.7	168	170.6	173	175.6	178	180.4	183	185.6	188.3	191.1	192.8
ទី	Ba 56	6	Hf 72	Ta 73	ы 74	Re 75	Ds 76	Ir 77	Pt 78	Au 79	Hg B0	11 81	Pb 82	Bi 83	Po 84	At 85	Rn 86
60.5 .5 2.911 .429	25.58 .51	16.36 .445	5.84 .59 24.92 .558	4.809.6 31.47.565	6.2 .61 34.75 .573	8.023 .61 31.48 .58	8.874 .62 32.26 .591	10.12 .62 27.5 .597	9.962 .63 23.26 .605	14.63 .63 15.23 .611	85.28 .64 2.695 .621	30.52 .65 7.616 .632	28.42 .65 8.267 .64	26.65 .66 8.908 .645	39.02 .66 6.142 .649	0 66. 0 55. 0	293.6 .68 .838 .681
193.5	861	200.8		125.2	127.8	130	4.011	134.5	14	511	141 5	14T. B	144.2	148.7	151.2	153.4	155.9
Fr 87	Ra 88	Ac 89	/	85 5	Pr 59	09 PN	Pm 61	5a 62	Eu 63	6d 64	4 53	Dy 66	Ho &7	Er 68	Ta 69	Yb 70	Lu 21
0 .68 0 .685	35.82 .69 7.01 .693	14.09.69 17.98.697	/	11.49 .52 15.83 .449	13.56 .52 13.57 .452	14.85 .53 12.52 .461	0 .53 0 .464	23.89 .54 7.938 .478	27.74 .54 6.914 .483	12.49 .55 15.5 .497	12.87.56 15.2.503	17.24 .56 11.47 .512	16.81 .57 11.89 .519	16.16 .57 12.5 .526	22.15 .58 9.22 .531	33.64 .58 6.136 .542	12.24 .59 17.04 .54B
			ľ								-						
			/	203.2	206.1	208.3											
			/	Th 90	16 Pa	U 92											
			7	8.914 .7 26.49 .711	0 .709	7.871 .71 24 .728											

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	76-94	μ 2 2 3 3	0 .14		B4.29 94.16 98.37 102.6 110.3			3.277 .17 .17 9.017 .17 5.278 .18 11.5 .18 38.68 .19 1792 .19 124.3 .097 144.4 .101 84 .104 39.5 .106 11.01 .108 .249 .111	efficient k in LSS Unit	120.6 127.7 129.5 136.4 137.3 136.5	A1 13 S1 14 P 15 S 16 C1 17 A7 18	14.5 .21 7.701 .21 14.61 .22 18.54 .22 39.41 .22 714.8 .23 35.79 .118 .23 35.79 .118 44.06 .121 30.24 .124 24.47 .126 11.15 .129 .584 .113	.i 177.2 183.8 183.8 190.9 192.7 196.5 201 207.7 209.7 212.7	26 Co 27 Ni 28 Cu 29 Zn 30 Ga 31 Ga 32 As 33 Se 34 Br 35 Kr 36.	26 19-55 26 30.25 27 60.14 27 29.3 28 18.5 28.42 29 72.36 29 744.5 3 155 24.16 18.63 16.7 19.29 177 19.56 18 72.36 29 744.5 3 155 24.78 16 18.46 7.167 164, 19.57 174, 19.29 134.56 188 7357 189 3559 192 3559 192 3559 192 3559 192 3559 192 3559 192 3559 192 3559 192 3559 192 3559 192 3559 192 3559 312<	.7 256.8 260.6 266.2 269.2 277.9 282.2 284.7 291.8 295.4	44 Rh 45 Pa 46 Ag 47 Ca 48 In 49 Sh 30 Sh 31 Te 32 I 33 Xe 34	32 21.58 32 27.7 35 90.22 35 90.22 35 91.94 37.127 34 39.09 35 98.69 35 688.5 35 218 24.45 :221 16.21 :228 4.744 :235 10.27 :237 11.66 :242 10.97 :249 10.97 :239 68.5 .625 .239	.2 411.7 416.9 422.6 427.5 432.3 437.5 45.3 45.3 45.3 489.4 955.9 457.3	76 Ir 77 Pt 78 Au 79 Hg 80 T1 B1 Pb 82 B1 83 Po 84 At 85 Rn 85	42 23.43.42 23.06.42 33.89.43 197.5.43 70.67.43 65.8 44 61.69.44 90.54 90.54.44 0 .44 678.5.45 33 345 25.15.348 21.14.352 13.78.355 2.42 .36 6.703.366 7.319.37 7.856.373 5.405.375 0 .375 72 .391		17 336 341.6 345.1 350.6 355.1 360.4 365.6 375.6 361.2 1 5 4 5 5 4 5 5 1 7 5 7 5 75.6 361.2	21 37 35.21.38 64.13.38 28.88.38 29.79.39 39.9.39 39.92.39 30.92.39 37.42.39 31.3.4 77.92.4 28.36.4	28 8.066 .287 6.795 .29 15.46 .297 15.09 .3 11.28 .305 11.62 .308 12.14 .312 8.918 .314 5.874 .32 16.24 .333				
A AT NORMAL INCI				EL/1000		ALDRIC N	Alpha		Inelasti				167.7	Hn 25	29.86 .26 19. 17.21 .154 24.	246.7	Tc 43	14.46 .32 21. 29.58 .215 28.	401.6	Re 75	18.59 .41 20. 29.2 .339 29.		326.6	34.28 .37 0	12.94 .279 0	490.2	1	U 92	U 72
IRICAL FORMUALF					77.33		1	9.856 .14	ſ				164.5	Cr 24	21.77 .25	242.5	Ma 42	13.07 .31 29.83 .211	396.2	н 74	14.37 .41 32.41 .336		322.1	31.29 .37	14.16 .274	486.4		Pa 91	Pa 91
HATSUNAMI EMPI LE						symbol	٩		ild Energy(eV)				158.2	د 23	11.28 .25 32.85 .148	238.5	ND 41	11.9 .31 33.58 .207	391.1	Ta 73	11.14 .41 29.55 .332		316	26.48.36	16.56 .272	479.4		44 42	44
DF THE THIRD PROJECTII Z - NUM MASS-VL3									Thresho				155.3	T1 22	8.05 .25 31.24 .144	233.2	2r 40	10.22 .31 27.95 .204	385.9	Hf 72	13.53 .41 23.54 .328	V	/	/	7	[/	/	/
PARAMETERS													152.4	Sc 21	16.46 .24 26.22 .141	228.5	Y 39	21.51 .3 19.78 .201	310.2	La 57	25.31 .36 17.18 .27		474.9	32.57 .46	15.29 .399	:			
TABLE 27					77.33	Be 4		9.856.16 84.54.094		118.4	Mg 12	27.75 .2 16.13 .116	153.7	3 C	751.98.23 13.4.137	222.8	sr 38	53.71 .3 7.837 .198	304.6	Ba 56	58.91 .36 7.324 .268		468.7	82.77 .45	5.972 .397				
	141	- -	0 .11		71.46	11 3	. !	7 .15 52.95 .091		111.6	Na 11	35.02 .2 12.4 .113	147	K 19	64.55 .23 6.896 .135	218	89 23	107 .3	300.9	ទួ	139.2.36		463.4	1 0 1 1 0	242. 0				

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	88.66	He 2	0 .14 0 .095	125.3	Ne 10	1899 .19 .26 .111			Hr 18 763.5 .23 .606 .133	236.4	kr, 36	802.1.29 .572 .19		326.1	Xe 54	744.6.35		4.100 Fin 86	736 .44	419.1	۲ <i>n</i> 71	30.74 .39 16.37 .317			
				116.6	0 L	41.18 .19 11.49 .108		0.40	42.04.22	233.2	5r 35	77.92 .29 5.964 .185		322.3	1	106.7 .34 4.447 .249	0.000	At B5	0 .43 0 .367	413.1	Yb 70	84.44 .39 5.922 .314			
				116.9	8	11.95 .18 41.26 .107			19.76.22 25.43.126	276.5	Se 34	41.36.29 11.07.183		314.4	Te 52	52.25 .34 8.918 .249		Po 84	97.99 .43 5.42 .367	408.4	Ten 69	55.59 .39 8.997 .308			
				112.2	N 7	5.576 .17 87.81 .104		1.011	51 - 7 - 15 15.57 - 21 31.45 - 124	223.8	As 33	31.03.28 14.97.179		311.9	59 21 21	42.26 .34 11.18 .242		400.4 B: 83	46.9 .43 7.88 .365	402.3	Er 68	40.559 12.25 .306			
				107.6	ہ د	9.514 .17 151 .102			51 14 6.194 .21 45.83 .121	218.9	e B	19.67 .28 19.82 .176		\$07.2	с С С	7.703 .33 12.88 .238		Pb 82	71.36 .43	294.5	Ho 67	42.16 .38 11.73 .302			
				96.45	ร 8	3.454 .16 130.1 .098		c.oc1	AL 13 15.42 .21 34.65 .118	214.7	Ga 31	31.5 .27 14.8 .172		303.1	In 49	45. 37 . 33 10. 46 . 233		4/4.4 T1 81	76.64 .42 6.807 .358	9.097	Dy 66	43.22 .38 11.39 .299			
				L			,			212.9	Zn 30	64.63 .27 7.378 .167		297.8	Cd 48	97.48 .33 4.854 .23		7.744 08 PH	214.2 .42 2.43 .353	THA	Tb 45	32.27 .38 15.25 .294			
										207.4	Сп 23	32.5 .27 19.4 .165		294.7	Ag 47	43. U5 . 32 12. 55 . 224		464 Au 79	36.75 .42 13.85 .348	179.9	Gd 64	31.28 .37 15.02 .291			
						:				207	N1 28	21 .26 25.9 .16		288.5	Pd 46	29.92 .32 16.64 .222		Pt 78	25.02 .41 21.24 .345	174.1	Eu 63	69.45 .37 7.076 .285			
										198	Ca 27	20.97 .26 25.35 .159		284.5	Rh 45	23.3 .32 24.94 .218		1r 77	25.41 .41 25.29 .341	20.7	Sm 62	59.79 .37 8.162 .282			
				000	itc Number	a a	astic coettic			194.7	Fe 26	20.84 .25 25.77 .155		278.9	Ru 44	22.83 .31 29.46 .215		446.1 Ds 76	22.29 .41 29.81 .338	7.4.7	Pm 61	0 .36			
				54 44 7 EL/1	Hton	14 V Stor				187.7	74 23	32.02 .25 17.77 .153		273.4	Tc 43	15.61 .31 30.22 .212		441.2 Re 75	20.15 .4 29.38 .333	045	09 PN	37.1 .36 13.11 .274	537.1	U 92	19.7 .46 19.97 .405
28.71 59.71				88.6	1	10.37				184.2	Cr 24	23.33 .25 25.85 .15		268.9	Mo 42	14.1 .31 30.5 .208		4-004 H	15.57 .4 32.62 .329	746.2	Pr 59	33.87 .35 14.36 .269	₽ - <u>2</u> 23- •	Pa 91	0 .45 0 .396
HBER				1	Symbo	-	ora Energy (eV.			177.3	د 23 د	12.08.25 33.94.147		264.6	1₽ qN	12.83 .3 34.35 .204		427.4 Ta 73	12.08 .4 29.76 .325	748.5	ې ۲	28.66 .36 16.79 .268	525.4	Th 90	22.33 .45 22.31 .397
z - NU MAGS-N						ł				174.1	T1 22	8.617 .24 32.31 .144		258.8	2r 40	11.02 .3 28.61 .201		473.7	14.65 .4 23.71 .321		/			/	/
										171	Sc 21	17.61 .24 27.14 .141		253.7	62 >	23.19 .3 20.25 .198		1.2440 La 57	27.39.36 17.42.265	520.4	Ac 89	35.53 .44 15.3 .39			
				88. 64	Be 4	10.37 .16 88.54 .095	C 811		29.45 .2 29.45 .2 16.8 .116	172.8	Ca 20	36.31 .23 13.89 .137		247.4	у В	57.89 .3 8.026 .196		330.1 Ba 56	63.74 .35 7.427 .263	513.4	88 88	89.78 .44 5.976 .388			
	163	 x		82.1	L1 3	7.357 .15 55.5 .092	1 761		57.17 .2 57.17 .2 12.92 .113	165.4	K 19	68.95 .23 7.15 .134		242.2	Rb 37	115.3.29		1.200 Ca 33	150.6.35 3.158.257	509.1	Fr 87	0 .44 0 .384			

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	6.66	ц Т	0 .15		120.1 125 130 129.3 138.8	C + N 7 0 8 F 9 Ne 10	727 .17 5.708 .17 12.25 .18 42.29 .18 1952 .19 62.3 .101 94.26 .103 44.25 .105 12.3 .106 .278 .109		159 160.8 169 169.5 157.9	51 14 P 15 S 16 C1 17 Ar 18	457 2 16.09 21 20.43 21 45.53 22 791.9 2.22 8.84 .118 33.45 .12 27.05 .123 12.25 .642 .128	236.4 241.5 244.2 254.5	Ge 32 As 33 Se 34 Br 35 'kr 36	0.58 .27 32.48 .27 43.33 .28 81.64 .28 840.9 .28 0.73 .167 15.65 .17 11.55 .174 6.222 .176 .596 .18	328.4 333.3 335.7 344.1 348	Sn Su Sb S1 1e 52 1 53 Xe 54	.109.32 44.5 33 55.03 37 112.4 33 784.5 34 53.23 55.03 3.27 254 11.51 227 9.167 234 4.572 234 651 239		Pb B7 B1 B1 D4 D4 D4 B5 B1 B6		421.4 427.4 433.8 478.6 444.9	Ho 67 Er 68 Tm 69 Yb 70 Lu 71	4.5 .37 42.8 .37 58.68 .37 58.44 .38 32.45 .38 1.94 .282 12.47 .283 9.148 .387 6.016 .292 16.62 .295				
					107.8	n a	3.528 .16 139.9 .097		150.4	AI 13	15.9 .2 36.94 .116	1.255	Ga 31	32.95 .27 15.49 .164	324.2	In 49	47.74 .32 10.79 .219	+	19	80.96 .41 6.866 .332	415.5	Dy 66	45.61 .37 11.6 .279				
												230.4	Zn 30	67.53 .26 7.739 .16	318.7	Cd 48	102.6.32 5.011.216	107	H B	226.2 .4 2.453 .328	410.5	Tb 65	34.05 .36 15.54 .274				
												224.6	Cr 23	33.95 .26 20.36 .157	315.6	Ag 47	45.28.31 12.97.211	7 101	Au 79	38.82 .4 13.99 .323	404.1	Gd 64	53 . 36 15. 93 . 272				
								SS Unit				224.5	N1 28	21.91.25	209.1	Pd 46	31.46 .31 17.21 .209	C 907	Pt 78	26.43 .4 21.47 .321	400.4	Eu 63	73.26 .36 7.225 .266				
								cient k in LS				214.8	Co 27	21.87 .25 26.87 .152	305	Rh 45	24.49 .31 25.82 .205		2 I	26.84 .4 25.57 .317	394	Sm 62	63.06 .36 8.338 .264				
INCIDENCE				1000		mic Number	2	lastic Coeffi				211.5	Fe 26	21.73 .25 27.13 .149	299.1	Ru 44	23.99 .3 30.53 .203	***	42 a	23.54 .39	340.5	Pm 61	0 .35 0 .258				
ALA AT NORMAL) 	28 -	4 Ato	16 .094					203.9	E S	33.38 .25 18.71 .147	293.4	Tc 43	16.4 .3 31.33 .2	9 4 2 4	Re 75	21.28 .39 29.75 .309	383.5	07 PN	39.13 .35 13.41 .256	547.4		7%	20.82 .44
PIRICAL FORMU 29 63.55				l	- 66	a di	10.58					200.3	Cr 24	24.3 .24 27.26 .144	288.7	Mo 42	14.81 .3 31.65 .196	0.11	47.13	16.44 .39	378.5	Pr 39	35.71 .35 14.7 .252	543.4	i	га <u>ү</u> 1	0 43
MATSUNAMI EN ILEO MBER						DOWYO	,	old Energy(eV				192.9	د 23	12.58 .24 35.8 .141	284.2	ND 41	13.47 .29 35.68 .193			12.75 .39	371.4	5e 38	30.22 .35 17.2 .251	555.1			23.59 .43
OF THE THIRD PROJECT Z - NUI MASS-IN							I	Thresh				189.7	11 22	8.963 .24 34.12 .138	278.1	2r 40	11.57 .29 29.73 .19	450.2	## 22	15.48 .38 24.06 .299	/	/	/	V	/	/	/
PARAMETERS				-				-				186.6	Sc 21	18.3 .23 28.7 .136	272.8	۲ 39	24.34 .29 21.06 .187	1 172	12	28.87 .34 17.84 .249	550.4	Ac 89	37.33 .43 15.36 .362				
TABLE 29					99.28	Be 4	10.58 .16 95.31 .094		148.2	Mg 12	30.34 .2 17.94 .114	189	Ca 20	37.67 .22 14.72 .132	266.2	Sr 38	60.73 .29 8.352 .185	1 021	Ba Sh	67.18 .34 7.614 .246	543.3	88 88	94.87.43 636				
	184.5	п н	0 .11		92.18	L1 3	7.495 .15		139.9	Na 11	38.26 .19 13.81 .111	181	K 19	71.5 .22	240.6	Rb 37	120.9.29	2.955	1	158.7 .34 3.241 .241	537.3	Fr 87	0 .42 0 .356				

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The Fargement of the factor o				<u> </u>				<u> </u>					<u> </u>	_			—					·				
The state is a state if a state is		171.6	He 2.	0 0 098	224.8	Ne 10	2294 .18 .354 .107	260.1	Ar 18	961.4 .21 .794 .12	372	kr, 36	1064 .26 .7 .158	491.3	Xe 54	1015 . 3 . 729 . 202	722.6	Rn 86	1022 .37	615.5	Lu 71	42.42 .34 17.96 .244				
Tate 30 metrate very application. Spritteners and the second structure of much of model. Impairing the second structure of much of model. Impairing the second structure of much of model. 1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.					210.3	о- ц	49.55 .17 15.69 .104	264.8	CI 17	52.54 .2 15.3 .118	368.8	면 55	103.1 .25 7.334 .155	487	1 53	145.2.3 5.143.198	723.4	At 85	0 .3b 0 .279	607.2	Yb 70	116.5 .34 6.512 .242				
Total 3 Description of the production of production of the production of t					213.2	8	14.26 .17 56.73 .104	265.8	S 16	24.54 .2 33.84 .117	358.7	Se 34	54.67 .2. 13.63 .154	475.1	Te 52	71.08 .3 10.31 .198	713.3	Po 84	136 .36 5.753 .278	501.5	Tm 69	76.62 .33 9.934 .239				
Tate 3 0 means 0 me					206.4	~ z	6.619 .16 121.2 .103	253.5	P 15	19.28 .19 41.92 .115	356.1	As 33	40.87 .25 18.55 .151	473.2	SP 21	57.37 .29	704.1	B1 B3	92.82 .36 8.372 .277	593	Er 68	55.86 .33 13.56 .237				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	·				199.6	ہ ں	11.22 .16 209.5 .102	252.3	Si 14	10.09 .19 61.46 .114	349.5	Ge 32	25.85 .25 24.64 .149	467.1	5 20	10.44 .29 15.04 .191	695.5	Pb 82	98.97 .36 7.814 .275	585.3	Ho 67	58.05 .33 13 .234				
Tate 30 Properties of "Negating perioden interaction of the function of the funct					180.1	ກ ອ	4.057 .15 181 .098	239.4	A1 13	18.93 .19 46.56 .111	344.3	Ga 31	41.29.24	462.3	In 49	61.4 .29 12.28 .188	889	11 81	106.3 .36	577.7	Dy 66	59.47 .33 12.66 .232				
Tate 30 Reserved of "Registry frammer Fignation: Figuation: Fignation: Fignation: Fignation: Fignation: Figuation:					.						343.4	Zn 30	84.35 .24 9.273 .144	455.3	Cd 48	131.8 .29 5.714 .185	681.4	Hg 80	296.8 .36 2.602 .269	9.152	Tb 65	44.36 .32 17.01 .229				
Tate 30 Reprint fragmention of the second of t											335.6	Cu 29	42.33.24 24.45.142	452.2	Ag 47	58.07.28 14.86.182	674.8	Au 79	50.9 .35 14.87 .265	563.2	Gd 64	42.98 .32 17.46 .227				
Tate 30 Remetries or "FR_THERE ACTION FOR THE ACTION FOR							i Unit				337.4	Ni 28	27.22 .23 32.9 .139	443.4	Pd 46	40.32.28 19.73.18	666.4	Pt 78	34.65 .35 22.86 .263	529.3	Eu 63	95.31 .32 7.954 .223				
TRAIL 30 PARAGETERS OF THE TATIBILITY INTERPOLATION CONTRICT CONTRILIACIENCLE CONTRICT CONTRI							tient k in LSS				322.8	Co 27	27.16.23 32.44.138	438-5	Rh 45	31.34 .28 29.71 .177	428-9	Ir 77	35.17 .35 27.29 .261	550.8	Sm 62	82.01 .32 9.192 .221				
TABLE 30 PARAMETERS OF THE THIRD AFTRUMMENTAL FORMULA AT NORMUL. 331.2 331.2 131.1 131.1 2 - NUMBER	INCIDENCE				1000		lastic Coeffic				319.1	Fe 26	26.9 .23 32.88 .135	430.6	Ru 44	30.67 .28 35.19 .175	650.7	05 76	30.84 .35	547.3	Pm 61	0 .31 0 .216				
TABLE 30 ReARETERS OF THE THICK FLORM 731.2 321.2 8.4 1 0.113 110. 130.4 167 1.1 3 1.1 3 1.1 3 1.1 3 1.1 10. 1.10. 10. 1.10. 10. 1.10. 10. 1.11. 10. 1.12.11. 11. 1.13.11.11. 11. 1.13.11.11. 11. 1.13.11.11. 11. 1.13.11.11. 11. 1.13.11.11. 11. 1.13.11.11.12 11. 1.13.11.11.12 11. 1.13.11.11.12 204.11 1.13.11.11.12 204.11 1.13.11.11 20.11 1.13.11.11 20.11 1.13.11.11 20.11 1.13.11.11 20.11 1.13.11.11 20.11 1.13.11.11 20.11 1.13.11.11 20.11 1.13.11.12 21.12 1.13.11.12 21.12 1.14.12 11.12 1.14.12 11.12 1.14.12 11.12 1.14.12	4LA AT NORMAL						15 10 10 10 10				308.2	К Ч	41.27 .23 22.71 .134	423.2	Tc 43	20.94 .27	644.6	Re 73	27.87 .35	537.6	09 PN	50.8 .31 14.86 .215	769.9	U 92	27.4 .38	20.68 .305
TABLE 30 PARAMETERS OF THE THILE OFTENDERTILE 321.2 H 1 9 :11 0 :136.4 167 1.1 3 Be 1.136.4 167 1.136.4 167 1.136.4 167 1.136.4 122.11.015 1.136.4 122.11.015 2.275 111 1.1 Nq<12	PIRICAL FORMU 5 36 83.8				167		123.6				304.1	с 24	29.95 .22 33.2 .131	417.4	Mo 42	18.89 .27 36.68 .171	636.B	M 74	21.52 .34 35.49 .253	531.5	Pr 59	46.32 .31 16.34 .212	745.7	Pa 91	0.38	0 .299
TABLE 30 PARAMETERS OF THE THE PROJECT 2 - NU MASSAN 321.2 H 1 1 0 :11 0 :11 3 156.4 167 156.4 167 156.4 167 156.4 167 156.4 167 156.4 167 156.4 167 156.4 167 156.4 167 156.4 167 156.4 167 156.2 11 151.1 12 2253 237.3 235.9 13 235.9 13 151.108 25.7 255.9 11 230.4 12 151.108 25.7 25.91.12 35.94 230.1 25.91 151.108 25.7 255.91 19.21 230.4 35.94 230.4 35.94 230.5 35.94 230.6 97.76 230.7 35.94 230.8 19.1.23 35.97 19.1.23 35.97 19.1.23 35.97 19.1.23 25.91 11.22	, Matsunami Em TLEK MBER				ć	namyn	old Energy(eV				293.4	2	15.48 .22 43.67 .13	412	Nb 41	17.15 .27 41.48 .168	629.6	Ta 73	16.68 .34 32.47 .25	521.9	5	39.19 .31 19.12 .211	754.4	41 8	31.04 .38	23.23 .299
TABLE 30 PARAMETERS 321:2 156.4 167 115.4 167 167 155.4 151.1 167 155.4 121.1 105 113 18.4 167 155.4 121.1 105 113 18.4 167 114 10 12 125 133.16 1095 111 10 12 111 10 12 1225 237.3 111 1225 2304 111 1219 108 227.4 286.4 1217 108 227.9 111 1217 110 227.1 225.1 225.1 1212 93.1 122 93.2 31.2 130.4 230.4 337.7 350.8 212.8 15.55 20.4 280.4 350.8 212.8 15.55 20.4 20.8 20.9 212.8 15.55 20.4 20.8 20.9 212.8 <	OF THE THIRD PROJECT 2 - NU MASS-N						Thresh				289.9	11 23	11 .22 41.78 .128	403.7	Zr 40	34.62 .166	621.9	Hf 72	20.25 .34 25.93 .247		/	/	V	/	/	/
TABLE 30 321:2 1156.4 167 1156.4 167 167 1156.4 167 167 1156.4 113 8e 4 1156.4 11 3 8e 4 1156.4 11 3 8e 4 1156.4 11 3 8e 4 1156.4 11 10 12 1159.093 121.01 225.4 11 2255 229.5 277.3 11 1251.108 257.4 11 12 145.19 121 106 227.4 145.19 121 108 257.4 155.2 101 21 124 155.2 102 227.4 337.7 155.2 102 227.4 337.7 155.2 123 102.2 337.7 155.2 200.4 2 204.3 155.2 205.4 30.6 206.3 155.2 206.4 3 337.7 155.2 206.4 3 337.7 155.2 206.4 3 337.7 155.2 206.4 3 337.7	PARAMETERS										286.4	Sc 21	22.38 .21 35.28 .126	396.8	ůî ≻	30.91 .26 24.58 .164	512.8	3) [37.42 .31 19.86 .209	748.8	Ac 89	49.1 .35 16 .294				
321.2 H 1 1156.4 1156.4 1156.4 1156.4 1156.4 1156.4 1156.4 1156.4 1155.2	TABLE 30				167	8 8 7	12.11 .15 123.6 .095	237.3	Ng 12	35.94 .18 22.7 .11	292.4	3 5	45.8 .21 18.21 .124	387.7	ъ В	77.06 .26	504.3	Ba 56	87.04 .31 8.466 .208	739.5	Ra 88	124.8 . T8 6.254 . 293				
		321.2	- I	0 11: 0	156.4	с г	8.534 .14 77.89 .093	225	Na 11	45.19 .18 17.51 .108	280.6	K 19	86.78 .21 9.391 .122	380.4	вь 37 У	153.2 .26 4.899 .16	499.8	55	205.4.3 3.627.204	731.9	Fr 87	6. 60				



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	447.1	Ца 13	0 .12 0 .105		542.1	Ne 10	3042 .16 .533 .108		589.2	Ar 18	1.154 .19	769.8	кг 36	1580 .23 .952 .138	ven *	C *0004	Xe 54	1569 .26 .933 .166	1320	Rn 86	1644 .31 .881 .221	1157	Lu 71	67.15 .28 21.9 .193				
L					209.8	с 1	65.44 .16 23.66 .106		606.8	11	72.31 .18 22.4 .114	767.6	Br 35	152.4.22 10.02.136		8.004	1 53	224 .26 6.616 .164	1330	At BS	0 .3	1143	Yb 70	184.2.28 7.956.192				
					522.8	8 0	18.7 .15 86.04 .107		614.7	S 16	33.55 .18 49.84 .114	748.1	5a 34	80.67 .22 18.65 .135		C *0054	Te 52	109.6 .26 13.25 .163	1311	Po 84	218 .3 6.774 .215	1135	Tm 69	121 .28 17.19 .189				
					510.5	2 2	8.625 .15 184.6 .107		588.8	۹ ۲	26.27 .17 61.85 .113	747.4	As 33	60.03 .22 25.53 .134		4.164	Sb 51	88.15.25 16.83.16	1295	B1 83	148.7.5 9.868.214	1121	Er 68	88.12 .28 16.66 .188				
					498.4	ہ ت	14.54 .14 320.2 .106		591.3	S1 14	13.66 .17 91.16 .112	736.4	Ge 32	37.85 .22 34.02 .132		\$75	5n 50	16.01 .25 19.55 .159	1281	Pb 82	158.5 .3 9.226 .213	1108	Ho 67	91.48 .28 16.02 .187				
					452.6	ກ a	5.231 .14 277.3 .102		563.5	AI 13	25.54 .17 69.2 .11	729.2	Ga 31	60.25 .21 25.62 .131	:-	\$11.3	In 49	93.88 .25 16.03 .157	1269	T1 81	170 .3 8.599 .211	105=	Dy 66	93.62 .28 15.64 .185				
												733	Zn 30	122.4.21 12.94.13		8.004	Cd 48	201.1 .25 7.481 .155	1260	н _д во	474.4 .3 3.092 .209	1087	Tb 65	69.71 .28 21.1 .183				
												718.9	Cu 29	61.25 .21 34.22 .128		904° 3	Ag 47	88.31 .24 19.57 .153	1250	Au 79	B1.26 .3 17.74 .207	1073	Gd 64	67.48 .27 21.7 .182				
								2100 e				729.3	N1 28	39.13 .2 46.39 .127		1 898.4	9 4 Pd	61.23.24 26.03.152	1236	Pt 78	55.27 .3 27.32 .205	1070	Eu 63	149.3.27 9.942.179				
								CIENC K 11 LO				698.1	Co 27	39.03 .2 45.73 .126		F87.4	Rh 45	47.46 .24 39.38 .15	1224	Ir 77	56.05 .29 32.69 .204	1055	Sm 62	128.3 .27 11.51 .178				
INCIDENCE				1000	Tetter Visiter							694.5	Fe 26	38.47 .2 46.57 .125		868.8	Ru 44	46.75 .149 46.75 .149	1211	0s 76	49.11 .29 38.69 .202	1053	Pm 61	0 .27 0 .175				-
ala at Normal												672.3	Hn 25	58.9 .2 32.2 .123		836.1	Tc 43	31.59 .24 48.22 .148	1202	Re 75	44.32 .29 38.43 .2	1035	07 PN	79.23 .27 18.74 .174	1395	U 92	44.24 .32 23.73 .232	
PIRICAL FORMU 54 131.3					423		1.061					667.7	Cr 24	42.55 .2 47.3 .122		847.9	Mo 42	28.41 .23 49.05 .146	1190	M 74	34.2 .29 42.88 .198	1027	4 8	72.11 .26 20.67 .172	1392	16 ed	0 .32 0 .228	
MATSUNANI EM TLE MBER					odau0		L	old Energy (ev				646	د ۲	21.94 .2 62.32 .121		840.3	ND 41	25.73 .23 55.7 .145	1178	Ta 73	26.48 .29 39.35 .197	1009	28 Ce 28	60.96 .26 24.22 .171	1371	Th 90	50.04 .32 26.8 .228	
C THE THIRD PROJECT Z - NU MASS-N												642.8	T1 22	15.51 .19 59.92 .12		822.6	Zr 40	22.03.23	1166	Hf 72	32.1 .29 31.51 .195		/	/		/	/	
PARAMETERS				-								439.6	Sc 21	31.39 .19 50.84 .119		814.2	42 >	46.15 .23 33.19 .142	992.8	La 57	58.16 .26 25.19 .17	1364	Ac 89	79.08.31				
TABLE 31					423.8	Be 4	15.53 .14		563.6	Mg 12	48.19 .17 33.9 .11	640.6	50 C	63.71 .19 26.46 .118		797.2	Sr 38	114.9.23 13.2.141	978	Ba 56	135.1.26 10.78.169	1348	Ra 88	200.8 .31 7.255 .224				
	851.8	- H	0 .147		401.2	Li 3	10.88 .13		537.2	Na 11	60.35 .16 26.21 .108	636	K 19	120.4 .18 13.67 .117		784.9	В 37	227.8.23 6.644.135	973.1	55 52	318 .26 4.632 .167	1336	Fr 87	0 .31 0 .222				

	TABLE 3	2 PARAMETERI	B OF THE THIRI 2 - NUF MASS-NU	D MATGUNAMI EL ILE 18ER	PJRICAL FORMU 0 00.5	ALA AT NORMAL	INCIDENCE						•		r		
2175																•	1128
 *																	He 2.
0 0 139						•											0 .11 0 .112
1002	1050	r			1050	T EN	000					1114	1221	1243	1265	1223	. 5621
с Г	Be 4			Symbol	Be 4	Atom	dc Number					ю в	ہ د	N N	8 0	F P	Ne 10
13.71 .12	19.63 .13 287 .106		ć	-	19.63	13 106			4			6.435 .13 417.7 .108	18.5 .13 481.6 .112	11.01 .14 276.9 .112	23.96 .14 128.8 .112	84.24 .14 35.29 .11	3927 .15 .793 .113
3761		. <i>.</i>		otu cilergylevi					, 110				1 104	8721	3041	7021	1744
														1007		101	
78-26 -15	62.67 .15											AI 13 33.36 .15	17.89 .16	34.55 .16	5 16 44.23 .16	CL 17 95.8 .16	AF 18
38.89 .112	50.23 .114											102.2 .113	134.5 .115	90.94 .114	73.18 .116	32.77 .115	1.68 .114
1451	1503	1443	1442	1441	1486	1489	1535	1535	1602	1568	1594	1575	1584	1602	1595	1634	1630
K 19	Ca 20	Sc 21	11 22	22 >	Cr 24	ž 12	Fe 2b	Co 27	N1 28	с С	ZN 30	Ga 31	Ge 32	As 33	Se 34	r R	kr · 36
140.5 .17	85.09 .17 38.51 .119	42.19 .17 75.6 .117	20.92 .17 86.47 .118	29.73 .18 89.64 .118	57.76 .18 67.97 .119	80.26 .18 46.13 .12	52.51 .18 66.64 .121	53.46 .18 65.23 .121	53.63 .18 66.19 .123	84.4 .19 48.59 .123	169.1 .19 18.34 .124	83.6 .19 36.15 .124	52.69 .19 47.87 .125	83.79 .19 35.84 .126	113 .2 26.08 .127	213.8.2 14 .128	2225 .2 1.324 .128
															L		
1458	1679	1712	1730	1757	1767	1778	1799	1823	1828	1858	1852	1871	1875	1868	1874	1922	1923
62 62	sr 38	6F >	Zr 40	Nb 41	Mo 42	Tc 43	Ru 44	Rh 45	Pd 46	Ag 47	Cd 48	In 49	S S	5 5 5	Te 52	8	Xe 54
321.5 .2 9.232 .129	162.5 .2 18.31 .13	45.37 .2 45.96 .131	31.27 .2 64.39 .132	36.59 .21 76.85 .133	40.51 .21 67.48 .134	45.16 .21 66.16 .135	66.4 .21 64.04 .136	68.1 .21 53.84 .137	88.1 .21 35.48 .138	127.3.21 26.64.139	290.7 .22 10.14 .14	136 .22 21.68 .141	23.26.22 26.36.142	128.3 .22 22.64 .143	160.2 .22 17.72 .144	327.3 .22 8.858 .145	2299 .23 1.245 .146
1950	1952	1979	2252	2272	2289	2309	2320	2343	2361	2384	2398	2410	2428	2453	2481	2515	2483
5	Ba 56	(r= 37	Hf 72	Ta 73	W 74	Re 75	0= 76	Ir 77	Pt 78	Au 79	Hg BO	11 81	Pb 82	B1 83	Pa 84	At 85	Rn 86
466.5 .23 6.171 .147	198.8 23 14.31 .148	85.46 .23 33.39 .149	48.34 .25 40.49 .165	39.92 .25 50.46 .166	51.62 .25 54.87 .167	66.98 .25 49.1 .168	74.34.25	84.93.25 41.58.171	83.86 .26 34.67 .172	123.4.26 22.48.173	721.4 .26 3.909 .174	258.9.26 10.84.176	241.6.26 11.61.177	226.9 .26 12.4 .178	332.8.26 8.505.178	0 -26 0 -179	2519 .27 1.097 .182
2511	2529	2557		2008	2041	2053	2086	2082	2108	2105	2131	2142	2162	2183	2208	2216	2239
Fr 87	Ra 88	Ac 89	/	Ce Sg	Pr 59	09 PN	Pa 61	Sm 62	Eu 63	Gd 64	Tb á5	Dy 66	Ho 67	Er 68	Ta 69	Yb 70	Lu 71
0 .27 0 .183	308.3 .27 9.008 .184	121.4 .27 23 .185	/	89.87 .25 32.07 .15	106.4 .23 27.36 .151	117.1 .23 24.73 .152	0 .153	190.4 .24 15.11 .154	221.7 .24 13.04 .155	100.5 .24 28.34 .156	103.9.24 27.52.157	139.8 .24 20.34 .159	136.8.24 20.8.16	132 .24 21.59 .161	181.4 .24 15.78 .162	276.7.25	101 . 25 28.22 . 164
			$\left[\right]$	2565	2604	2601											
			/	Th 90	Pa 91	ц 22											
			/	76.97 .27	0	48.18 .27											
			7	33.14 .187	0 .187	29.23 .189											

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- Fig. 1 Best-fit values of f for light-ion sputtering, where the ratio of f to $\sqrt{U_s}$ is plotted as a function of the mass ratio M_2/M_1 , the solid line is calculated from eq.(8).
- Fig. 2 Best-fit values of θ_{opt} for light-ion sputtering, where the best-fit θ_{opt} 's are plotted against η and the solid line is the theoretical curve calculated from Eq. (12).
- Fig. 3 The best-fit values of f for relatively high-energy heavy ion sputtering, where the solid line corresponds to Sigmund f_s of m = 1/3.
- Fig. 4 The ratios of the best-fit f's to Sigmund f_s as a function of $\eta = 1 - (E_{th}/E)^{\frac{1}{2}}$, where the solid line corresponds to Eq. (17).
- Fig. 5 The best-fit values of 90° θ_{opt} as a function of ψ , where the solid line corresponds to $\theta_{opt} = 90^\circ - 286 \psi^{0.45}$.

Figs. 6 through 58

The normalized sputtering yield $Y(\theta)/Y(0)$ as a function of the angle of incidence, where the solid lines in these figures are best-fit curves to the present empirical formula, and the solid lines with x marks show the results calculated by putting the average values of f and Σ into the present empirical formula. The average parameters of f and Σ are easily calculated using the parameters listed in Table 5 through 18.

- 53 -



f

- 54 --







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- 59 -





(0) \/ (8) \







(0) \/ (+9) \



(0) // (8) /



(0) \/ (8) \







- 67 -


- 68 --



- 69 --



- 70 -







- 73 -







- 76 -



- 77 -



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- 78 -







- 81 -













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- 87 --

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- 88 -



- 89 -







Fig. 38



- 92 -



- 93 -



- 94 -



- 95 -



(0) Y (8) Y



- 97 -



- 98 -







- 100 -

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- 101 -



(0) Y (9) Y






- 105 --









- 109 -



- 110 -



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	(1981)
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